THE DATASHEET OF

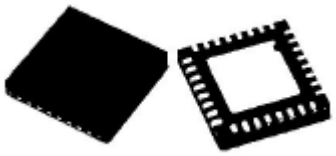
L6229QTR

L6229Q

DMOS driver for three-phase brushless DC motor

Features

- Operating supply voltage from 8 to 52 V
- 2.8 A output peak current (1.4 A RMS)
- $R_{DS(on)}$ 0.73 Ω typ. value @ T_J = 25 °C
- Operating frequency up to 100 kHz
- Non dissipative overcurrent detection and protection
- Diagnostic output
- Constant t_{OFF} PWM current controller
- Slow decay synchronous rectification
- 60° and 120° hall effect decoding logic
- Brake function
- Cross conduction protection
- Thermal shutdown
- Under voltage lockout
- Integrated fast free wheeling diodes



VFQFPN32 5 mm x 5 mm

Description

The L6229Q is a DMOS fully integrated three-phase motor driver with overcurrent protection.

Realized in BCDmultipower technology, the device combines isolated DMOS power transistors with CMOS and bipolar circuits on the same chip.

The device includes all the circuitry needed to drive a three-phase BLDC motor including: a three-phase DMOS bridge, a constant off time PWM current controller and the decoding logic for single ended hall sensors that generates the required sequence for the power stage.

Available in VFQFPN-32 5 x 5 package, the L6229Q features a non-dissipative overcurrent protection on the high side power MOSFETs and thermal shutdown.

Table 1. Device summary

Order codes	Package	Packaging
L6229Q	VFQFPN32 5x5x1.0 mm	Tube
L6229QTR		Tape and reel

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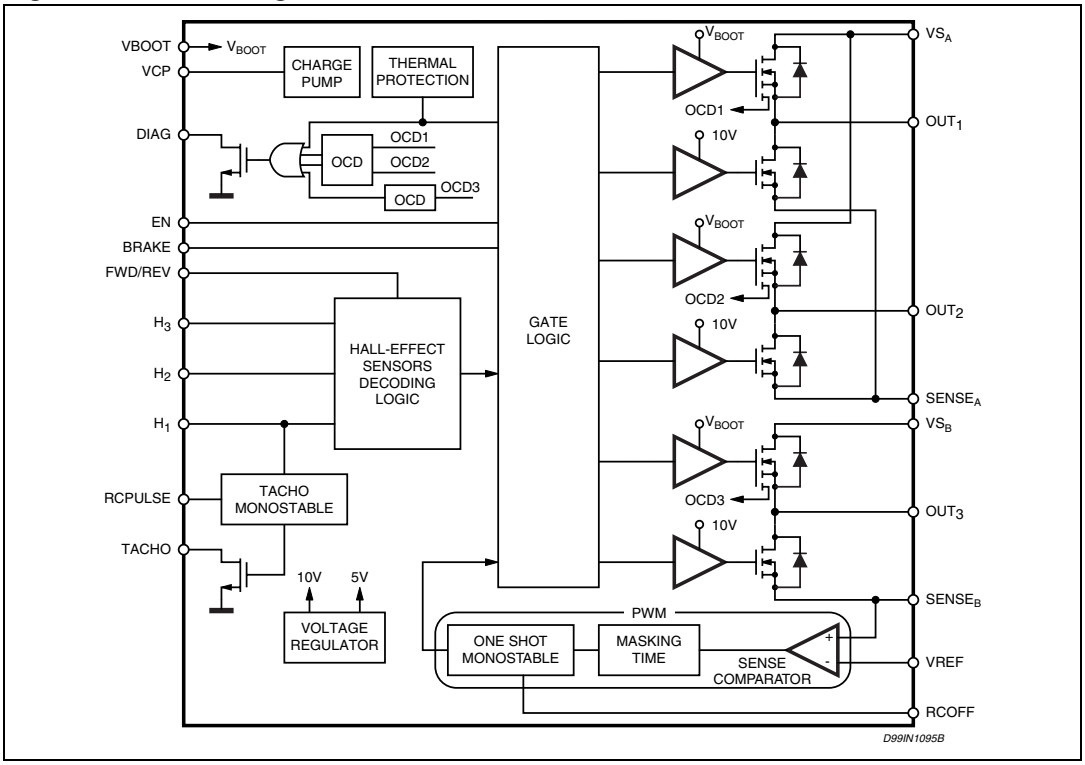
1 Block diagram

Figure 1. Block diagram



2 Electrical data

2.1 Absolute maximum ratings

Table 2. Absolute maximum ratings

Symbol	Parameter	Parameter	Value	Unit
V_S	Supply voltage	$V_{SA} = V_{SB} = V_S$	60	V
V_{OD}	Differential voltage between: VS_A, OUT_1, OUT_2, $SENSE_A$ and VS_B, OUT_3, $SENSE_B$	$V_{SA} = V_{SB} = V_S = 60$ V; $V_{SENSEA} = V_{SENSEB}$ = GND	60	V
V_{BOOT}	Bootstrap peak voltage	$V_{SA} = V_{SB} = V_S$	V_S + 10	V
V_{IN}, V_{EN}	Logic inputs voltage range		-0.3 to +7	V
V_{REF}	Voltage range at pin VREF		-0.3 to +7	V
V_{RCOFF}	Voltage range at pin RCOFF		-0.3 to +7	V
$V_{RCPULSE}$	Voltage range at pin RCPULSE		-0.3 to +7	V
V_{SENSE}	Voltage range at pins $SENSE_A$ and $SENSE_B$		-1 to +4	V
$I_{S(peak)}$	Pulsed supply current (for each V_S pin)	$V_{SA} = V_{SB} = V_S$; $T_{PULSE} < 1$ ms	3.55	A
I_S	RMS supply current (for each V_S pin)	$V_{SA} = V_{SB} = V_S$	1.4	A
T_{stg}, T_{OP}	Storage and operating temperature range		-40 to 150	°C

