WINSOURCE ELECTRONICS

THE DATASHEET OF

LT3972IDD#PBF

33V, 3.5A, 2.4MHz Step-Down Switching Regulator with 75µA Quiescent Current

FEATURES

- **Wide Input Range:**
  Operation from 3.6V to 33V
  Overvoltage Lockout Protects Circuits Through 62V Transients
- **3.5A Maximum Output Current**
- **Low Ripple (<15mV$_{P-P}$) Burst Mode® Operation:**
  I_Q = 75µA at 12V$_{IN}$ to 3.3V$_{OUT}$
- **Adjustable Switching Frequency: 200kHz to 2.4MHz**
- **Low Shutdown Current: I_Q < 1µA**
- **Integrated Boost Diode**
- **Synchronizable Between 250kHz to 2MHz**
- Power Good Flag
- Saturating Switch Design: 95mΩ On-Resistance
- Output Voltage: 0.79V to 30V
- Thermal Protection
- Soft-Start Capability
- Small 10-Pin Thermally Enhanced MSOP and (3mm × 3mm) DFN Packages

APPLICATIONS

- Automotive Battery Regulation
- Distributed Supply Regulation
- Industrial Supplies
- Wall Transformer Regulation

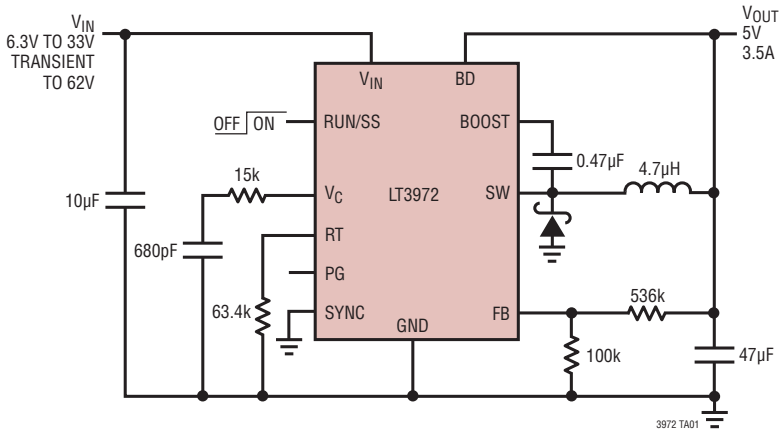
DESCRIPTION

The LT®3972 is an adjustable frequency (200kHz to 2.4MHz) monolithic buck switching regulator that accepts input voltages up to 33V (62V maximum). A high efficiency 95mΩ switch is included on the die along with a boost Schottky diode and the necessary oscillator, control and logic circuitry. Current mode topology is used for fast transient response and good loop stability. Low ripple Burst Mode operation maintains high efficiency at low output currents while keeping output ripple below 15mV in a typical application. In addition, the LT3972 can further enhance low output current efficiency by drawing bias current from the output when V_{OUT} is above 3V. Shutdown reduces input supply current to less than 1µA while a resistor and capacitor on the RUN/SS pin provide a controlled output voltage ramp (soft-start). A power good flag signals when V_{OUT} reaches 91% of the programmed output voltage. The LT3972 is available in 10-pin MSOP and 3mm × 3mm DFN packages with exposed pads for low thermal resistance.

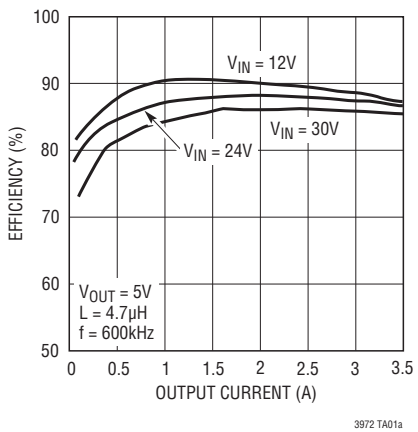
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TYPICAL APPLICATION

5V Step-Down Converter



Efficiency

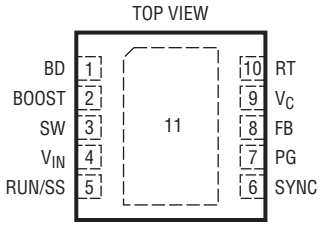


ABSOLUTE MAXIMUM RATINGS (Note 1)

V_{IN}, RUN/SS Voltage (Note 5) 62V
BOOST Pin Voltage 56V
BOOST Pin Above SW Pin 30V
FB, RT, V_C Voltage 5V
PG, BD, SYNC Voltage 30V

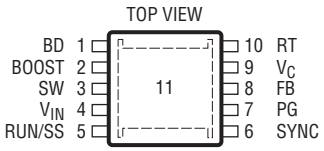
Operating Junction Temperature Range (Note 2)
LT3972E ..... –40°C to 125°C
LT3972I ..... –40°C to 125°C
LT3972H ..... –40°C to 150°C
Storage Temperature Range ..... –65°C to 150°C
Lead Temperature (Soldering, 10 sec)
(MSE Only) ..... 300°C

PIN CONFIGURATION



DD PACKAGE
10-LEAD (3mm × 3mm) PLASTIC DFN

θ_{JA} = 45°C/W, θ_{JC} = 10°C/W
EXPOSED PAD (PIN 11) IS GND, MUST BE SOLDERED TO PCB



MSE PACKAGE
10-LEAD PLASTIC MSOP

θ_{JA} = 45°C/W, θ_{JC} = 10°C/W
EXPOSED PAD (PIN 11) IS GND, MUST BE SOLDERED TO PCB

ORDER INFORMATION

LEAD FREE FINISH	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	TEMPERATURE RANGE
LT3972EDD#PBF	LT3972EDD#TRPBF	LDXR	10-Lead (3mm × 3mm) Plastic DFN	–40°C to 125°C
LT3972IDD#PBF	LT3972IDD#TRPBF	LDXR	10-Lead (3mm × 3mm) Plastic DFN	–40°C to 125°C
LT3972EMSE#PBF	LT3972EMSE#TRPBF	LTDXS	10-Lead Plastic MSOP	–40°C to 125°C
LT3972IMSE#PBF	LT3972IMSE#TRPBF	LTDXS	10-Lead Plastic MSOP	–40°C to 125°C
LT3972HMSE#PBF	LT3972HMSE#TRPBF	LTDXS	10-Lead Plastic MSOP	–40°C to 150°C

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.
Consult LTC Marketing for information on non-standard lead based finish parts.

For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at T_A = 25°C. V_{IN} = 10V, $V_{RUN/SS}$ = 10V, V_{BOOST} = 15V, V_{BD} = 3.3V unless otherwise noted. (Note 2)

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
Minimum Input Voltage		●		3	3.6	V
V_{IN} Overvoltage Lockout		●	33	35	37	V
Quiescent Current from V_{IN}	$V_{RUN/SS}$ = 0.2V			0.01	0.5	µA
	V_{BD} = 3V, Not Switching	●		30	65	µA
	V_{BD} = 0, Not Switching			120	160	µA

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at T_A = 25°C. V_{IN} = 10V, $V_{RUN/SS}$ = 10V, V_{BOOST} = 15V, V_{BD} = 3.3V unless otherwise noted. (Note 2)

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
Quiescent Current from BD	$V_{RUN/SS}$ = 0.2V			0.01	0.5	µA
	V_{BD} = 3V, Not Switching	●		90	130	µA
	V_{BD} = 0, Not Switching			1	5	µA
Minimum Bias Voltage (BD Pin)				2.7	3	V
Feedback Voltage		 ●	780 775	790 790	800 805	mV mV
FB Pin Bias Current (Note 3)	V_{FB} = 0.8V, V_C = 1.2V	●		10	40	nA
FB Voltage Line Regulation	4V < V_{IN} < 33V			0.002	0.01	%/V
Error Amp g_m				500		µmho
Error Amp Gain				2000		
V_C Source Current				60		µA
V_C Sink Current				60		µA
V_C Pin to Switch Current Gain				5.3		A/V
V_C Clamp Voltage				2		V
Switching Frequency	R_T = 8.66k R_T = 29.4k R_T = 187k		2.2 1.0 200	2.45 1.1 230	2.7 1.25 260	MHz MHz kHz
Minimum Switch Off-Time		●		60	150	ns
Switch Current Limit	Duty Cycle = 5%		4.6	5.4	6.2	A
Switch V_{CESAT}	I_{SW} = 3.5A			335		mV
Boost Schottky Reverse Leakage	V_{BD} = 0V			0.02	2	µA
Minimum Boost Voltage (Note 4)		●		1.5	2	V
BOOST Pin Current	I_{SW} = 1A			35	50	mA
RUN/SS Pin Current	$V_{RUN/SS}$ = 2.5V			5	8	µA
RUN/SS Input Voltage High					2.5	V
RUN/SS Input Voltage Low			0.2			V
PG Threshold Offset from Feedback Voltage	V_{FB} Rising			65		mV
PG Hysteresis				10		mV
PG Leakage	V_{PG} = 5V			0.1	1	µA
PG Sink Current	V_{PG} = 0.4V	●	200	800		µA
SYNC Low Threshold			0.5			V
SYNC High Threshold					0.7	V
SYNC Pin Bias Current	V_{SYNC} = 0V			0.1		µA

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: The LT3972E is guaranteed to meet performance specifications from 0°C to 125°C. Specifications over the –40°C to 125°C operating temperature range are assured by design, characterization and correlation with statistical process controls. The LT3972I specifications are guaranteed over the –40°C to 125°C temperature range. The LT3972H specifications are guaranteed over the –40°C to 150°C operating temperature range. High junction temperatures degrade operating lifetimes. Operating lifetime is derated at junction temperatures greater than 125°C.

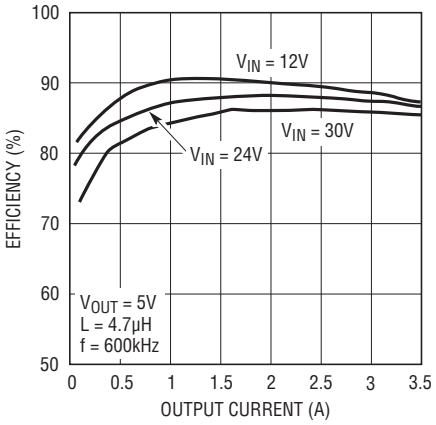
Note 3: Bias current flows out of the FB pin.

Note 4: This is the minimum voltage across the boost capacitor needed to guarantee full saturation of the switch.

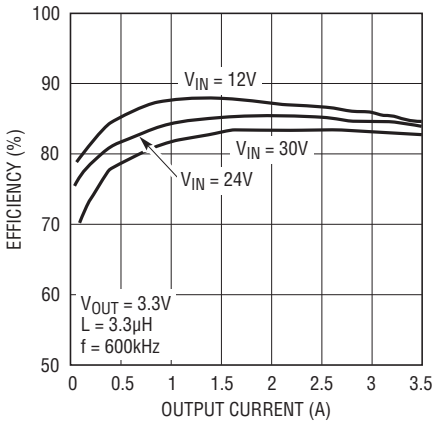
Note 5: Absolute Maximum at V_{IN} and RUN/SS pins is 62V for non-repetitive 1 minute transients, and 40V for continuous operation.

TYPICAL PERFORMANCE CHARACTERISTICS T_A = 25°C unless otherwise noted.

