



**THE DATASHEET OF
S29GL032N11FFIV10**



AN-1793 LM3433 4A to 20A LED Driver Evaluation Board

1 Introduction

The LM3433 is an adaptive constant on-time DC/DC buck constant current controller designed to drive a high brightness LEDs (HB LED) at high forward currents. It is a true current source that provides a constant current with constant ripple current regardless of the LED forward voltage drop. The board can accept an input voltage ranging from -9V to -14V w.r.t. GND. The output configuration allows the anodes of multiple LEDs to be tied directly to the ground referenced chassis for maximum heat sink efficacy when a negative input voltage is used.

2 LM3433 Board Description

The evaluation board is designed to provide a constant current in the range of 4A to 20A. The LM3433 requires two input voltages for operation. A positive voltage with respect to GND is required for the bias and control circuitry and a negative voltage with respect to GND is required for the main power input. This allows for the capability of using common anode LEDs so that the anodes can be tied to the ground referenced chassis. The evaluation board only requires one input voltage of -12V with respect to GND. The positive voltage is supplied by the LM5002 circuit. The LM5002 circuit also provides a UVLO function to remove the possibility of the LM3433 from drawing high currents at low input voltages during startup. Initially the output current is set at the minimum of approximately 4A with the POT P1 fully counter-clockwise. To set the desired current level a short may be connected between LED+ and LED-, then use a current probe and turn the POT clockwise until the desired current is reached. PWM dimming FETs are included on-board for testing when the LED can be connected directly next to the board. A shutdown test post on J2, ENA, is included so that startup and shutdown functions can be tested using an external voltage.

3 Setting the LED Current

The LM3433 evaluation board is designed so that the LED current can be set in multiple ways. There is a shunt on J2 initially connecting the ADJ pin to the POT allowing the current to be adjusted using the POT P1. This POT will apply a voltage to the ADJ pin between 0.3V and 1.5V w.r.t. GND to adjust the voltage across the sense resistor (R_{SENSE}) R15. The shunt may also be removed and an external voltage positive w.r.t. GND can then be applied to the ADJ test point on the board. A 5m Ω resistor comes mounted on the board so using the V_{SENSE} vs. V_{ADJ} graph in the [Section 6](#) section the current can be set using [Equation 1](#):

$$I_{\text{LED}} = V_{\text{SENSE}}/R_{\text{SENSE}} \quad (1)$$

Alternatively the shunt can be removed and connect the ADJ test point can be connected to the VINX test point to fix V_{SENSE} at 60mV.

4 PWM Dimming

The LM3433 is capable if high speed PWM dimming in excess of 40kHz. Dimming is accomplished by shorting across the LED with a FET(s). Dimming FETs are included on the evaluation board for testing LEDs placed close to the board. The FETs on the evaluation board should be removed if using dimming FETs remotely placed close to the LED (recommended).

To use the dimming function apply square wave to the PWM test point on the board that has a positive voltage w.r.t. GND. When this pin is pulled high the dimming FET is enabled and the LED turns off. When it is pulled low the dimming FET is turned off and the LED turns on. A scope plot of PWM dimming is included in the *Typical Performance Characteristics* section showing 30kHz dimming at 50% duty cycle.

5 High Current Operation and Component Lifetime

When driving high current LEDs, particularly when PWM dimming, component lifetime may become a factor. In these cases the input ripple current that the input capacitors are required to withstand can become large. At lower currents long life ceramic capacitors may be able to handle this ripple current without a problem. At higher currents more input capacitance may be required. To remain cost effective this may require putting one or more aluminum electrolytic capacitors in parallel with the ceramic input capacitors. Since the operational lifetime of LEDs is very long (up to 50,000 hours) the longevity of an aluminum electrolytic capacitor can become the main factor in the overall system lifetime. The first consideration for selecting the input capacitors is the RMS ripple current they will be required to handle. This current is given by [Equation 2](#):

$$I_{\text{RMS}} = I_{\text{LED}} \frac{\sqrt{V_{\text{LED}}(|V_{\text{EE}}| - V_{\text{LED}})}}{|V_{\text{EE}}|} \quad (2)$$

The parallel combination of the ceramic and aluminum electrolytic input capacitors must be able to handle this ripple current. The aluminum electrolytic in particular should be able to handle the ripple current without a significant rise in core temperature. A good rule of thumb is that if the case temperature of the capacitor is 5°C above the ambient board temperature then the capacitor is not capable of sustaining the ripple current for its full rated lifetime and a more robust or lower ESR capacitor should be selected.