2.2 Recommended operating conditions

Table 3. Recommended operating conditions

Symbol	Parameter	Parameter	Min	Max	Unit
V_S	Supply voltage	$V_{SA} = V_{SB} = V_S$	8	52	V
V_{OD}	Differential voltage between VS_A, $OUT1_A$, $OUT2_A$, $SENSE_A$ and VS_B, $OUT1_B$, $OUT2_B$, $SENSE_B$	$V_{SA} = V_{SB} = V_S$; $V_{SENSEA} = V_{SENSEB}$		52	V
V_{REFA}, V_{REFB}	Voltage range at pins V_{REFA} and V_{REFB}		-0.1	5	V
V_{SENSEA}, V_{SENSEB}	Voltage range at pins $SENSE_A$ and $SENSE_B$	(pulsed $t_W < t_{rr}$) (DC)	-6 -1	6 1	V V
I_{OUT}	RMS output current			1.4	A
T_J	Operating junction temperature		-25	+125	°C
f_{sw}	Switching frequency			100	kHz

2.3 Thermal data

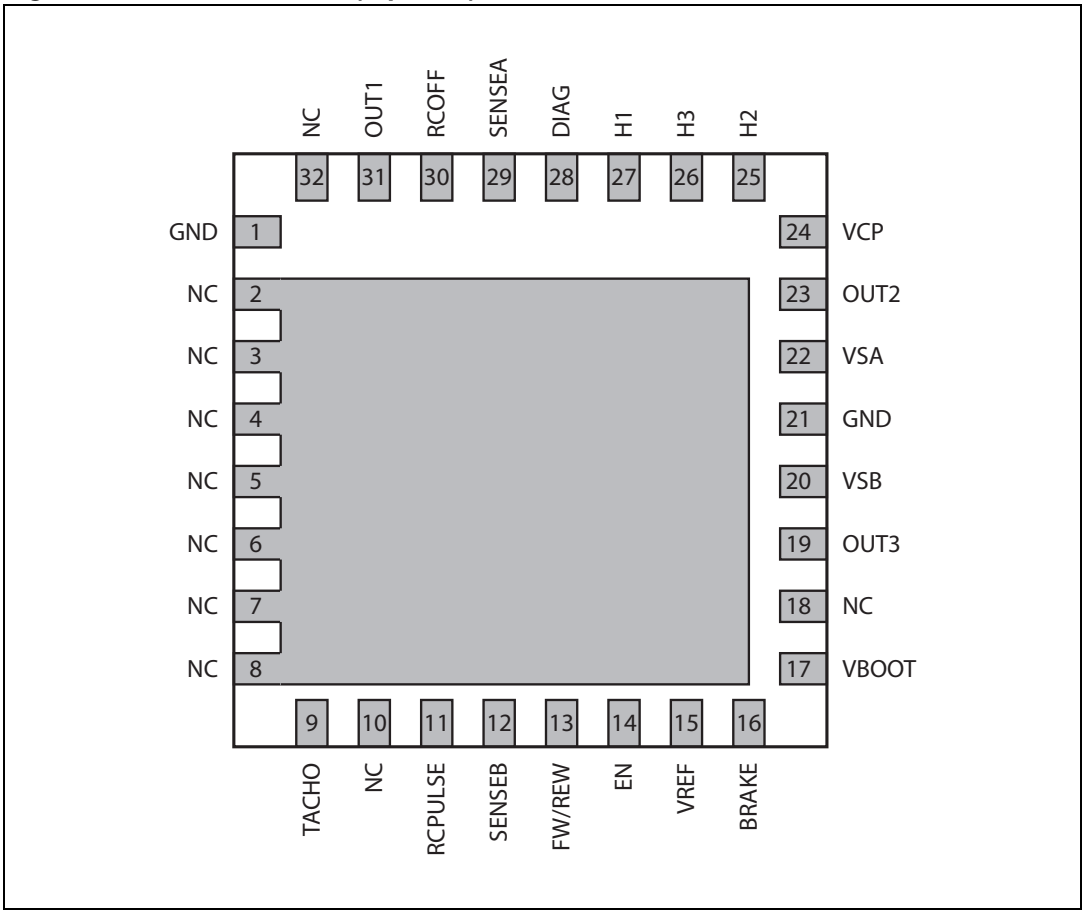
Table 4. Thermal data

Symbol	Parameter	Value	Unit
$R_{th(JA)}$	Thermal resistance junction-ambient max. (1)	42	°C/W

1. Mounted on a double-layer FR4 PCB with a dissipating copper surface of 0.5 cm^2 on the top side plus 6 cm^2 ground layer connected through 18 via holes (9 below the IC).

3 Pin connection

Figure 2. Pin connection (top view)



Note: 1 The pins 2 to 8 are connected to die PAD.