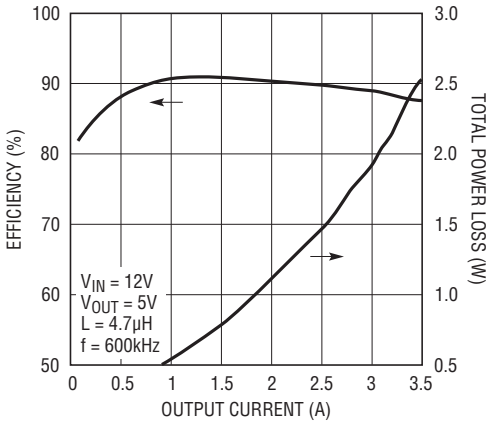
Efficiency



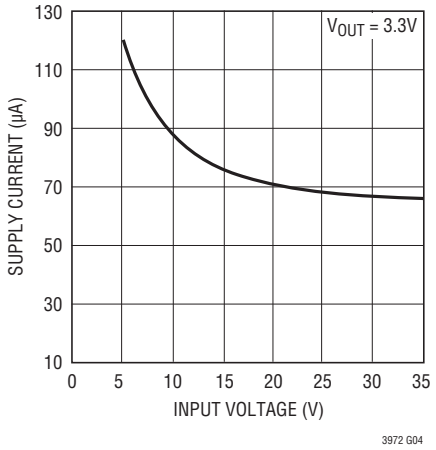
Efficiency



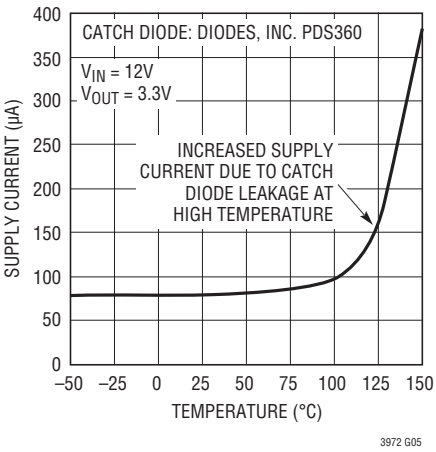
Efficiency



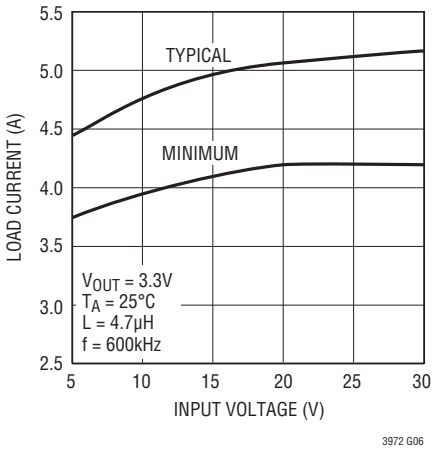
No-Load Supply Current



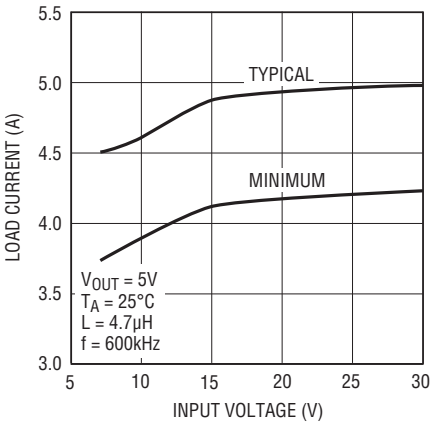
No-Load Supply Current



Maximum Load Current



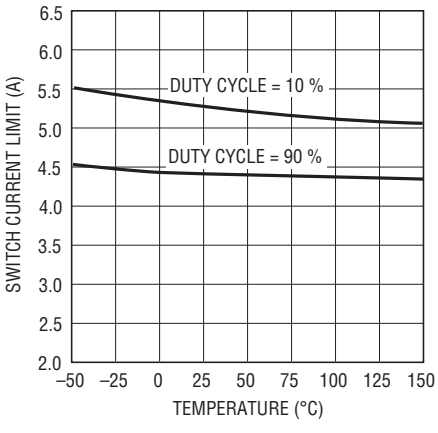
Maximum Load Current



Switch Current Limit

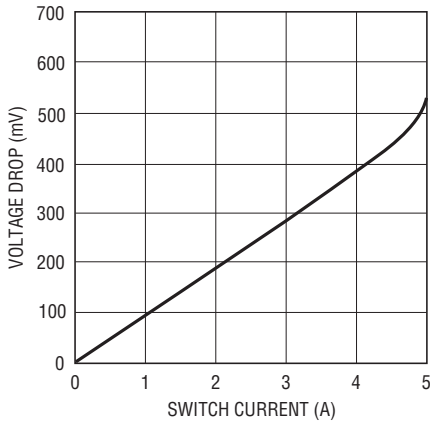


Switch Current Limit



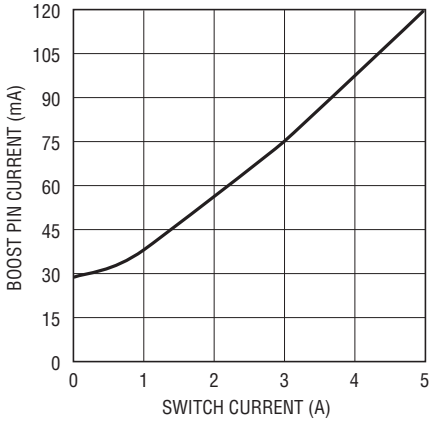
TYPICAL PERFORMANCE CHARACTERISTICS T_A = 25°C unless otherwise noted.

Switch Voltage Drop



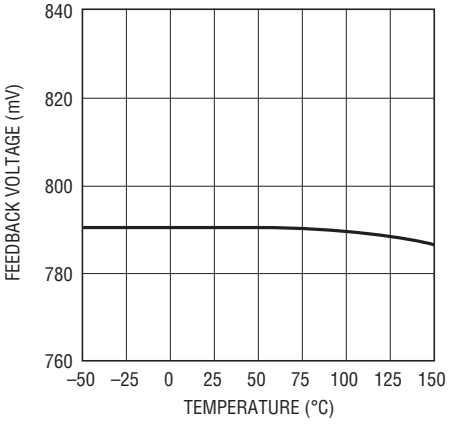
3972 G10

BOOST Pin Current



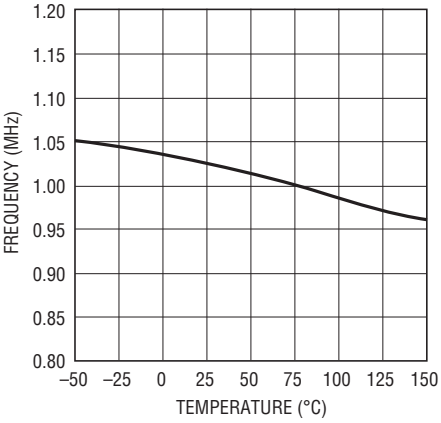
3972 G11

Feedback Voltage



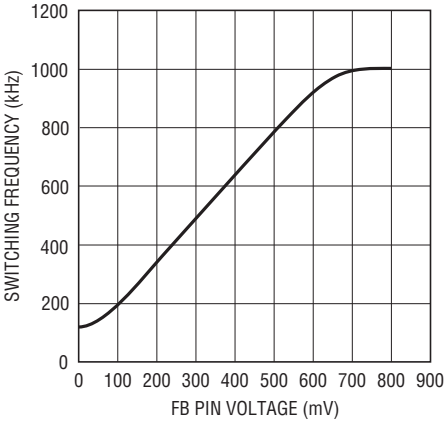
3972 G12

Switching Frequency



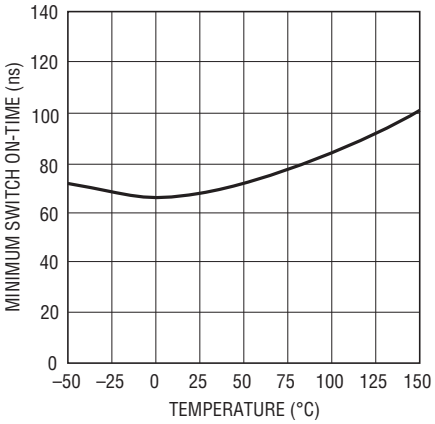
3972 G13

Frequency Foldback



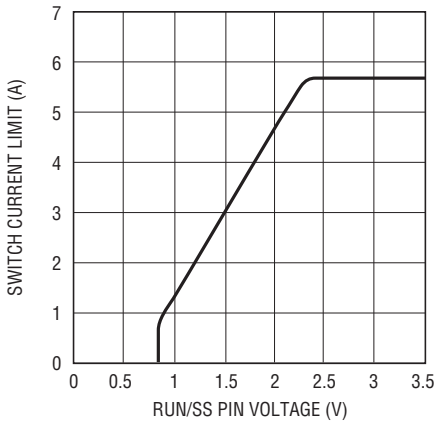
3972 G14

Minimum Switch On-Time



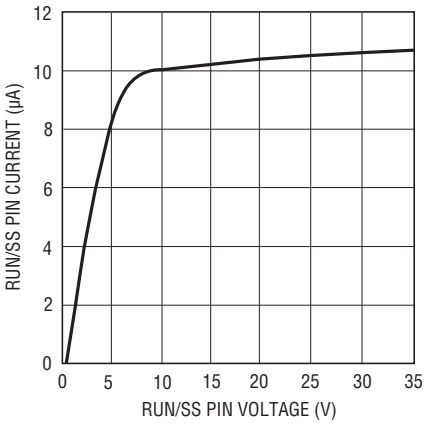
3972 G15

Soft-Start



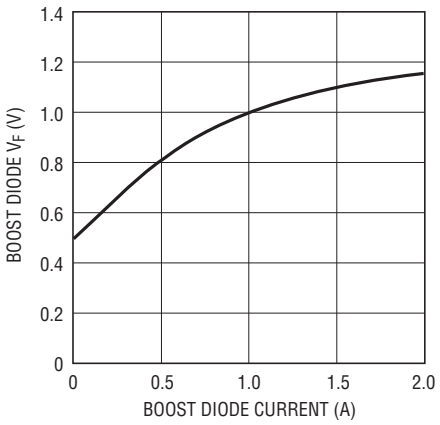
3972 G16

RUN/SS Pin Current



3972 G17

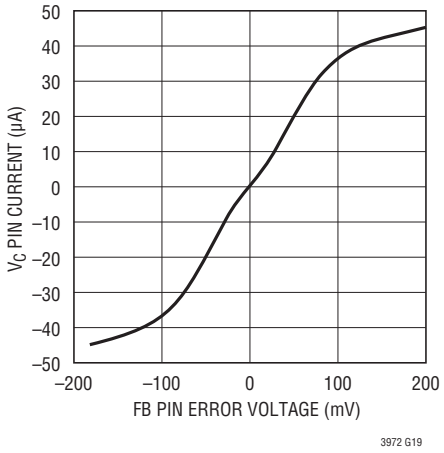
Boost Diode



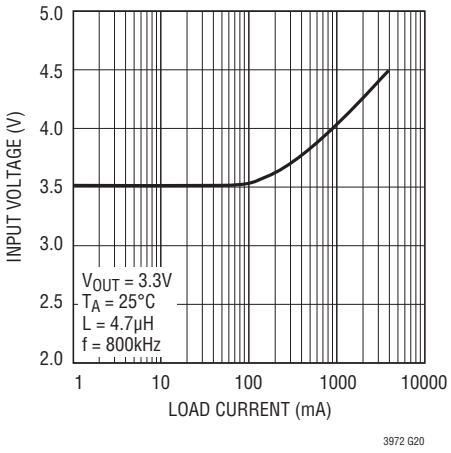
3972 G18

TYPICAL PERFORMANCE CHARACTERISTICS T_A = 25°C unless otherwise noted.