The other main considerations for aluminum electrolytic capacitor lifetime are the rated lifetime and the ambient operating temperature. An aluminum electrolytic capacitor comes with a lifetime rating at a given core temperature, such as 5000 hours at 105°C. As dictated by physics the capacitor lifetime should double for each 7°C below this temperature the capacitor operates at and should halve for each 7°C above this temperature the capacitor operates at. A good quality aluminum electrolytic capacitor will also have a core temperature of approximately 3°C to 5°C above the ambient temperature at rated RMS operating current. So as an example, a capacitor rated for 5,000 hours at 105°C that is operating in an ambient environment of 85°C will have a core temperature of approximately 90°C at full rated RMS operating current. In this case the expected operating lifetime of the capacitor will be approximately just over 20,000 hours. The actual lifetime ($\text{Life}_{\text{ACTUAL}}$) can be found using [Equation 3](#):

$$\text{Life}_{\text{ACTUAL}} = \text{Life}_{\text{RATED}} \times 2^{\left(\frac{T_{\text{CORE}} - T_{\text{ACTUAL}}}{7}\right)} \quad (3)$$

Where $\text{Life}_{\text{RATED}}$ is the rated lifetime at the rated core temperature T_{CORE} . For example, if the ambient temperature is 85°C the core temperature is 85°C + 5°C = 90°C. $(105^\circ\text{C} - 90^\circ\text{C})/7^\circ\text{C} = 2.143$. $2^{2.143} = 4.417$. So the expected lifetime is $5,000 \times 4.417 = 22,085$ hours. Long life capacitors are recommended for LED applications and are available with ratings of up to 20,000 hours or more at 105°C.