2 The die PAD must be connected to GND pin.

Table 5. Pin description

N°	Pin	Type	Function
1, 21	GND	GND	Ground terminals.
9	TACHO	Open drain output	Frequency-to-voltage open drain output. Every pulse from pin H_1 is shaped as a fixed and adjustable length pulse.
11	RCPULSE	RC pin	RC network pin. A parallel RC network connected between this pin and ground sets the duration of the monostable pulse used for the frequency-to-voltage converter.
12	$SENSE_B$	Power supply	Half bridge 3 source Pin. This pin must be connected together with pin $SENSE_A$ to power ground through a sensing power resistor. At this pin also the Inverting Input of the sense comparator is connected.
13	FWD/REV	Logic input	Selects the direction of the rotation. HIGH logic level sets forward operation, whereas LOW logic level sets reverse operation. If not used, it has to be connected to GND or +5 V.
14	EN	Logic input	Chip enable. LOW logic level switches OFF all power MOSFETs. If not used, it has to be connected to +5 V.
15	VREF	Logic input	Current controller reference voltage. Do not leave this pin open or connect to GND.
16	BRAKE	Logic input	Brake input pin. LOW logic level switches ON all high side power MOSFETs, implementing the brake function. If not used, it has to be connected to +5 V.
17	VBOOT	Supply voltage	Bootstrap voltage needed for driving the upper power MOSFETs.
19	OUT_3	Power output	Output half bridge 3.
20	VS_B	Power supply	Half bridge 3 power supply voltage. It must be connected to the supply voltage together with pin VS_A.
22	VS_A	Power supply	Half bridge 1 and half bridge 2 power supply voltage. It must be connected to the supply voltage together with pin VS_B.
23	OUT_2	Power output	Output half bridge 2.
24	VCP	Output	Charge pump oscillator output.
25	H_2	Sensor input	Single ended hall effect sensor input 2.
26	H_3	Sensor input	Single ended hall effect sensor input 3.
27	H_1	Sensor input	Single ended hall effect sensor input 1.
28	DIAG	Open drain output	Overcurrent detection and thermal protection pin. An internal open drain transistor pulls to GND when an overcurrent on one of the high side MOSFETs is detected or during thermal protection.
29	$SENSE_A$	Power supply	Half bridge 1 and half bridge 2 source pin. This pin must be connected together with pin $SENSE_B$ to power ground through a sensing power resistor.
30	RCOFF	RC pin	RC network pin. A parallel RC network connected between this pin and ground sets the current controller OFF-Time.
31	OUT_1	Power output	Output half bridge 1.

4 Electrical characteristics

Table 6. Electrical characteristics
(V_S = 48 V, T_A = 25 °C, unless otherwise specified)

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
$V_{Sth(ON)}$	Turn-on threshold		5.8	6.3	6.8	V
$V_{Sth(OFF)}$	Turn-off threshold		5	5.5	6	V
I_S	Quiescent supply current	All bridges OFF; T_J = -25 °C to 125 °C(1)		5	10	mA
$T_{j(OFF)}$	Thermal shutdown temperature			165		°C
Output DMOS transistors						
$R_{DS(on)}$	High-side + low-side switch ON resistance	T_J = 25 °C		1.47	1.69	Ω
		T_J =125 °C (1)		2.35	2.70	Ω
I_{DSS}	Leakage current	EN = Low; OUT = V_S			2	mA
		EN = Low; OUT = GND	-0.3			mA
Source drain diodes						
V_{SD}	Forward ON voltage	I_{SD} = 1.4 A, EN = LOW		1.15	1.3	V
t_{rr}	Reverse recovery time	I_f = 1.4 A		300		ns
t_{fr}	Forward recovery time			200		ns
Logic inputs (EN, CONTROL, HALF/FULL, CLOCK, RESET, CW/CCW)						
V_{IL}	Low level logic input voltage		-0.3		0.8	V
V_{IH}	High level logic input voltage		2		7	V
I_{IL}	Low level logic input current	GND logic input voltage	-10			µA
I_{IH}	High level logic input current	7 V logic input voltage			10	µA
$V_{th(ON)}$	Turn-on input threshold			1.8	2.0	V
$V_{th(OFF)}$	Turn-off input threshold		0.8	1.3		V
$V_{th(HYS)}$	Input threshold hysteresis		0.25	0.5		V
Switching characteristics						
$t_{D(ON)EN}$	Enable to output turn-on delay time (2)	I_{LOAD} = 1.4 A, resistive load	500	650	800	ns
$t_{D(OFF)EN}$	Enable to output turn-off delay time (2)		500		1000	ns
$t_{D(on)IN}$	Other logic inputs to OUT turn-ON delay time			1.6		µs
$t_{D(off)IN}$	Other logic inputs to OUT turn-OFF delay time			800		ns
t_{RISE}	Output rise time (2)		40		250	ns
t_{FALL}	Output fall time (2)		40		250	ns
t_{DT}	Dead time		0.5	1		µs

Table 6. Electrical characteristics (continued)
(V_S = 48 V, T_A = 25 °C, unless otherwise specified)

Symbol	Parameter	Test condition	Min	Typ	Max	Unit
f_{CP}	Charge pump frequency	T_J = -25 °C to 125 °C (1)		0.6	1	MHz
PWM comparator and monostable						
I_{RCOFF}	Source current at pin RCOFF	V_{RCOFF} = 2.5 V	3.5	5.5		mA
V_{OFFSET}	Offset voltage on sense comparator (3)	V_{ref} = 0.5 V		±5		mV
t_{prop}	Turn OFF propagation delay (4)	V_{ref} = 0.5 V		500		ns
t_{blank}	Internal blanking time on sense comparator			1		µs
$t_{ON(min)}$	Minimum on time			2.5	3	µs
t_{OFF}	PWM recirculation time	R_{OFF} = 20 kΩ; C_{OFF} = 1 nF		13		µs
		R_{OFF} = 100 kΩ; C_{OFF} = 1 nF		61		µs
I_{BIAS}	Input bias current at pin VREF				10	µA
Tacho monostable						
$I_{RCPULSE}$	Source current at pin RCPULSE	$V_{RCPULSE}$ = 2.5 V	3.5	5.5		mA
t_{PULSE}	Monostable of time	R_{PUL} = 20 kΩ; C_{PUL} = 1 nF		12		µs
		R_{PUL} = 100 kΩ; C_{PUL} = 1 nF		60		µs
R_{TACHO}	Open drain ON resistance			40	60	W
Over current detection and protection						
I_{SOVER}	Supply overcurrent protection threshold	T_J = -25 to 125 °C (2)	2	2.8	3.55	A
R_{OPDR}	Open drain ON resistance	I_{DIAG} = 4 mA		40	60	W
I_{OH}	OCD high level leakage current	V_{DIAG} = 5 V		1		µA
$t_{OCD(ON)}$	OCD turn-ON delay time (4)	I_{DIAG} = 4 mA; C_{DIAG} < 100 pF		200		ns
$t_{OCD(OFF)}$	OCD turn-OFF delay time (4)	I_{DIAG} = 4 mA; C_{DIAG} < 100 pF		100		ns