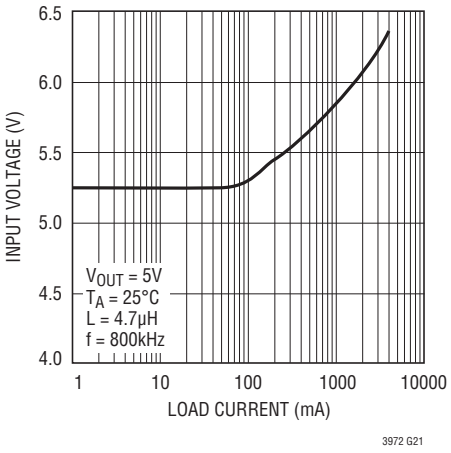
Error Amp Output Current



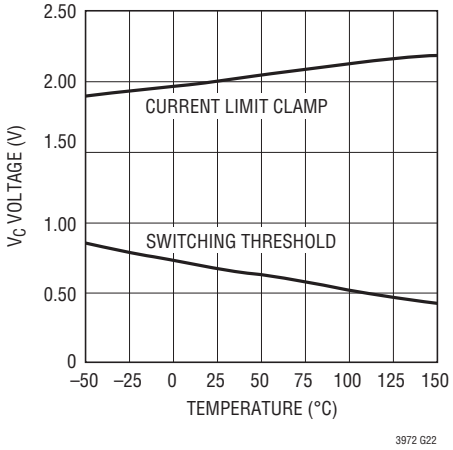
Minimum Input Voltage



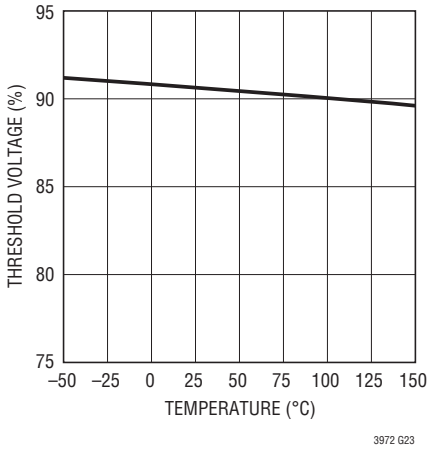
Minimum Input Voltage



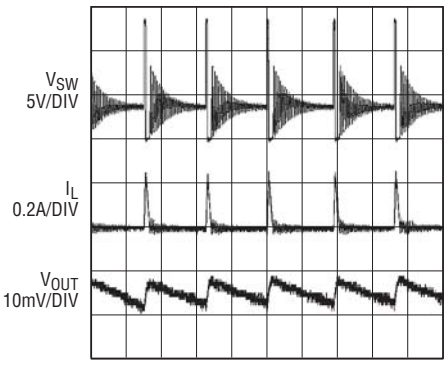
V_C Voltages



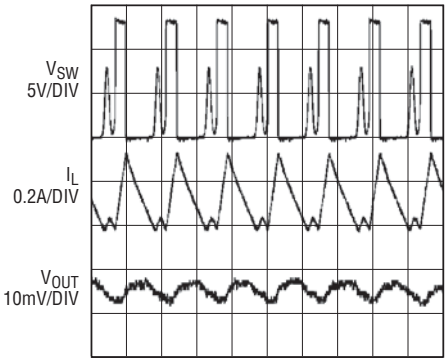
Power Good Threshold



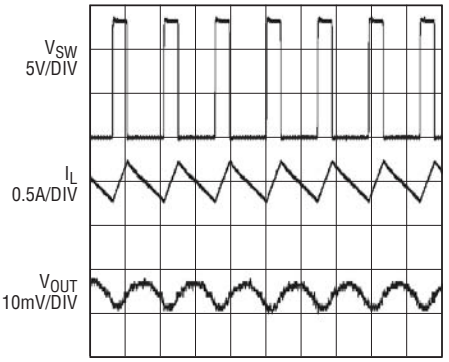
Switching Waveforms; Burst Mode Operation



Switching Waveforms; Transition from Burst Mode Operation to Full Frequency



Switching Waveforms; Full Frequency Continuous Operation



PIN FUNCTIONS

BD (Pin 1): This pin connects to the anode of the boost Schottky diode. BD also supplies current to the internal regulator.

BOOST (Pin 2): This pin is used to provide a drive voltage, higher than the input voltage, to the internal bipolar NPN power switch.

SW (Pin 3): The SW pin is the output of the internal power switch. Connect this pin to the inductor, catch diode and boost capacitor.

V_{IN} (Pin 4): The V_{IN} pin supplies current to the LT3972's internal regulator and to the internal power switch. This pin must be locally bypassed.

RUN/SS (Pin 5): The RUN/SS pin is used to put the LT3972 in shutdown mode. Tie to ground to shut down the LT3972. Tie to 2.5V or more for normal operation. If the shutdown feature is not used, tie this pin to the V_{IN} pin. RUN/SS also provides a soft-start function; see the Applications Information section.

SYNC (Pin 6): This is the external clock synchronization input. Ground this pin for low ripple Burst Mode operation at low output loads. Tie to a clock source for synchronization. Clock edges should have rise and fall times faster than 1µs. Tie Pin to GND if not used. See Synchronization section in Applications Information.

PG (Pin 7): The PG pin is the open-collector output of an internal comparator. PG remains low until the FB pin is within 9% of the final regulation voltage. PG output is valid when V_{IN} is above 3.6V and RUN/SS is high.

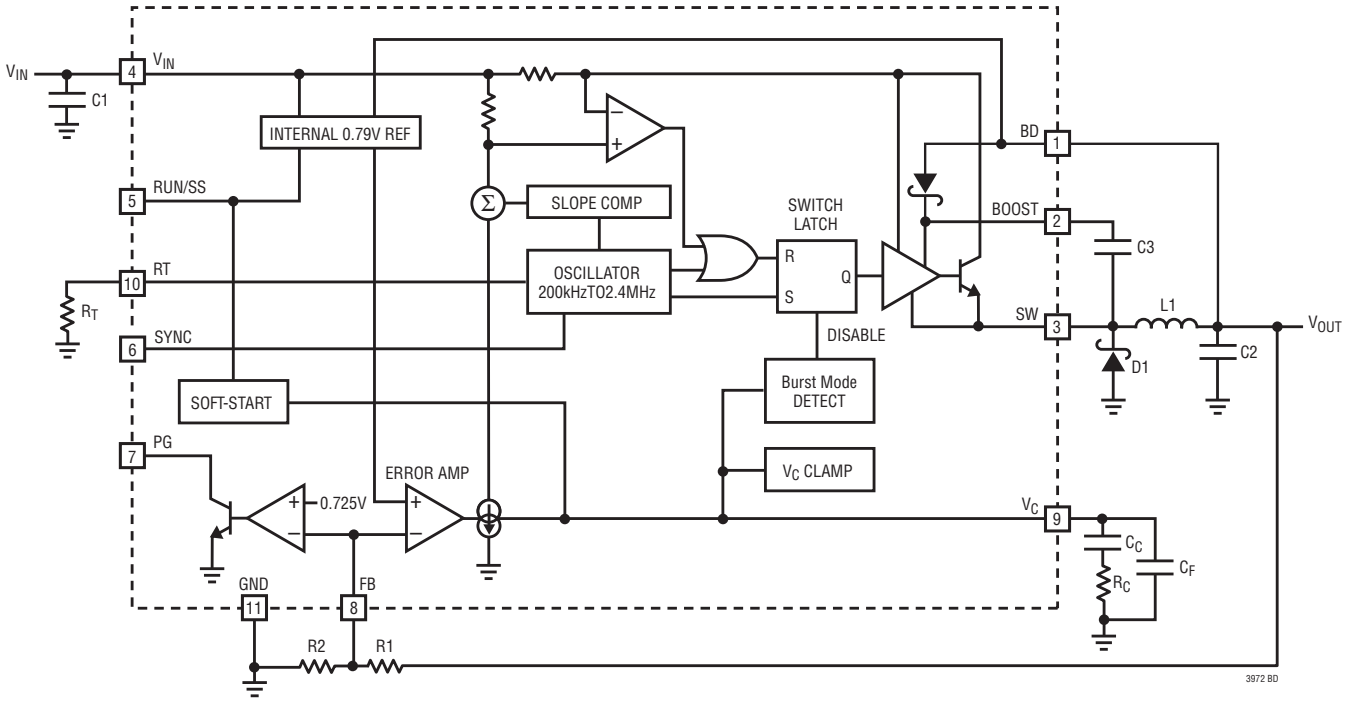
FB (Pin 8): The LT3972 regulates the FB pin to 0.790V. Connect the feedback resistor divider tap to this pin.

V_C (Pin 9): The V_C pin is the output of the internal error amplifier. The voltage on this pin controls the peak switch current. Tie an RC network from this pin to ground to compensate the control loop.

RT (Pin 10): Oscillator Resistor Input. Connecting a resistor to ground from this pin sets the switching frequency.

Exposed Pad (Pin 11): Ground. The Exposed Pad must be soldered to PCB.

BLOCK DIAGRAM



OPERATION

The LT3972 is a constant frequency, current mode step-down regulator. An oscillator, with frequency set by RT, enables an RS flip-flop, turning on the internal power switch. An amplifier and comparator monitor the current flowing between the V_{IN} and SW pins, turning the switch off when this current reaches a level determined by the voltage at V_C. An error amplifier measures the output voltage through an external resistor divider tied to the FB pin and servos the V_C pin. If the error amplifier's output increases, more current is delivered to the output; if it decreases, less current is delivered. An active clamp on the V_C pin provides current limit. The V_C pin is also clamped to the voltage on the RUN/SS pin; soft-start is implemented by generating a voltage ramp at the RUN/SS pin using an external resistor and capacitor.

An internal regulator provides power to the control circuitry. The bias regulator normally draws power from the V_{IN} pin, but if the BD pin is connected to an external voltage higher than 3V bias power will be drawn from the external source (typically the regulated output voltage). This improves efficiency. The RUN/SS pin is used to place the LT3972 in shutdown, disconnecting the output and reducing the input current to less than 0.5µA.

The switch driver operates from either the input or from the BOOST pin. An external capacitor and diode are used to generate a voltage at the BOOST pin that is higher than the input supply. This allows the driver to fully saturate the internal bipolar NPN power switch for efficient operation.

To further optimize efficiency, the LT3972 automatically switches to Burst Mode operation in light load situations. Between bursts, all circuitry associated with controlling the output switch is shut down, reducing the input supply current to 75µA in a typical application.

The oscillator reduces the LT3972's operating frequency when the voltage at the FB pin is low. This frequency foldback helps to control the output current during start-up and overload.

The LT3972 contains a power good comparator which trips when the FB pin is at 91% of its regulated value. The PG output is an open-collector transistor that is off when the output is in regulation, allowing an external resistor to pull the PG pin high. Power good is valid when the LT3972 is enabled and V_{IN} is above 3.6V.

The LT3972 has an overvoltage protection feature which disables switching action when the V_{IN} goes above 35V typical (33V minimum). When switching is disabled, the LT3972 can safely sustain input voltages up to 62V.

APPLICATIONS INFORMATION

FB Resistor Network

The output voltage is programmed with a resistor divider between the output and the FB pin. Choose the 1% resistors according to:

$$R1 = R2\left(\frac{V_{OUT}}{0.79V} - 1\right)$$

Reference designators refer to the Block Diagram.

Setting the Switching Frequency

The LT3972 uses a constant frequency PWM architecture that can be programmed to switch from 200kHz to 2.4MHz by using a resistor tied from the RT pin to ground. A table showing the necessary R_T value for a desired switching frequency is in Figure 1.