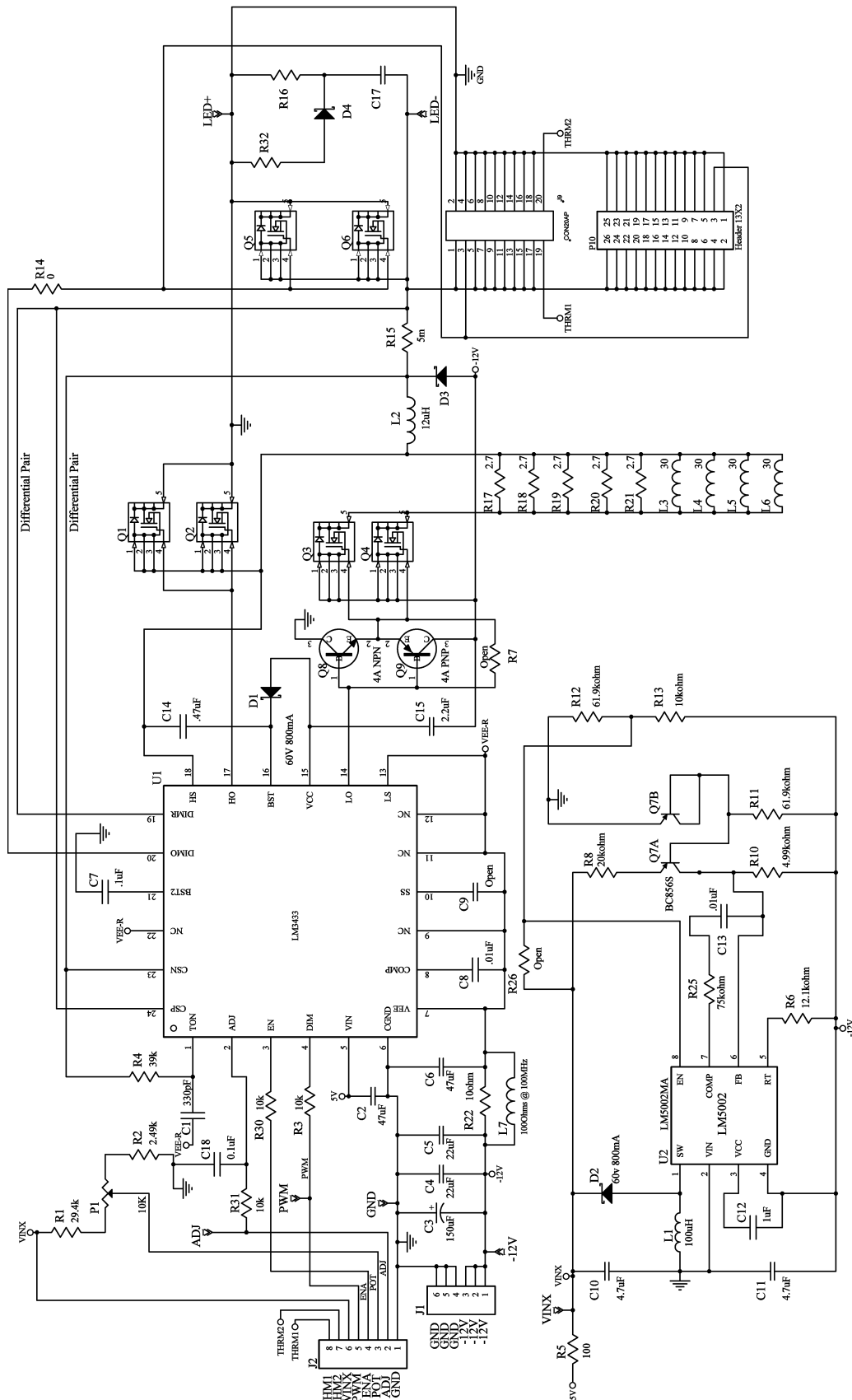


Figure 1. LM3433 Evaluation Board Schematic

Table 1. Bill of Materials (BOM)