1. Tested at 25 °C in a restricted range and guaranteed by characterization
2. See *Figure 3*.
3. Measured applying a voltage of 1 V to pin SENSE and a voltage drop from 2 V to 0 V to pin VREF.
4. See *Figure 4*.

Figure 3. Switching characteristic definition

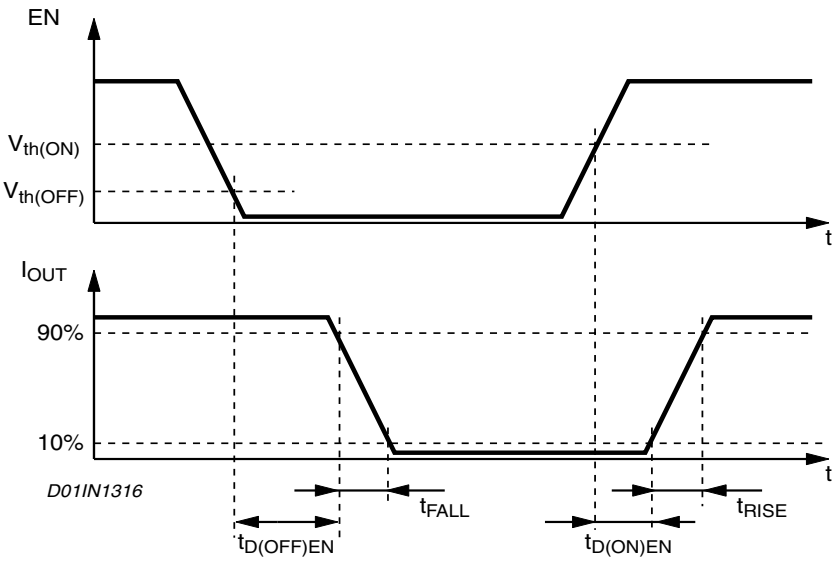
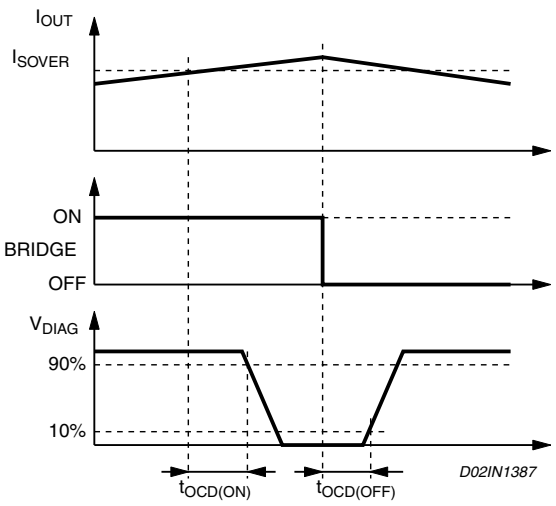


Figure 4. Overcurrent detection timing definition



5 Circuit description

5.1 Power stages and charge pump

The L6229Q integrates a three-phase bridge, which consists of 6 power MOSFETs connected as shown on the block diagram (see *Figure 1*). each power MOS has an $R_{DS(ON)}$ = 0.73 Ω (typical value @ 25 °C) with intrinsic fast freewheeling diode. Switching patterns are generated by the PWM current controller and the hall effect sensor decoding logic (see relative paragraph 3.3 and 3.5). Cross conduction protection is implemented by using a dead time (t_{DT} = 1 µs typical value) set by internal timing circuit between the turn off and turn on of two power MOSFETs in one leg of a bridge.

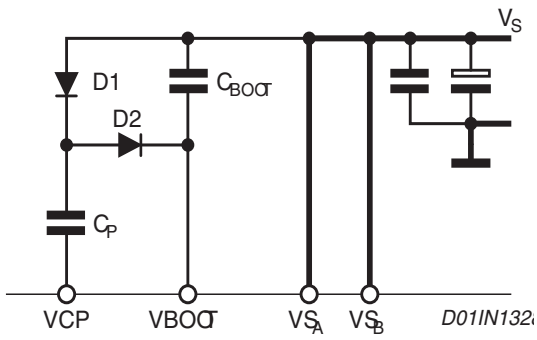
Pins VS_A and VS_B must be connected together to the supply voltage (V_S).

Using N-channel power MOS for the upper transistors in the bridge requires a gate drive voltage above the power supply voltage. The bootstrapped supply (V_{BOOT}) is obtained through an internal oscillator and few external components to realize a charge pump circuit as shown in *Figure 5*. The oscillator output (pin VCP) is a square wave at 600 kHz (typically) with 10 V amplitude. Recommended values/part numbers for the charge pump circuit are shown in *Table 7*.

Table 7. Charge pump external component values

Component	Value
C_{BOOT}	220 nF
C_P	10 nF
D1	1N4148
D2	1N4148

Figure 5. Charge pump circuit



5.2 Logic inputs

Pins FWD/REV, BRAKE, EN, H1, H2 and H3 are TTL/CMOS and microcontroller compatible logic inputs. The internal structure is shown in *Figure 6*. Typical value for turn-on and turn-off thresholds are respectively $V_{th(ON)}$= 1.8 V and $V_{th(OFF)}$= 1.3 V.