SWITCHING FREQUENCY (MHz)	R_T VALUE (kΩ)
0.2	215
0.3	140
0.4	100
0.5	78.7
0.6	63.4
0.7	53.6
0.8	45.3
0.9	39.2
1.0	34
1.2	26.7
1.4	22.1
1.6	18.2
1.8	15
2.0	12.7
2.2	10.7
2.4	9.09

Figure 1. Switching Frequency vs R_T Value

Operating Frequency Trade-Offs

Selection of the operating frequency is a trade-off between efficiency, component size, minimum dropout voltage, and maximum input voltage. The advantage of high frequency operation is that smaller inductor and capacitor values may be used. The disadvantages are lower efficiency, lower maximum input voltage, and higher dropout voltage. The highest acceptable switching frequency ($f_{SW(MAX)}$) for a given application can be calculated as follows:

$$f_{SW(MAX)} = \frac{V_D + V_{OUT}}{t_{ON(MIN)}\left(V_D + V_{IN} - V_{SW}\right)}$$

where V_{IN} is the typical input voltage, V_{OUT} is the output voltage, V_D is the catch diode drop (~0.5V) and V_{SW} is the internal switch drop (~0.5V at max load). This equation shows that slower switching frequency is necessary to safely accommodate high V_{IN}/V_{OUT} ratio. Also, as shown in the next section, lower frequency allows a lower dropout voltage. The reason input voltage range depends on the switching frequency is because the LT3972 switch has finite minimum on and off times. The switch can turn on for a minimum of ~150ns and turn off for a minimum of ~150ns. Typical minimum on-time at 25°C is 80ns. This means that the minimum and maximum duty cycles are:

$$DC_{MIN} = f_{SW}t_{ON(MIN)}$$

$$DC_{MAX} = 1 - f_{SW}t_{OFF(MIN)}$$

where f_{SW} is the switching frequency, the $t_{ON(MIN)}$ is the minimum switch on-time (~150ns), and the $t_{OFF(MIN)}$ is the minimum switch off-time (~150ns). These equations show that duty cycle range increases when switching frequency is decreased.

A good choice of switching frequency should allow adequate input voltage range (see next section) and keep the inductor and capacitor values small.

Input Voltage Range

The maximum input voltage for LT3972 applications depends on switching frequency, Absolute Maximum Ratings of the V_{IN} and BOOST pins, and the operating mode.

The LT3972 can operate from input voltages of up to 33V, and withstand voltages up to 62V. Note that while V_{IN} is above 35V typical (33V minimum and 37V maximum) the part will keep the switch off and the output will not be in regulation.

To safely allow inputs of up to 62V, be sure to choose a Schottky diode, inductor size, and switching frequency to allow safe operation at 37V according to the following discussions.

While the output is in start-up, short-circuit, or other overload conditions, the switching frequency should be chosen according to the following equation:

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$$V_{IN(MAX)} = \frac{V_{OUT} + V_D}{f_{SW} t_{ON(MIN)}} - V_D + V_{SW}$$

where $V_{IN(MAX)}$ is the maximum operating input voltage, V_{OUT} is the output voltage, V_D is the catch diode drop (~0.5V), V_{SW} is the internal switch drop (~0.5V at max load), f_{SW} is the switching frequency (set by R_T), and $t_{ON(MIN)}$ is the minimum switch on-time (~100ns). Note that a higher switching frequency will depress the maximum operating input voltage. Conversely, a lower switching frequency will be necessary to achieve safe operation at high input voltages.

If the output is in regulation and no short-circuit, start-up, or overload events are expected, then input voltage transients of up to 33V are acceptable regardless of the switching frequency. In this mode, the LT3972 may enter pulse-skipping operation where some switching pulses are skipped to maintain output regulation. In this mode the output voltage ripple and inductor current ripple will be higher than in normal operation.

The minimum input voltage is determined by either the LT3972's minimum operating voltage of ~3.6V or by its maximum duty cycle (see equation in previous section). The minimum input voltage due to duty cycle is:

$$V_{IN(MIN)} = \frac{V_{OUT} + V_D}{1 - f_{SW} t_{OFF(MIN)}} - V_D + V_{SW}$$

where $V_{IN(MIN)}$ is the minimum input voltage, and $t_{OFF(MIN)}$ is the minimum switch off-time (150ns). Note that higher switching frequency will increase the minimum input voltage. If a lower dropout voltage is desired, a lower switching frequency should be used.

Inductor Selection

For a given input and output voltage, the inductor value and switching frequency will determine the ripple current. The ripple current ΔI_L increases with higher V_{IN} or V_{OUT} and decreases with higher inductance and faster switching frequency. A reasonable starting point for selecting the ripple current is:

$$\Delta I_L = 0.4(I_{OUT(MAX)})$$

where $I_{OUT(MAX)}$ is the maximum output load current. To guarantee sufficient output current, peak inductor current must be lower than the LT3972's switch current limit (I_{LIM}). The peak inductor current is:

$$I_{L(PEAK)} = I_{OUT(MAX)} + \Delta I_L/2$$

where $I_{L(PEAK)}$ is the peak inductor current, $I_{OUT(MAX)}$ is the maximum output load current, and ΔI_L is the inductor ripple current. The LT3972's switch current limit (I_{LIM}) is 5.5A at low duty cycles and decreases linearly to 4.5A at DC = 0.8. The maximum output current is a function of the inductor ripple current:

$$I_{OUT(MAX)} = I_{LIM} - \Delta I_L/2$$

Be sure to pick an inductor ripple current that provides sufficient maximum output current ($I_{OUT(MAX)}$).

The largest inductor ripple current occurs at the highest V_{IN}. To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation:

$$L = \left(\frac{V_{OUT} + V_D}{f_{SW} \Delta I_L}\right)\left(1 - \frac{V_{OUT} + V_D}{V_{IN(MAX)}}\right)$$

where V_D is the voltage drop of the catch diode (~0.4V), $V_{IN(MAX)}$ is the maximum input voltage, V_{OUT} is the output voltage, f_{SW} is the switching frequency (set by RT), and L is in the inductor value.

The inductor's RMS current rating must be greater than the maximum load current and its saturation current should be about 30% higher. For robust operation in fault conditions (start-up or short circuit) and high input voltage (>30V), the saturation current should be above 5A. To keep the efficiency high, the series resistance (DCR) should be less than 0.1Ω, and the core material should be intended for high frequency applications. Table 1 lists several vendors and suitable types.

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Table 1. Inductor Vendors

VENDOR	URL	PART SERIES	TYPE
Murata	www.murata.com	LQH55D	Open
TDK	www.componenttdk.com	SLF10145	Shielded
Toko	www.toko.com	D75C D75F	Shielded Open
Sumida	www.sumida.com	CDRH74 CR75 CDRH8D43	Shielded Open Shielded
NEC	www.nec.com	MPLC073 MPBI0755	Shielded Shielded

Of course, such a simple design guide will not always result in the optimum inductor for your application. A larger value inductor provides a slightly higher maximum load current and will reduce the output voltage ripple. If your load is lower than 3.5A, then you can decrease the value of the inductor and operate with higher ripple current. This allows you to use a physically smaller inductor, or one with a lower DCR resulting in higher efficiency. There are several graphs in the Typical Performance Characteristics section of this data sheet that show the maximum load current as a function of input voltage and inductor value for several popular output voltages. Low inductance may result in discontinuous mode operation, which is okay but further reduces maximum load current. For details of maximum output current and discontinuous mode operation, see Linear Technology Application Note 44. Finally, for duty cycles greater than 50% ($V_{OUT}/V_{IN} > 0.5$), there is a minimum inductance required to avoid subharmonic oscillations. See AN19.

Input Capacitor

Bypass the input of the LT3972 circuit with a ceramic capacitor of X7R or X5R type. Y5V types have poor performance over temperature and applied voltage, and should not be used. A 10µF to 22µF ceramic capacitor is adequate to bypass the LT3972 and will easily handle the ripple current. Note that larger input capacitance is required when a lower switching frequency is used. If the input power source has high impedance, or there is significant inductance due to long wires or cables, additional bulk capacitance may be necessary. This can be provided with a lower performance electrolytic capacitor.

Step-down regulators draw current from the input supply in pulses with very fast rise and fall times. The input capacitor is required to reduce the resulting voltage ripple at the LT3972 and to force this very high frequency switching current into a tight local loop, minimizing EMI. A 10µF capacitor is capable of this task, but only if it is placed close to the LT3972 and the catch diode (see the PCB Layout section). A second precaution regarding the ceramic input capacitor concerns the maximum input voltage rating of the LT3972. A ceramic input capacitor combined with trace or cable inductance forms a high quality (under damped) tank circuit. If the LT3972 circuit is plugged into a live supply, the input voltage can ring to twice its nominal value, possibly exceeding the LT3972's voltage rating. This situation is easily avoided (see the Hot Plugging Safety section).

For space sensitive applications, a 4.7µF ceramic capacitor can be used for local bypassing of the LT3972 input. However, the lower input capacitance will result in increased input current ripple and input voltage ripple, and may couple noise into other circuitry. Also, the increased voltage ripple will raise the minimum operating voltage of the LT3972 to ~3.7V.

Output Capacitor and Output Ripple

The output capacitor has two essential functions. Along with the inductor, it filters the square wave generated by the LT3972 to produce the DC output. In this role it determines the output ripple, and low impedance at the switching frequency is important. The second function is to store energy in order to satisfy transient loads and stabilize the LT3972's control loop. Ceramic capacitors have very low equivalent series resistance (ESR) and provide the best ripple performance. A good starting value is:

$$C_{OUT} = \frac{100}{V_{OUT} f_{SW}}$$

where f_{SW} is in MHz, and C_{OUT} is the recommended output capacitance in µF. Use X5R or X7R types. This choice will provide low output ripple and good transient response. Transient performance can be improved with a higher value capacitor if the compensation network is also adjusted to maintain the loop bandwidth. A lower

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Table 2. Capacitor Vendors

VENDOR	PHONE	URL	PART SERIES	COMMANDS
Panasonic	(714) 373-7366	www.panasonic.com	Ceramic, Polymer, Tantalum	EEF Series
Kemet	(864) 963-6300	www.kemet.com	Ceramic, Tantalum	T494, T495
Sanyo	(408) 749-9714	www.sanyovideo.com	Ceramic, Polymer, Tantalum	POSCAP
Murata	(408) 436-1300	www.murata.com	Ceramic	
AVX		www.avxcorp.com	Ceramic, Tantalum	TPS Series
Taiyo Yuden	(864) 963-6300	www.taiyo-yuden.com	Ceramic	

value of output capacitor can be used to save space and cost but transient performance will suffer. See the Frequency Compensation section to choose an appropriate compensation network.

When choosing a capacitor, look carefully through the data sheet to find out what the actual capacitance is under operating conditions (applied voltage and temperature). A physically larger capacitor, or one with a higher voltage rating, may be required. High performance tantalum or electrolytic capacitors can be used for the output capacitor. Low ESR is important, so choose one that is intended for use in switching regulators. The ESR should be specified by the supplier, and should be 0.05Ω or less. Such a capacitor will be larger than a ceramic capacitor and will have a larger capacitance, because the capacitor must be large to achieve low ESR. Table 2 lists several capacitor vendors.