| Qty | ID | Part Number | Type | Size | Parameters | Vendor |
|-----|------------------------|--------------------|-----------------|-------------------|-----------------|-------------------------|
| 1 | U1 | LM3433 | LED Driver | WQFN-24 | | TI |
| 1 | U2 | LM5002 | Boost Regulator | SOIC-8 | | TI |
| 1 | C1 | C0805C331J5GACTU | Capacitor | 0805 | 330pF, 50V | Kemet |
| 1 | C2 | GRM31CR60J476KE19L | Capacitor | 1206 | 47µF, 6.3V | Murata |
| 1 | C3 | 16SA150M | Capacitor | MULTICAP | 150µF, 16V | Sanyo |
| 2 | C4, C5 | GRM32ER61C226KE20L | Capacitor | 1210 | 22µF, 16V | Murata |
| 1 | C6 | GRM32ER61C476ME15L | Capacitor | 1210 | 47µF, 16V | Murata |
| 1 | C7 | C0805C104J5RACTU | Capacitor | 0805 | 0.1µF, 50V | Kemet |
| 2 | C8, C13 | HMK212BJ103KG-T | Capacitor | 0805 | 10nF, 100V | Taiyo Yuden |
| | C9 | OPEN | | 0805 | | |
| 2 | C10, C11 | GRM21BR61C475KA | Capacitor | 0805 | 4.7µF, 16V | Murata |
| 1 | C12 | 0805YD105KAT2A | Capacitor | 0805 | 1µF, 16V | AVX |
| 1 | C14 | B37941K9474K60 | Capacitor | 0805 | 0.47µF, 16V | EPCOS Inc. |
| 1 | C15 | GRM21BF51E225ZA01L | Capacitor | 0805 | 2.2µF, 25V | Murata |
| | C17 | OPEN | | 0805 | | |
| 1 | C18 | 08055C104JAT2A | Capacitor | 0805 | 0.1µF, 50V | AVX |
| 2 | D1, D2 | MA2YD2600L | Diode | SOD-123 | 60V, 800mA | Panasonic |
| 1 | D3 | MBRS240LT3 | Diode | SMB | 40V, 2A | ON Semiconductor |
| | D4 | OPEN | | SMB | | |
| 1 | J2 | B8B-EH-A(LF)(SN) | Connector | | | JST Sales America, Inc. |
| 1 | J1 | 1761582001 | Connector | | | Weidmuller |
| 1 | J9 | TFML-110-02-S-D | Connector | TFM-110-02-X-D-LC | | Samtec |
| 1 | L1 | LPS3008-104ML | Inductor | 3008 | 100µH, 150mA | Coilcraft |
| 1 | L2 | GA3252-AL | Inductor | GA3252-AL | 12µH, 14A | Coilcraft |
| 4 | L3, L4, L5, L6 | MPZ2012S300A | Ferrite Bead | 0805 | 30Ω @ 100MHz | TDK |
| 1 | L7 | MPZ2012S101A | Ferrite Bead | 0805 | 100Ω @ 100MHz | TDK |
| 1 | P1 | 3352T-1-103LF | Potentiometer | BOURNS2 | 10kΩ | Bourns |
| 1 | P10 | 3429-6002 | Connector | HDR13x2 | 13X2 Pin Header | 3M |
| 2 | Q1, Q2, Q3, Q4, Q5, Q6 | NTMFS4841NH | FET | PowerPAK | 30V, 11mΩ | ON Semiconductor |
| 1 | Q7 | BC856S | Dual PNP | SOT363_N | | Phillips |
| 1 | Q8 | ZXTN25040DFHTA | NPN | SOT-23B | | Zetex Inc. |
| 1 | Q9 | ZXTP25040DFHTA | PNP | SOT-23B | | Zetex Inc. |
| 1 | R1 | ERJ-6ENF2942V | Resistor | 0805 | 29.4kΩ | Panasonic |
| 1 | R2 | ERJ-6ENF2491V | Resistor | 0805 | 2.49kΩ | Panasonic |
| 3 | R3, R30, R31 | ERJ-6ENF1002V | Resistor | 0805 | 10kΩ | Panasonic |
| 1 | R4 | ERJ-6GEYJ393V | Resistor | 0805 | 39kΩ | Panasonic |
| 1 | R5 | ERJ-6GEYJ101V | Resistor | 0805 | 100Ω | Panasonic |
| | R7 | OPEN | | | | |
| 2 | R14 | ERJ-6GEY0R00V | Resistor | 0805 | 0Ω | Panasonic |
| 1 | R8 | ERJ-6ENF2002V | Resistor | 0805 | 20kΩ | Panasonic |
| 1 | R10 | ERJ-6ENF4991V | Resistor | 0805 | 4.99kΩ | Panasonic |
| 2 | R11, R12 | ERJ-6ENF6192V | Resistor | 0805 | 61.9kΩ | Panasonic |
| 1 | R13 | ERJ-6GEYJ103V | Resistor | 0805 | 10kΩ | Panasonic |

Table 1. Bill of Materials (BOM) (continued)

| Qty | ID | Part Number | Type | Size | Parameters | Vendor |
|-----|---------------------------------|-----------------|-----------|-------------|------------|-----------|
| 1 | R15 | WSL25125L000FEA | Resistor | CR6332-2512 | 0.005Ω | Vishay |
| 6 | R16, R17, R18, R19, R20, R21 | ERJ-6GEYJ2R7V | Resistor | 0805 | 2.7Ω | Panasonic |
| 1 | R22 | ERJ-6GEYJ100V | Resistor | 0805 | 10Ω | Panasonic |
| 1 | R25 | ERJ-6ENF7502V | Resistor | 0805 | 75kΩ | Panasonic |
| | R26 | OPEN | | 0805 | | |
| 2 | LED+, LED- | 1502-2 | Test Post | TP 1502 | 0.109" | Keystone |
| 3 | ADJ, PWM, VINX | 1593-2 | Test Post | TP 1593 | 0.084" | Keystone |