Pin EN (Enable) has identical input structure with the exception that the drain of the Overcurrent and thermal protection MOSFET is also connected to this pin. Due to this connection some care needs to be taken in driving this pin. The EN input may be driven in one of two configurations as shown in *Figure 10* or *Figure 11*. If driven by an open drain (collector) structure, a pull-up resistor R_{EN} and a capacitor C_{EN} are connected as shown in *Figure 10*. If the driver is a standard Push-Pull structure the resistor R_{EN} and the capacitor C_{EN} are connected as shown in *Figure 11*. The resistor R_{EN} should be chosen in the range from 2.2 kΩ to 180 kΩ. Recommended values for R_{EN} and C_{EN} are respectively 10 kΩ and 5.6 nF. More information on selecting the values is found in the overcurrent protection section.

Figure 6. Logic inputs internal structure

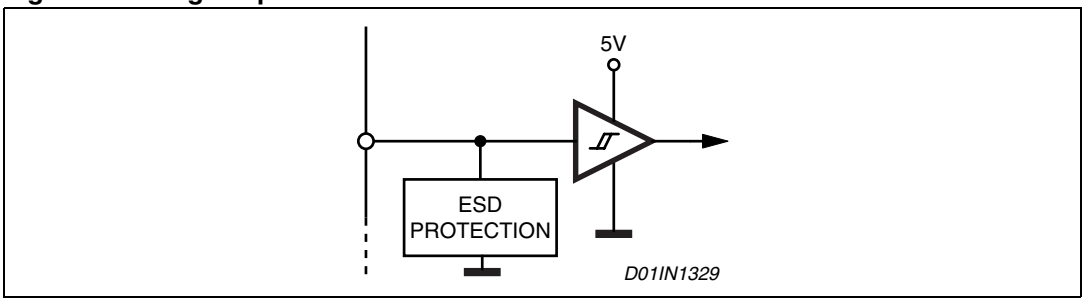


Figure 7. Pin EN open collector driving

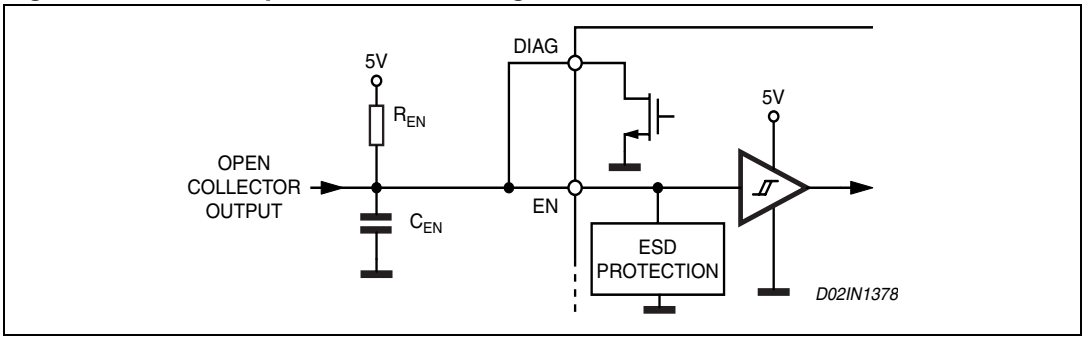
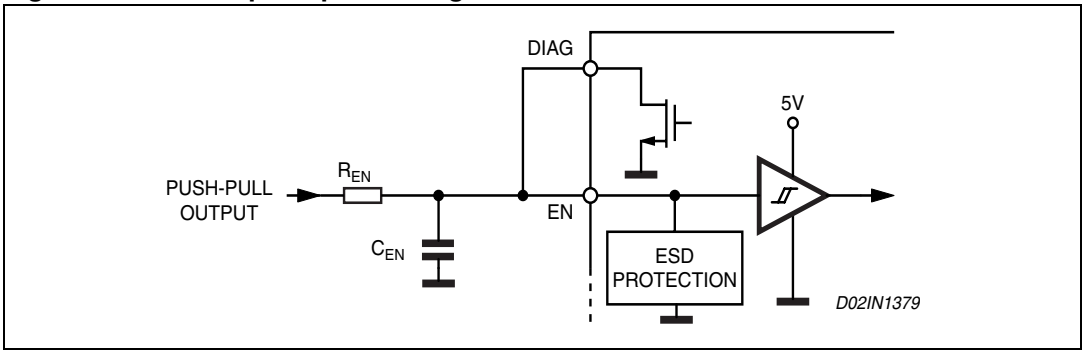


Figure 8. Pin EN push-pull driving



5.3 PWM current control

The L6229Q includes a constant off time PWM current controller. The current control circuit senses the bridge current by sensing the voltage drop across an external sense resistor connected between the source of the three lower power MOS transistors and ground, as shown in *Figure 9*. As the current in the motor increases the voltage across the sense resistor increases proportionally. When the voltage drop across the sense resistor becomes greater than the voltage at the reference input pin VREF the sense comparator triggers the monostable switching the bridge off. The power MOS remain off for the time set by the monostable and the motor current recirculates around the upper half of the bridge in slow decay mode as described in the next section. When the monostable times out, the bridge will again turn on. Since the internal dead time, used to prevent cross conduction in the bridge, delays the turn on of the power MOS, the effective off time t_{OFF} is the sum of the monostable time plus the dead time.

Figure 10 shows the typical operating waveforms of the output current, the voltage drop across the sensing resistor, the pin RC voltage and the status of the bridge. More details regarding the synchronous rectification and the output stage configuration are included in the next section.