Catch Diode

The catch diode conducts current only during switch off -time. Average forward current in normal operation can be calculated from:

$$I_{D(AVG)} = I_{OUT} (V_{IN} – V_{OUT})/V_{IN}$$

where I_{OUT} is the output load current. The only reason to consider a diode with a larger current rating than necessary for nominal operation is for the worst-case condition of shorted output. The diode current will then increase to the typical peak switch current. Peak reverse voltage is equal to the regulator input voltage. Use a Schottky diode with a reverse-voltage rating greater than the input voltage. The overvoltage protection feature in the LT3972 will keep the switch off when V_{IN} > 35V which allows the use of 40V rated Schottky even when V_{IN} ranges up to 62V. Table 3 lists several Schottky diodes and their manufacturers.

Table 3. Diode Vendors

PART NUMBER	V_R (V)	I_{AVE} (A)	V_F AT 3A (mV)
On Semiconductor			
MBRA340	40	3	500
Diodes Inc.			
PDS340	40	3	500
B340A	40	3	500
B340LA	40	3	450

Ceramic Capacitors

Ceramic capacitors are small, robust and have very low ESR. However, ceramic capacitors can cause problems when used with the LT3972 due to their piezoelectric nature. When in Burst Mode operation, the LT3972's switching frequency depends on the load current, and at very light loads the LT3972 can excite the ceramic capacitor at audio frequencies, generating audible noise. Since the LT3972 operates at a lower current limit during Burst Mode operation, the noise is nearly silent to a casual ear. If this is unacceptable, use a high performance tantalum or electrolytic capacitor at the output.

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Frequency Compensation

The LT3972 uses current mode control to regulate the output. This simplifies loop compensation. In particular, the LT3972 does not require the ESR of the output capacitor for stability, so you are free to use ceramic capacitors to achieve low output ripple and small circuit size. Frequency compensation is provided by the components tied to the V_C pin, as shown in Figure 2. Generally a capacitor (C_C) and a resistor (R_C) in series to ground are used. In addition, there may be lower value capacitor in parallel. This capacitor (C_F) is not part of the loop compensation but is used to filter noise at the switching frequency, and is required only if a phase-lead capacitor is used or if the output capacitor has high ESR.

Loop compensation determines the stability and transient performance. Designing the compensation network is a bit complicated and the best values depend on the application and in particular the type of output capacitor. A practical approach is to start with one of the circuits in this data sheet that is similar to your application and tune the compensation network to optimize the performance. Stability should then be checked across all operating conditions, including load current, input voltage and temperature. The LT1375 data sheet contains a more thorough discussion of loop compensation and describes how to test the stability using a transient load. Figure 2 shows an equivalent circuit for the LT3972 control loop. The error amplifier is a transconductance amplifier with finite output impedance. The power section, consisting of the modulator, power switch and inductor, is modeled as a transconductance amplifier generating an output current proportional to the voltage at the V_C pin. Note that the output capacitor integrates this current, and that the capacitor on the V_C pin (C_C) integrates the error amplifier output current, resulting in two poles in the loop. In most cases a zero is required and comes from either the output capacitor ESR or from a resistor, R_C, in series with C_C. This simple model works well as long as the value of the inductor is not too high and the loop crossover frequency is much lower than the switching frequency. A phase lead capacitor (C_{PL}) across the feedback divider may improve the transient response. Figure 3 shows the transient response when the load current is stepped from 1A to 3A and back to 1A.

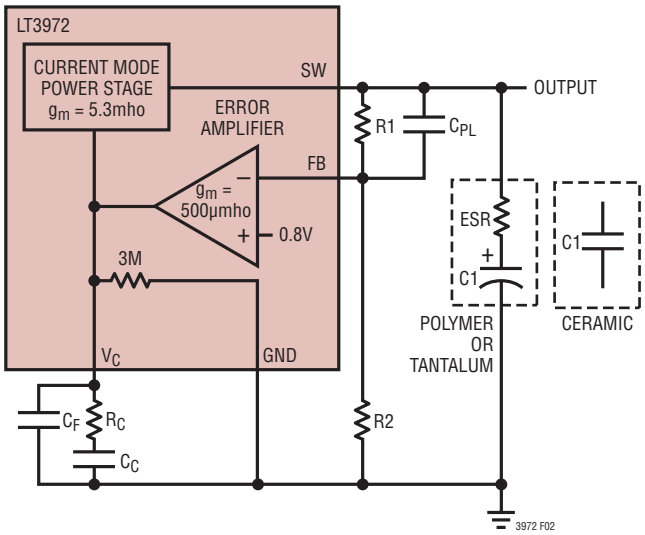


Figure 2. Model for Loop Response

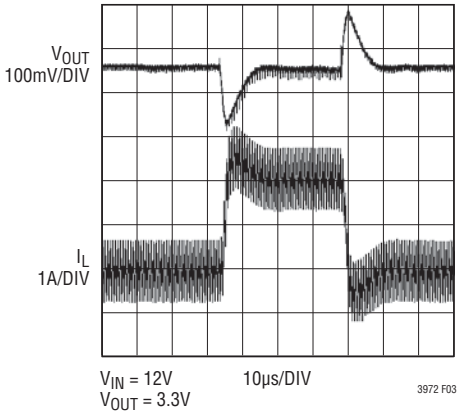


Figure 3. Transient Load Response of the LT3972 Front Page Application as the Load Current is Stepped from 1A to 3A. V_{OUT} = 5V

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Low Ripple Burst Mode Operation and Pulse-Skipping Mode

The LT3972 is capable of operating in either low ripple Burst Mode operation or pulse-skipping mode which are selected using the SYNC pin. See the Synchronization section for details.

To enhance efficiency at light loads, the LT3972 can be operated in low ripple Burst Mode operation which keeps the output capacitor charged to the proper voltage while minimizing the input quiescent current. During Burst Mode operation, the LT3972 delivers single cycle bursts of current to the output capacitor followed by sleep periods where the output power is delivered to the load by the output capacitor. Because the LT3972 delivers power to the output with single, low current pulses, the output ripple is kept below 15mV for a typical application. In addition, V_{IN} and BD quiescent currents are reduced to typically 30µA and 90µA respectively during the sleep time. As the load current decreases towards a no-load condition, the percentage of time that the LT3972 operates in sleep mode increases and the average input current is greatly reduced resulting in high efficiency even at very low loads. See Figure 4. At higher output loads (above 140mA for the front page application) the LT3972 will be running at the frequency programmed by the R_T resistor, and will be operating in standard PWM mode. The transition between PWM and low ripple Burst Mode operation is seamless, and will not disturb the output voltage.

If low quiescent current is not required the LT3972 can operate in pulse-skipping mode. The benefit of this mode is that the LT3972 will enter full frequency standard PWM operation at a lower output load current than when in Burst Mode operation. The front page application circuit will switch at full frequency at output loads higher than about 60mA. Select pulse-skipping mode by applying a clock signal or a DC voltage higher than 0.9V to the SYNC pin.

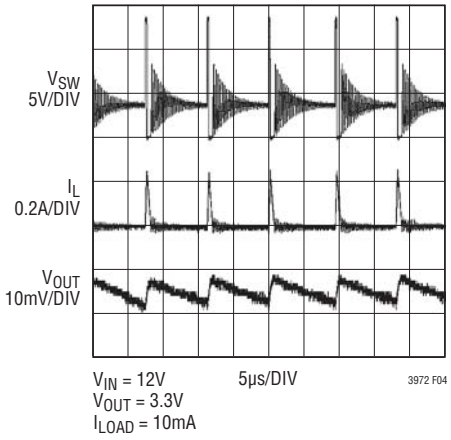


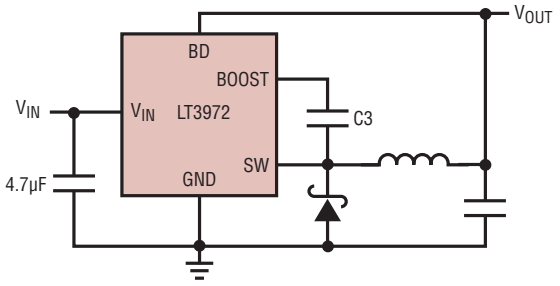
Figure 4. Burst Mode Operation

BOOST and BIAS Pin Considerations

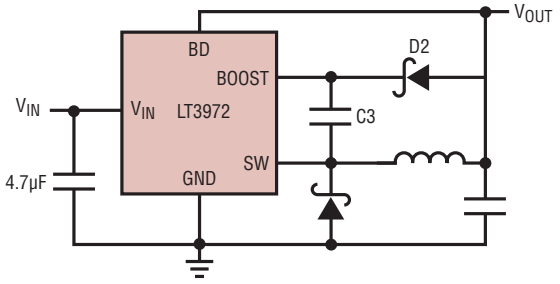
Capacitor C3 and the internal boost Schottky diode (see the Block Diagram) are used to generate a boost voltage that is higher than the input voltage. In most cases a 0.22µF capacitor will work well. Figure 2 shows three ways to arrange the boost circuit. The BOOST pin must be more than 2.3V above the SW pin for best efficiency. For outputs of 3V and above, the standard circuit (Figure 5a) is best. For outputs between 2.8V and 3V, use a 1µF boost capacitor. A 2.5V output presents a special case because it is marginally adequate to support the boosted drive stage while using the internal boost diode. For reliable BOOST pin operation with 2.5V outputs use a good external Schottky diode (such as the ON Semi MBR0540), and a 1µF boost capacitor (see Figure 5b). For lower output voltages the boost diode can be tied to the input (Figure 5c), or to another supply greater than 2.8V. Tying BD to V_{IN} reduces the maximum input voltage to 28V. The circuit in Figure 5a is more efficient because the BOOST pin current and BD pin quiescent current comes from a lower voltage source. You must also be sure that the maximum voltage ratings of the BOOST and BD pins are not exceeded.

The minimum operating voltage of an LT3972 application is limited by the minimum input voltage (3.6V) and by the maximum duty cycle as outlined in a previous section. For proper start-up, the minimum input voltage is also limited by the boost circuit. If the input voltage is ramped slowly, or the LT3972 is turned on with its RUN/SS pin when the output is already in regulation, then the boost capacitor may not be fully charged. Because the boost capacitor is charged with the energy stored in the inductor, the circuit will rely on some minimum load current to get the boost circuit running properly. This minimum load will depend on input and output voltages, and on the arrangement of the boost circuit. The minimum load generally goes to zero once the circuit has started. Figure 6 shows a plot

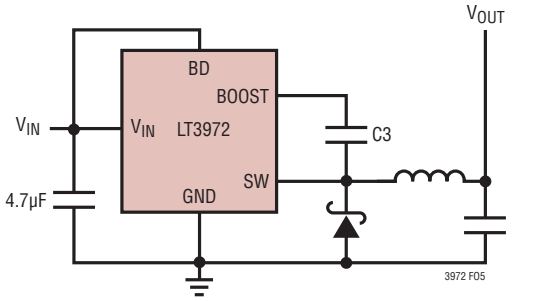
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(5a) For V_{OUT} > 2.8V



(5b) For 2.5V < V_{OUT} < 2.8V



(5c) For V_{OUT} < 2.5V; $V_{IN(MAX)}$ = 30V

Figure 5. Three Circuits For Generating The Boost Voltage

of minimum load to start and to run as a function of input voltage. In many cases the discharged output capacitor will present a load to the switcher, which will allow it to start. The plots show the worst-case situation where V_{IN} is ramping very slowly. For lower start-up voltage, the boost diode can be tied to V_{IN}; however, this restricts the input range to one-half of the absolute maximum rating of the BOOST pin.