6 Typical Performance Characteristics

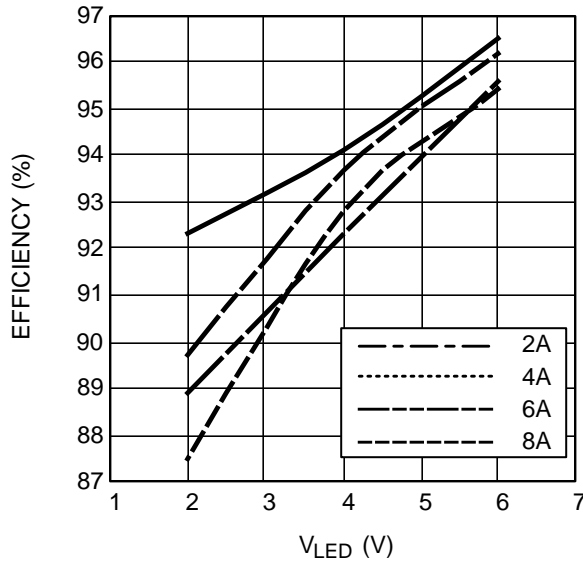


Figure 2. Efficiency vs. LED Forward Voltage ($V_{CGND} - V_{EE} = 9V$)

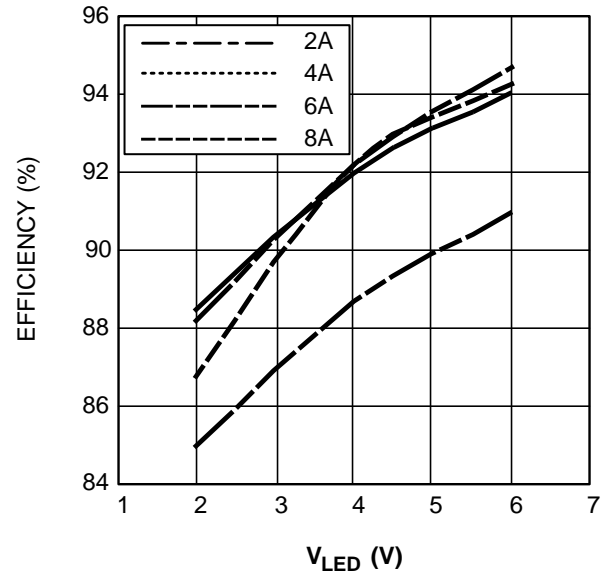


Figure 3. Efficiency vs. LED Forward Voltage ($V_{CGND} - V_{EE} = 12V$)

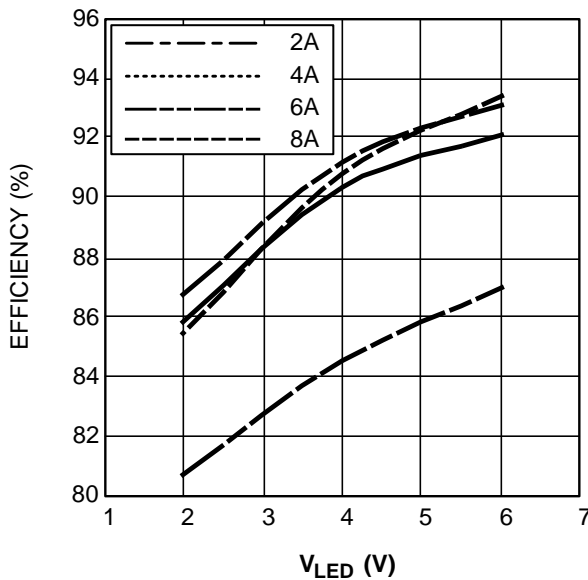


Figure 4. Efficiency vs. LED Forward Voltage ($V_{CGND} - V_{EE} = 14V$)