Immediately after the power MOS turn on, a high peak current flows through the sense resistor due to the reverse recovery of the freewheeling diodes. The L6229Q provides a 1 µs blanking time t_{BLANK} that inhibits the comparator output so that the current spike cannot prematurely re trigger the monostable.

Figure 9. PWM current controller simplified schematic

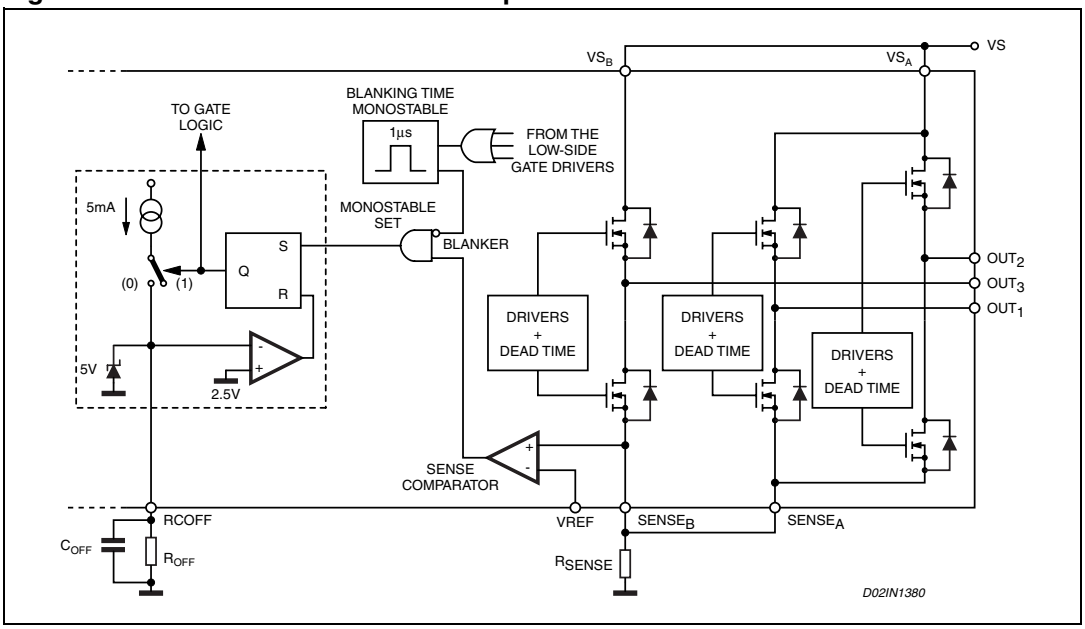


Figure 10. Output current regulation waveforms

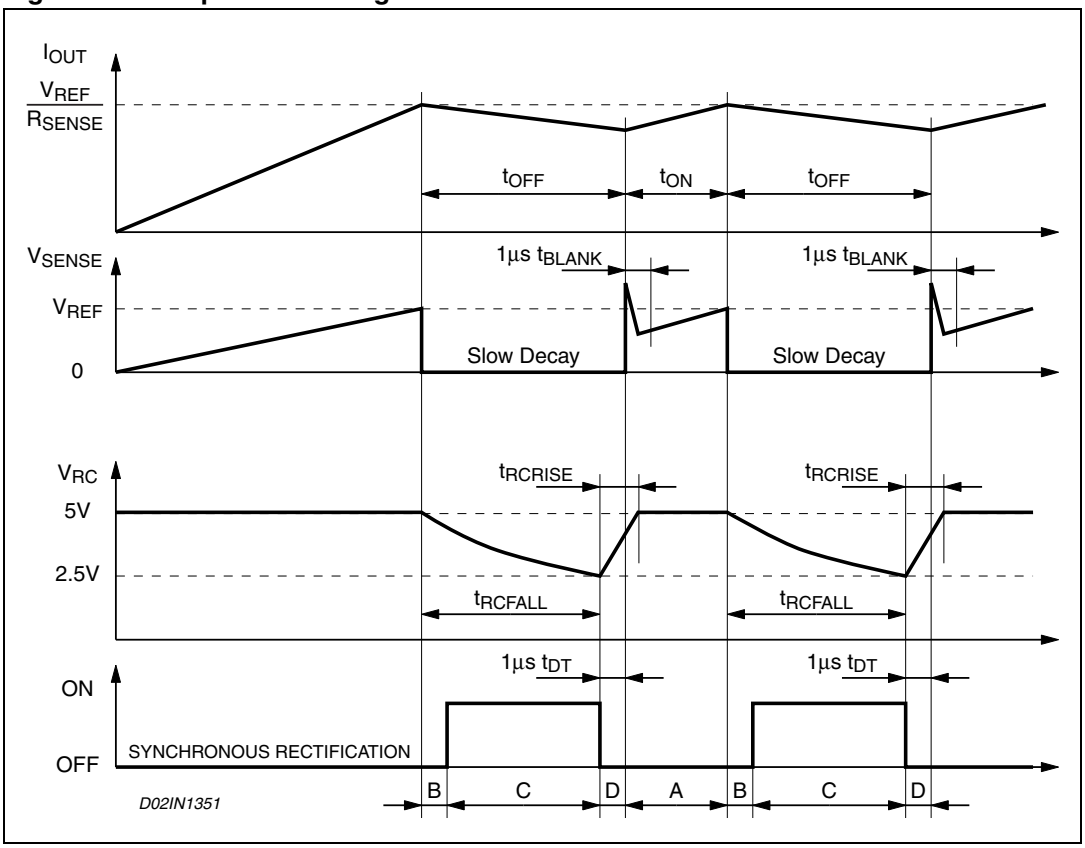


Figure 11 shows the magnitude of the Off Time t_{OFF} versus C_{OFF} and R_{OFF} values. It can be approximately calculated from the equations:

$t_{RCFALL} = 0.6 \cdot R_{OFF} \cdot C_{OFF}$

$t_{OFF} = t_{RCFALL} + t_{DT} = 0.6 \cdot R_{OFF} \cdot C_{OFF} + t_{DT}$

where R_{OFF} and C_{OFF} are the external component values and t_{DT} is the internally generated Dead Time with:

$20\ k\Omega \leq R_{OFF} \leq 100\ k\Omega$

$0.47\ nF \leq C_{OFF} \leq 100\ nF$

$t_{DT} = 1\ \mu s$ (typical value)

Therefore:

$t_{OFF(MIN)} = 6.6\ \mu s$

$t_{OFF(MAX)} = 6\ ms$

These values allow a sufficient range of t_{OFF} to implement the drive circuit for most motors.

The capacitor value chosen for C_{OFF} also affects the Rise Time t_{RCRISE} of the voltage at the pin RCOFF. The rise time t_{RCRISE} will only be an issue if the capacitor is not completely charged before the next time the monostable is triggered. Therefore, the on time t_{ON}, which depends by motors and supply parameters, has to be bigger than t_{RCRISE} for allowing a good current regulation by the PWM stage. Furthermore, the on time t_{ON} can not be smaller than the minimum on time $t_{ON(MIN)}$.

$$\begin{cases} t_{ON} > t_{ON(MIN)} = 2.5\mu s & \text{(typ. value)} \\ t_{ON} > t_{RCRISE} - t_{DT} \end{cases}$$

$$t_{RCRISE} = 600 \cdot C_{OFF}$$

Figure 12 shows the lower limit for the on time t_{ON} for having a good PWM current regulation capacity. It has to be said that t_{ON} is always bigger than $t_{ON(MIN)}$ because the device imposes this condition, but it can be smaller than t_{RCRISE} - t_{DT}. In this last case the device continues to work but the off time t_{OFF} is not more constant.

So, small C_{OFF} value gives more flexibility for the applications (allows smaller on time and, therefore, higher switching frequency), but, the smaller is the value for C_{OFF}, the more influential will be the noises on the circuit performance.

Figure 11. t_{OFF} versus C_{OFF} and R_{OFF}

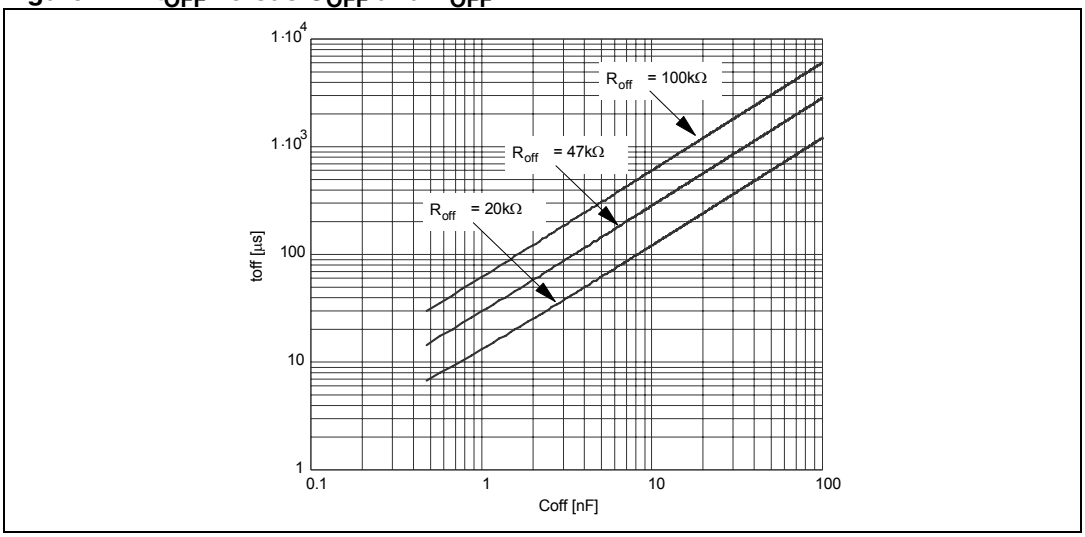
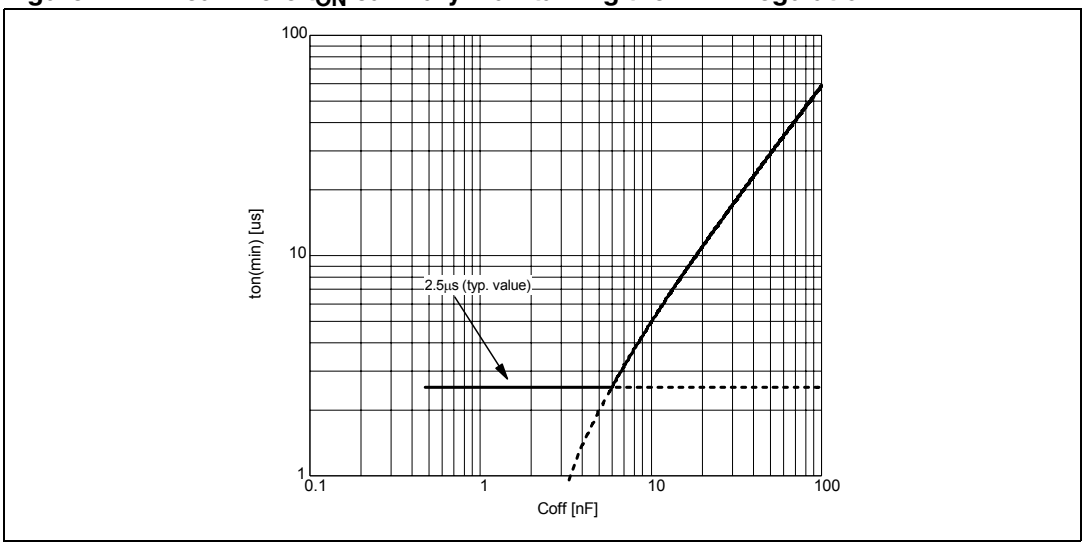