At light loads, the inductor current becomes discontinuous and the effective duty cycle can be very high. This reduces the minimum input voltage to approximately 300mV above V_{OUT}. At higher load currents, the inductor

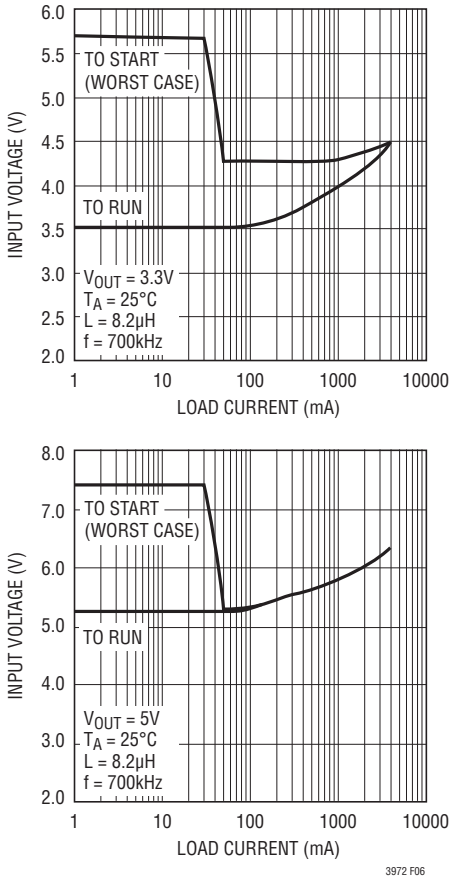


Figure 6. The Minimum Input Voltage Depends on Output Voltage, Load Current and Boost Circuit

current is continuous and the duty cycle is limited by the maximum duty cycle of the LT3972, requiring a higher input voltage to maintain regulation.

Soft-Start

The RUN/SS pin can be used to soft-start the LT3972, reducing the maximum input current during start-up. The RUN/SS pin is driven through an external RC filter to create a voltage ramp at this pin. Figure 7 shows the start-up and shutdown waveforms with the soft-start circuit. By choosing a large RC time constant, the peak start-up current can be reduced to the current that is required to regulate the output, with no overshoot. Choose the value of the resistor so that it can supply 20µA when the RUN/SS pin reaches 2.5V.

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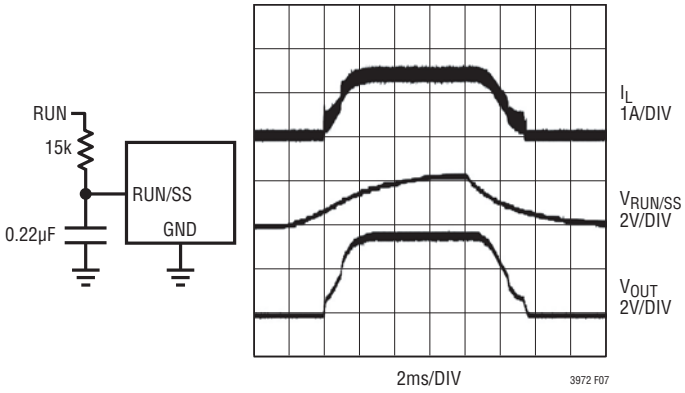


Figure 7. To Soft-Start the LT3972, add a Resisitor and Capacitor to the RUN/SS Pin

Synchronization

To select low ripple Burst Mode operation, tie the SYNC pin below 0.5V (this can be ground or a logic output).

Synchronizing the LT3972 oscillator to an external frequency can be done by connecting a square wave (with 20% to 80% duty cycle) to the SYNC pin. The square wave amplitude should have valleys that are below 0.3V and peaks that are above 0.8V (up to 6V).

The LT3972 will not enter Burst Mode operation at low output loads while synchronized to an external clock, but instead will skip pulses to maintain regulation.

The LT3972 may be synchronized over a 250kHz to 2MHz range. The R_T resistor should be chosen to set the LT3972 switching frequency 20% below the lowest synchronization input. For example, if the synchronization signal will be 250kHz and higher, the R_T should be chosen for 200kHz. To assure reliable and safe operation, the LT3972 will only synchronize when the output voltage is near regulation as indicated by the PG flag. It is therefore necessary to choose a large enough inductor value to supply the required output current at the frequency set by the R_T resistor. See the Inductor Selection section. It is also important to note that slope compensation is set by the R_T value: When the sync frequency is much higher than the one set by R_T, the slope compensation will be significantly reduced which may require a larger inductor value to prevent subharmonic oscillation.

Shorted and Reversed-Input Protection

If the inductor is chosen so that it won't saturate excessively, an LT3972 buck regulator will tolerate a shorted output. There is another situation to consider in systems where the output will be held high when the input to the LT3972 is absent. This may occur in battery charging applications or in battery backup systems where a battery or some other supply is diode ORed with the LT3972's output. If the V_{IN} pin is allowed to float and the RUN/SS pin is held high (either by a logic signal or because it is tied to V_{IN}), then the LT3972's internal circuitry will pull its quiescent current through its SW pin. This is fine if your system can tolerate a few mA in this state. If you ground the RUN/SS pin, the SW pin current will drop to essentially zero. However, if the V_{IN} pin is grounded while the output is held high, then parasitic diodes inside the LT3972 can pull large currents from the output through the SW pin and the V_{IN} pin. Figure 8 shows a circuit that will run only when the input voltage is present and that protects against a shorted or reversed input.

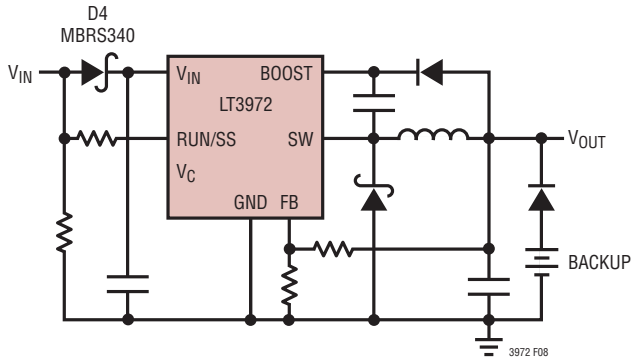


Figure 8. Diode D4 Prevents a Shorted Input from Discharging a Backup Battery Tied to the Output. It Also Protects the Circuit from a Reversed Input. The LT3972 Runs Only When the Input is Present

PCB Layout

For proper operation and minimum EMI, care must be taken during printed circuit board layout. Figure 9 shows the recommended component placement with trace, ground plane and via locations. Note that large, switched currents flow in the LT3972's V_{IN} and SW pins, the catch

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diode (D1) and the input capacitor (C1). The loop formed by these components should be as small as possible. These components, along with the inductor and output capacitor, should be placed on the same side of the circuit board, and their connections should be made on that layer. Place a local, unbroken ground plane below these components. The SW and BOOST nodes should be as small as possible. Finally, keep the FB and V_C nodes small so that the ground traces will shield them from the SW and BOOST nodes. The Exposed Pad on the bottom of the package must be soldered to ground so that the pad acts as a heat sink. To keep thermal resistance low, extend the ground plane as much as possible, and add thermal vias under and near the LT3972 to additional ground planes within the circuit board and on the bottom side.

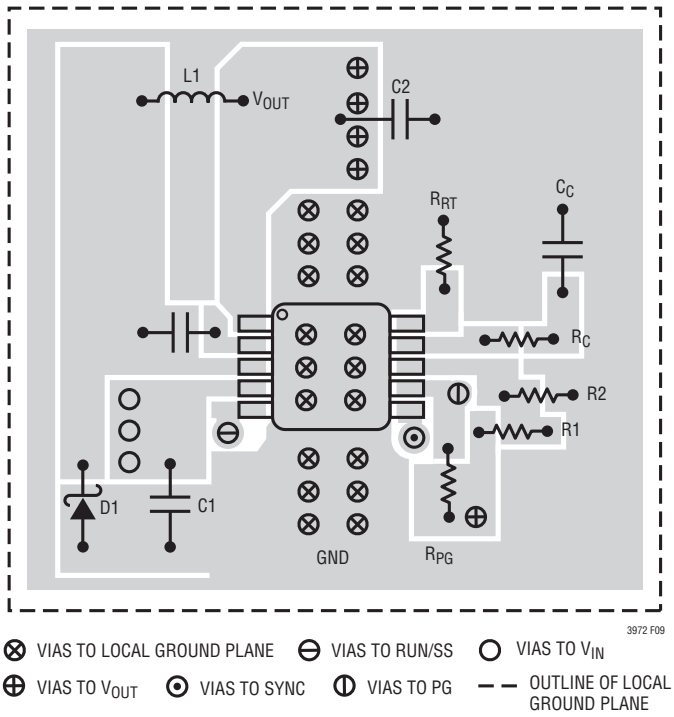


Figure 9. A Good PCB Layout Ensures Proper, Low EMI Operation

Hot Plugging Safely

The small size, robustness and low impedance of ceramic capacitors make them an attractive option for the input bypass capacitor of LT3972 circuits. However, these capacitors can cause problems if the LT3972 is plugged into a live supply (see Linear Technology Application Note 88 for a complete discussion). The low loss ceramic capacitor, combined with stray inductance in series with the power source, forms an under damped tank circuit, and the voltage at the V_{IN} pin of the LT3972 can ring to twice the nominal input voltage, possibly exceeding the LT3972's rating and damaging the part. If the input supply is poorly controlled or the user will be plugging the LT3972 into an energized supply, the input network should be designed to prevent this overshoot. Figure 10 shows the waveforms that result when an LT3972 circuit is connected to a 24V supply through six feet of 24-gauge twisted pair. The first plot is the response with a 4.7µF ceramic capacitor at the input. The input voltage rings as high as 50V and the input current peaks at 26A. A good solution is shown in Figure 10b. A 0.7Ω resistor is added in series with the input to eliminate the voltage overshoot (it also reduces the peak input current). A 0.1µF capacitor improves high frequency filtering. For high input voltages its impact on efficiency is minor, reducing efficiency by 1.5 percent for a 5V output at full load operating from 24V.

High Temperature Considerations

The PCB must provide heat sinking to keep the LT3972 cool. The Exposed Pad on the bottom of the package must be soldered to a ground plane. This ground should be tied to large copper layers below with thermal vias; these layers will spread the heat dissipated by the LT3972. Place additional vias can reduce thermal resistance further. With these steps, the thermal resistance from die (or junction)

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to ambient can be reduced to θ_{JA} = 35°C/W or less. With 100 LFPM airflow, this resistance can fall by another 25%. Further increases in airflow will lead to lower thermal resistance. Because of the large output current capability of the LT3972, it is possible to dissipate enough heat to raise the junction temperature beyond the absolute maximum of 125°C. When operating at high ambient temperatures, the maximum load current should be derated as the ambient temperature approaches 125°C.

Power dissipation within the LT3972 can be estimated by calculating the total power loss from an efficiency measurement and subtracting the catch diode loss and inductor loss. The die temperature is calculated by multiplying the LT3972 power dissipation by the thermal resistance from junction to ambient.

Other Linear Technology Publications

Application Notes 19, 35 and 44 contain more detailed descriptions and design information for buck regulators and other switching regulators. The LT1376 data sheet has a more extensive discussion of output ripple, loop compensation and stability testing. Design Note 100 shows how to generate a bipolar output supply using a buck regulator.