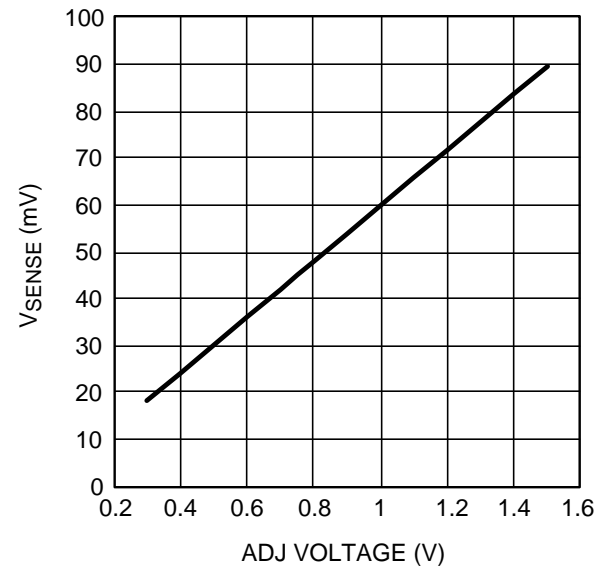
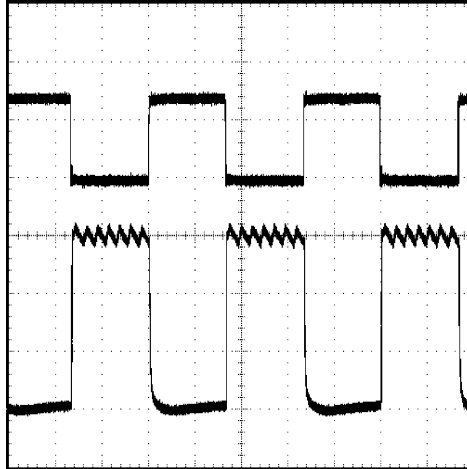


Figure 5. V_{SENSE} vs. V_{ADJ}



I_{LED} = 6A nominal, V_{IN} = 3.3V, V_{EE} = -12V Top trace: DIM input, 2V/div, DC Bottom trace: I_{LED}, 2A/div, DC T = 10 μ s/div
Figure 6. 30kHz PWM Dimming Waveform Showing Inductor Ripple Current

7 Layout

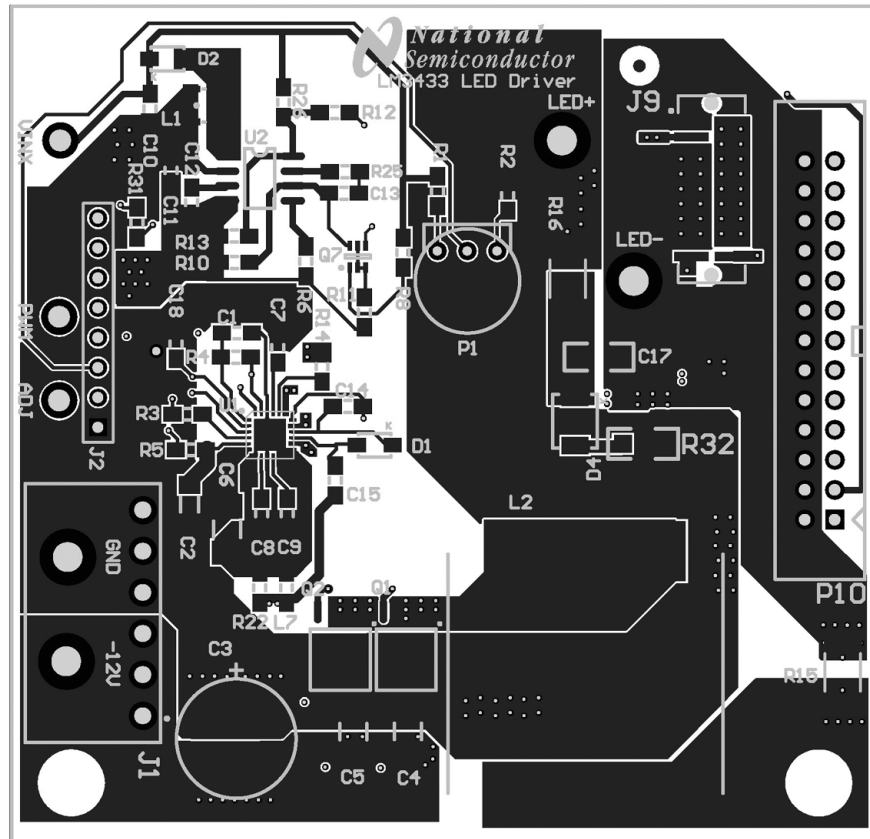


Figure 7. Top Layer and Top Overlay

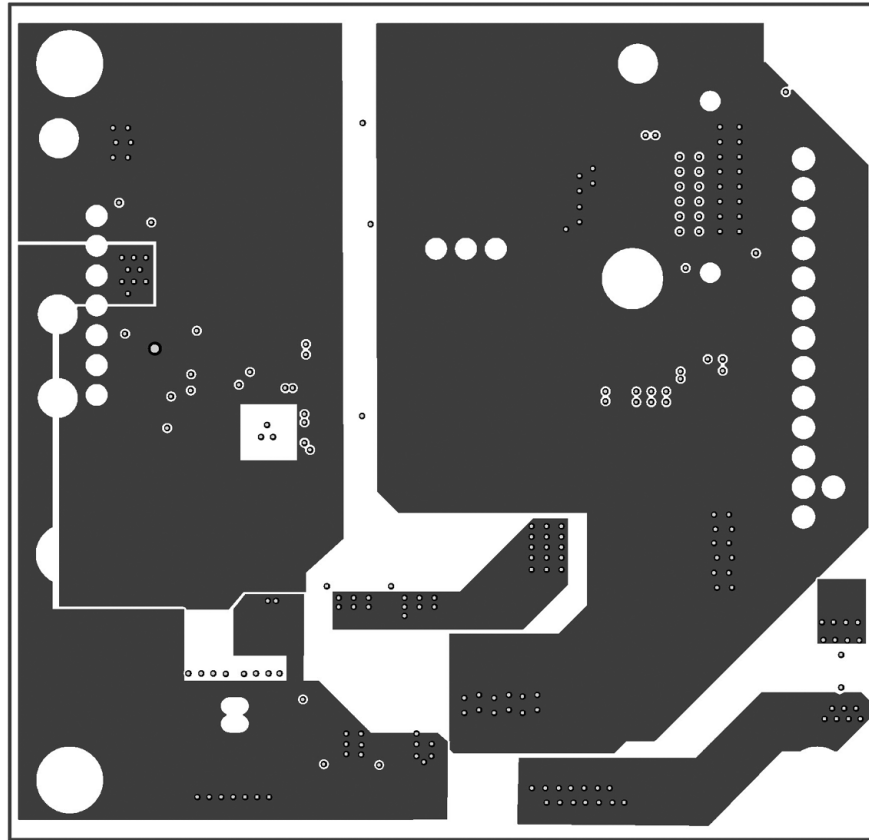


Figure 8. Upper Middle Layer

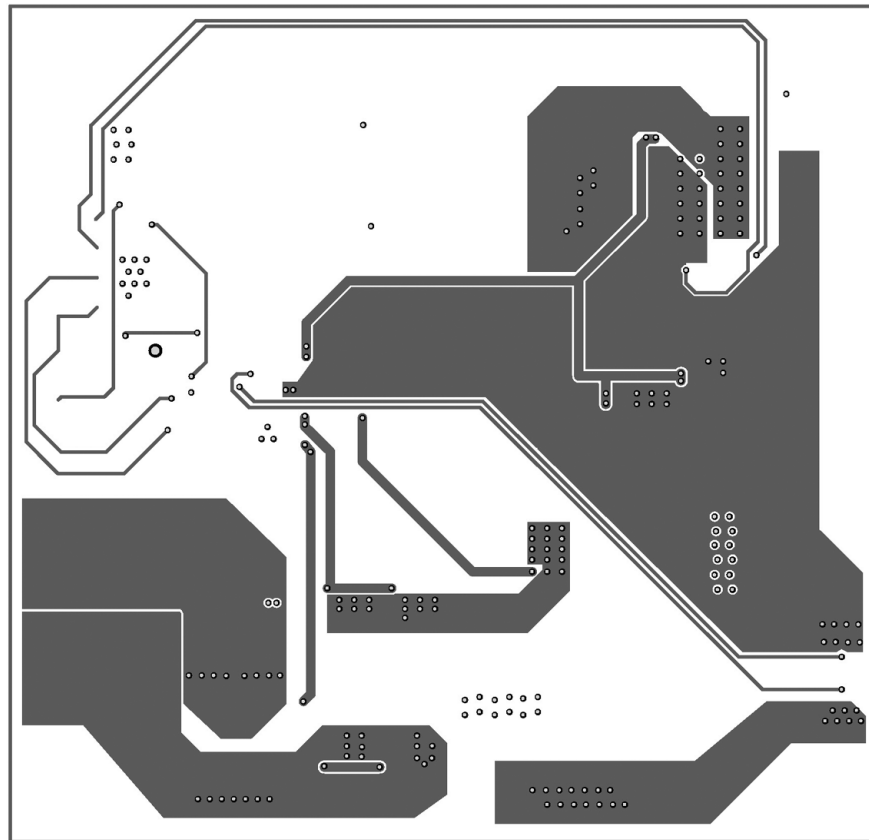