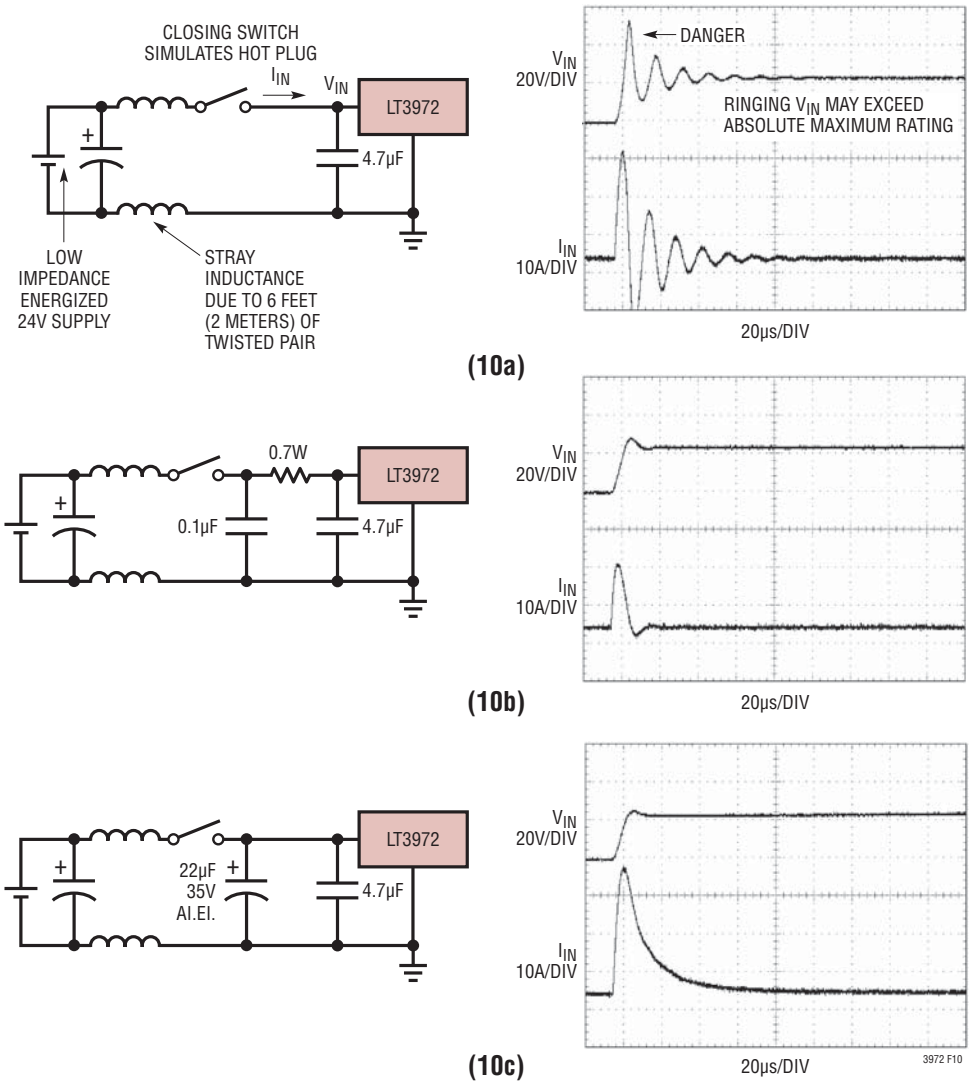
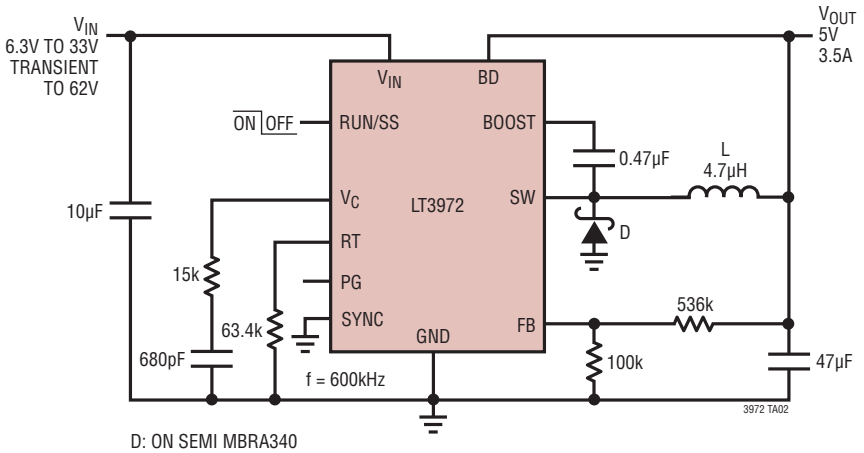


Figure 10. A Well Chosen Input Network Prevents Input Voltage Overshoot and Ensures Reliable Operation when the LT3972 is Connected to a Live Supply

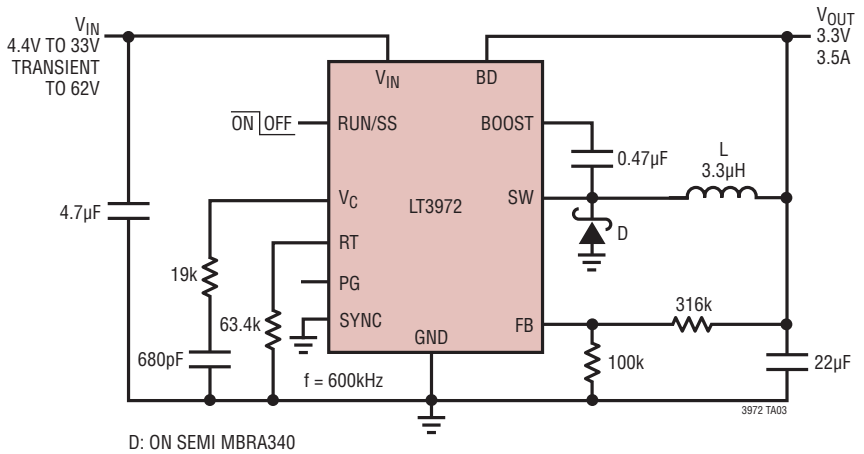
TYPICAL APPLICATIONS

5V Step-Down Converter



D: ON SEMI MBRA340
L: NEC MPLC0730L4R7

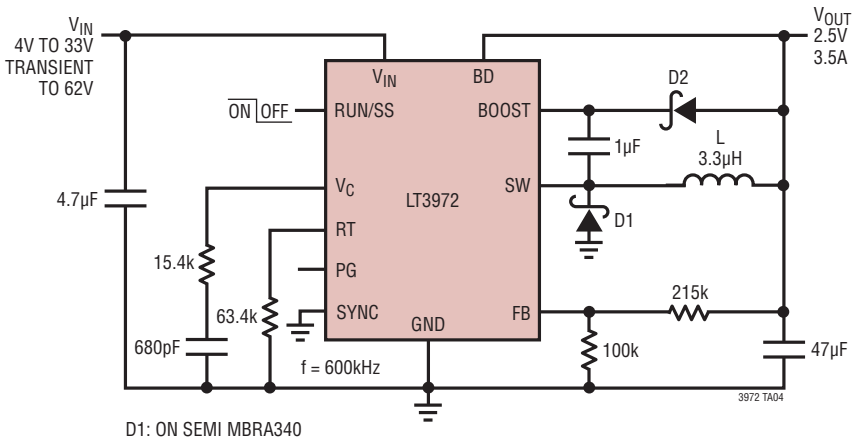
3.3V Step-Down Converter



D: ON SEMI MBRA340
L: NEC MPLC0730L3R3

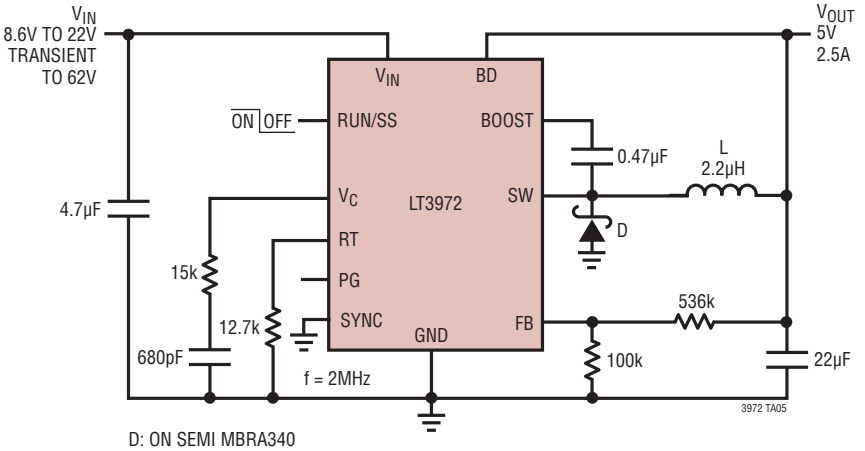
TYPICAL APPLICATIONS

2.5V Step-Down Converter



D1: ON SEMI MBRA340
D2: MBR0540
L: NEC MPLC0730L3R3

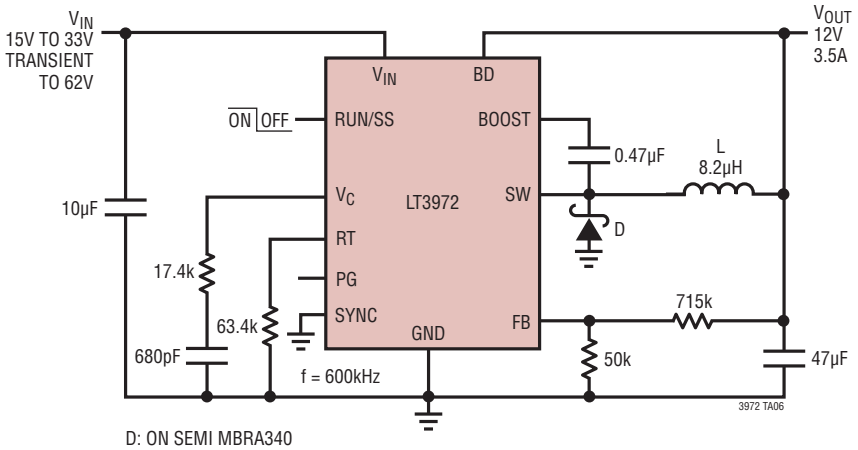
5V, 2MHz Step-Down Converter



D: ON SEMI MBRA340
L: NEC MPLC0730L2R2

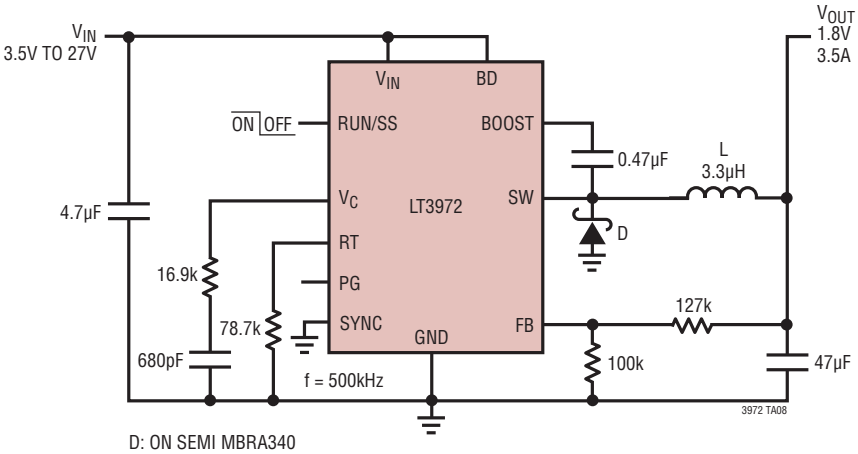
TYPICAL APPLICATIONS

12V Step-Down Converter



D: ON SEMI MBRA340
L: NEC MBP107558R2P

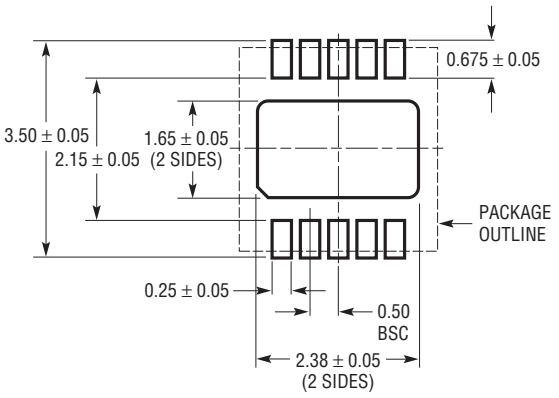
1.8V Step-Down Converter



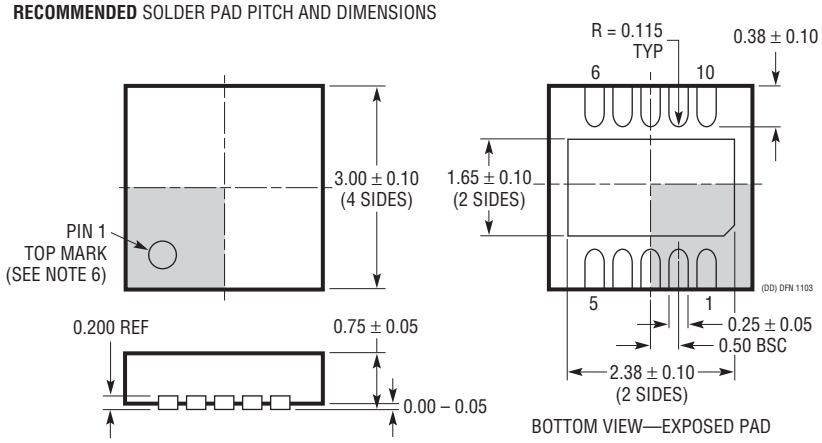
D: ON SEMI MBRA340
L: NEC MPLC0730L3R3

PACKAGE DESCRIPTION

DD Package
10-Lead Plastic DFN (3mm × 3mm)
(Reference LTC DWG # 05-08-1699)



RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS

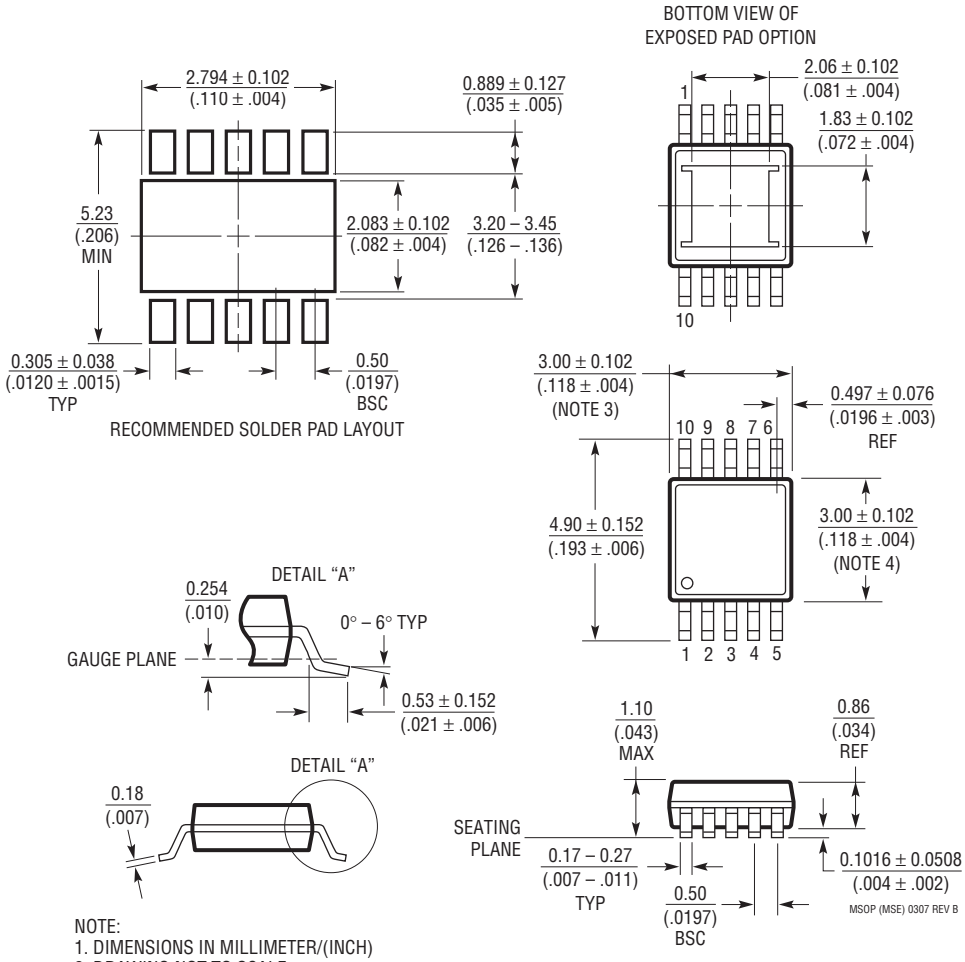


BOTTOM VIEW—EXPOSED PAD

NOTE:
1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE M0-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

PACKAGE DESCRIPTION

MSE Package
10-Lead Plastic MSOP, Exposed Die Pad
(Reference LTC DWG # 05-08-1664 Rev B)

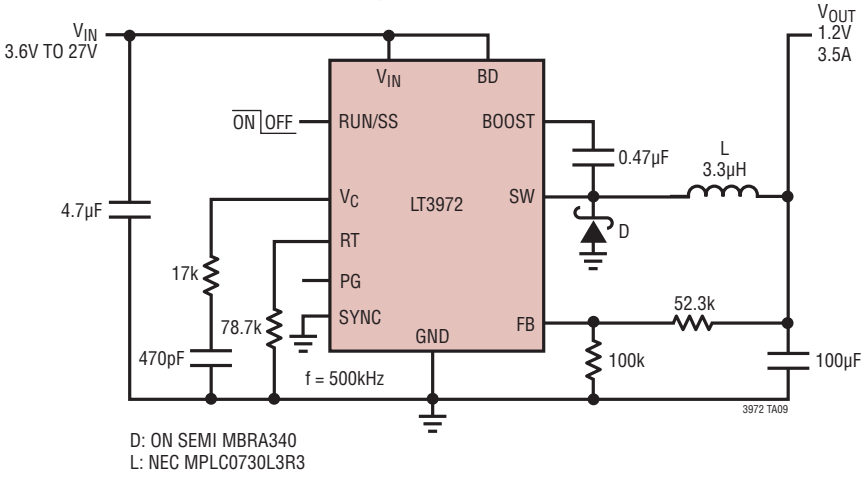


NOTE:
1. DIMENSIONS IN MILLIMETER/(INCH)
2. DRAWING NOT TO SCALE
3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
   MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
   INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

Information furnished by Linear Technology Corporation is believed to be accurate and reliable. However, no responsibility is assumed for its use. Linear Technology Corporation makes no representation that the interconnection of its circuits as described herein will not infringe on existing patent rights.

TYPICAL APPLICATION

1.2V Step-Down Converter



D: ON SEMI MBRA340
L: NEC MPLC0730L3R3

RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1933	500mA (I_{OUT}), 500kHz Step-Down Switching Regulator in SOT-23	V_{IN}: 3.6V to 36V, $V_{OUT(MIN)}$ = 1.2V, I_Q = 1.6mA, I_{SD} < 1µA, ThinSOT™ Package
LT1936	36V, 1.4A (I_{OUT}), 500kHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 36V, $V_{OUT(MIN)}$ = 1.2V, I_Q = 1.9mA, I_{SD} < 1µA, MS8E Package
LT1940	Dual 25V, 1.4A (I_{OUT}), 1.1MHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 25V, $V_{OUT(MIN)}$ = 1.2V, I_Q = 3.8mA, I_{SD} < 30µA, TSSOP16E Package
LT1976/LT1967	60V, 1.2A (I_{OUT}), 200kHz/500kHz, High Efficiency Step-Down DC/DC Converters with Burst Mode Operation	V_{IN}: 3.3V to 60V, $V_{OUT(MIN)}$ = 1.2V, I_Q = 100µA, I_{SD} < 1µA, TSSOP16E Package
LT3434/LT3435	60V, 2.4A (I_{OUT}), 200kHz/500kHz, High Efficiency Step-Down DC/DC Converters with Burst Mode Operation	V_{IN}: 3.3V to 60V, $V_{OUT(MIN)}$ = 1.2V, I_Q = 100µA, I_{SD} < 1µA, TSSOP16 Package
LT3437	60V, 400mA (I_{OUT}), Micropower Step-Down DC/DC Converter with Burst Mode Operation	V_{IN}: 3.3V to 60V, $V_{OUT(MIN)}$ = 1.25V, I_Q = 100µA, I_{SD} < 1µA, 3mm × 3mm DFN10 and TSSOP16E Packages
LT3480	36V with Transient Protection to 60V, 2A (I_{OUT}), 2.4MHz, High Efficiency Step-Down DC/DC Converter with Burst Mode Operation	V_{IN}: 3.6V to 38V, $V_{OUT(MIN)}$ = 0.78V, I_Q = 70µA, I_{SD} < 1µA, 3mm × 3mm DFN10 and MSOP10E Packages
LT3481	34V with Transient Protection to 36V, 2A (I_{OUT}), 2.8MHz, High Efficiency Step-Down DC/DC Converter with Burst Mode Operation	V_{IN}: 3.6V to 34V, $V_{OUT(MIN)}$ = 1.26V, I_Q = 50µA, I_{SD} < 1µA, 3mm × 3mm DFN10 and MSOP10E Packages
LT3493	36V, 1.4A (I_{OUT}), 750kHz High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 36V, $V_{OUT(MIN)}$ = 0.8V, I_Q = 1.9mA, I_{SD} < 1µA, 2mm × 3mm DFN6 Package
LT3505	36V with Transient Protection to 40V, 1.4A (I_{OUT}), 3MHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 34V, $V_{OUT(MIN)}$ = 0.78V, I_Q = 2mA, I_{SD} = 2µA, 3mm × 3mm DFN8 and MSOP8E Packages
LT3508	36V with Transient Protection to 40V, Dual 1.4A (I_{OUT}), 3MHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.7V to 37V, $V_{OUT(MIN)}$ = 0.8V, I_Q = 4.6mA, I_{SD} = 1µA, 4mm × 4mm QFN24 and TSSOP16E Packages
LT3680	36V, 3.5A, 2.4MHz, Low Quiescent Current (<75µA) Step-Down DC/DC Converter	V_{IN}: 3.6V to 36V, $V_{OUT(MIN)}$ = 0.8V, I_Q = 75µA, I_{SD} < 1µA, 3mm × 3mm DFN10, MS10E Package
LT3684	34V with Transient Protection to 36V, 2A (I_{OUT}), 2.8MHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 34V, $V_{OUT(MIN)}$ = 1.26V, I_Q = 850µA, I_{SD} < 1µA, 3mm × 3mm DFN10 and MSOP10E Packages
LT3685	36V with Transient Protection to 60V, Dual 2A (I_{OUT}), 2.4MHz, High Efficiency Step-Down DC/DC Converter	V_{IN}: 3.6V to 38V, $V_{OUT(MIN)}$ = 0.78V, I_Q = 70µA, I_{SD} < 1µA, 3mm × 3mm DFN10 and MSOP10E Packages
LT3693	36V, 3.5A, 2.4MHz, Step-Down DC/DC Converter	V_{IN}: 3.6V to 36V, $V_{OUT(MIN)}$ = 0.8V, I_Q = 1.3mA, I_{SD} < 1µA, 3mm × 3mm DFN10, MS10E Package

ThinSOT is a trademark of Linear Technology Corporation.

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