Figure 9. Lower Middle Layer

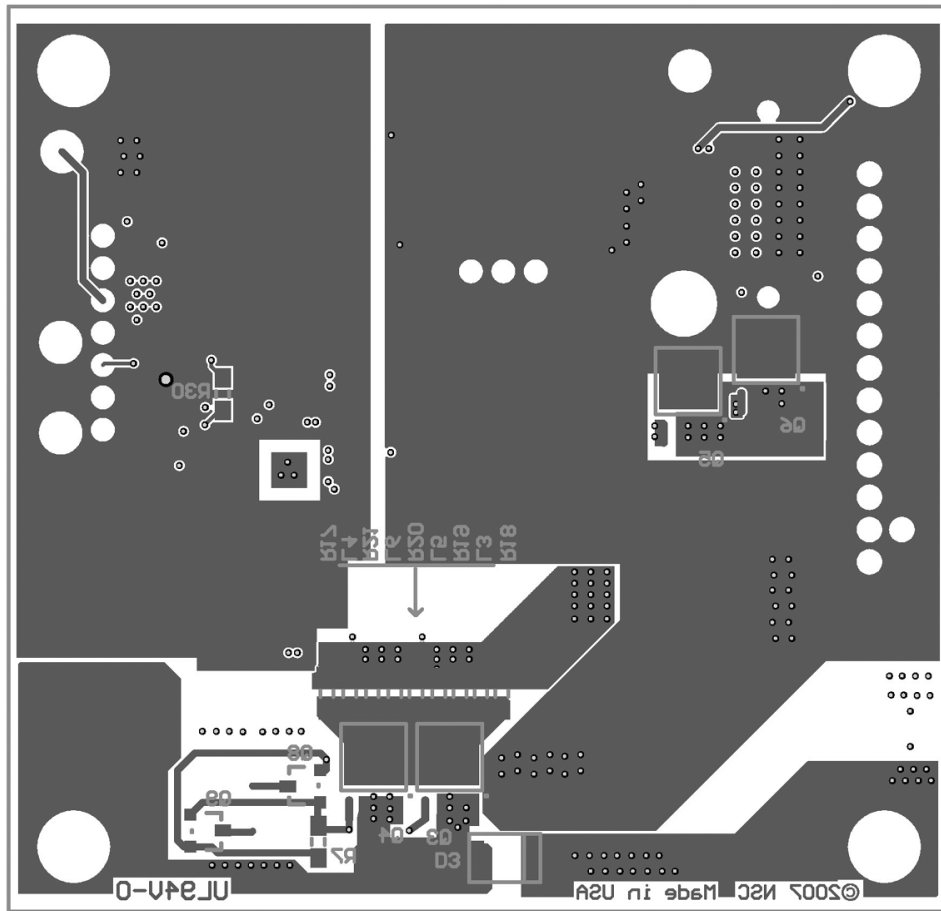


Figure 10. Bottom Layer and Bottom Overlay

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