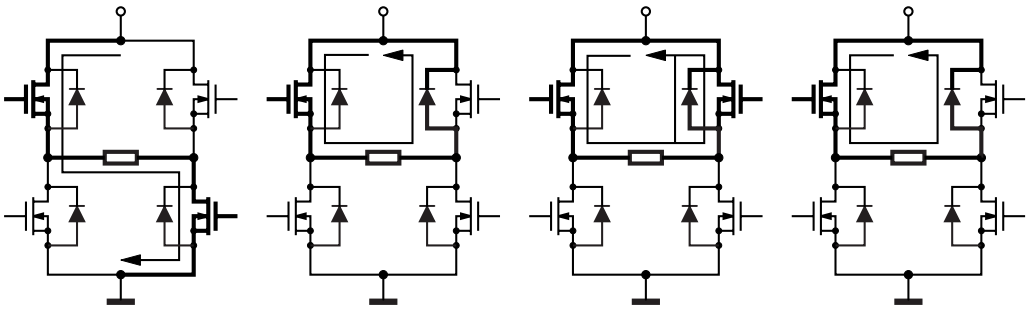
Figure 12. Area where t_{ON} can vary maintaining the PWM regulation



5.4 Slow decay mode

Figure 13 shows the operation of the bridge in the slow decay mode during the off time. At any time only two legs of the three-phase bridge are active, therefore only the two active legs of the bridge are shown in the figure and the third leg will be off. At the start of the Off Time, the lower power MOS is switched off and the current recirculates around the upper half of the bridge. Since the voltage across the coil is low, the current decays slowly. After the dead time the upper power MOS is operated in the synchronous rectification mode reducing the impedance of the freewheeling diode and the related conducting losses. When the monostable times out, upper MOS that was operating the synchronous mode turns off and the lower power MOS is turned on again after some delay set by the dead time to prevent cross conduction.

Figure 13. Slow decay mode output stage configurations



5.5 Decoding logic

The decoding logic section is a combinatory logic that provides the appropriate driving of the three-phase bridge outputs according to the signals coming from the three hall sensors that detect rotor position in a 3-phase BLDC motor. This novel combinatory logic discriminates between the actual sensor positions for sensors spaced at 60, 120, 240 and 300 electrical degrees. This decoding method allows the implementation of a universal IC without dedicating pins to select the sensor configuration.

There are eight possible input combinations for three sensor inputs. Six combinations are valid for rotor positions with 120 electrical degrees sensor phasing (see *Figure 14*, positions 1, 2, 3a, 4, 5 and 6a) and six combinations are valid for rotor positions with 60 electrical degrees phasing (see *Figure 15*, positions 1, 2, 3b, 4, 5 and 6b). Four of them are in common (1, 2, 4 and 5) whereas there are two combinations used only in 120 electrical degrees sensor phasing (3a and 6a) and two combinations used only in 60 electrical degrees sensor phasing (3b and 6b).

The decoder can drive motors with different sensor configuration simply by following the *Table 8*. For any input configuration (H_1, H_2 and H_3) there is one output configuration (OUT_1, OUT_2 and OUT_3). The output configuration 3a is the same than 3b and analogously output configuration 6a is the same than 6b.

The sequence of the Hall codes for 300 electrical degrees phasing is the reverse of 60 and the sequence of the Hall codes for 240 phasing is the reverse of 120. So, by decoding the 60

and the 120 codes it is possible to drive the motor with all the four conventions by changing the direction set.

Table 8. 60 and 120 electrical degree decoding logic in forward direction

Hall 120°	**1**	**2**	**3a**	**-**	**4**	**5**	**6a**	**-**
Hall 60°	1	2	-	3b	4	5	-	6b
H_1	H	H	L	H	L	L	H	L
H_2	L	H	H	H	H	L	L	L
H_3	L	L	L	H	H	H	H	L
OUT_1	Vs	High Z	GND	GND	GND	High Z	Vs	Vs
OUT_2	High Z	Vs	Vs	Vs	High Z	GND	GND	GND
OUT_3	GND	GND	High Z	High Z	Vs	Vs	High Z	High Z
Phasing	1->3	2->3	2->1	2->1	3->1	3->2	1->2	1->2

Figure 14. 120° hall sensor sequence

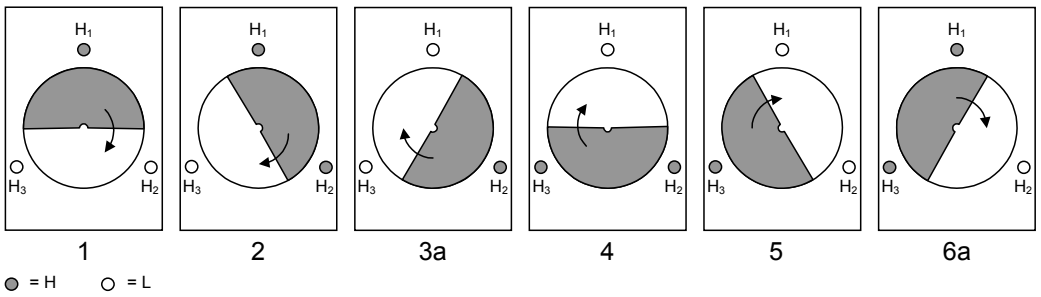
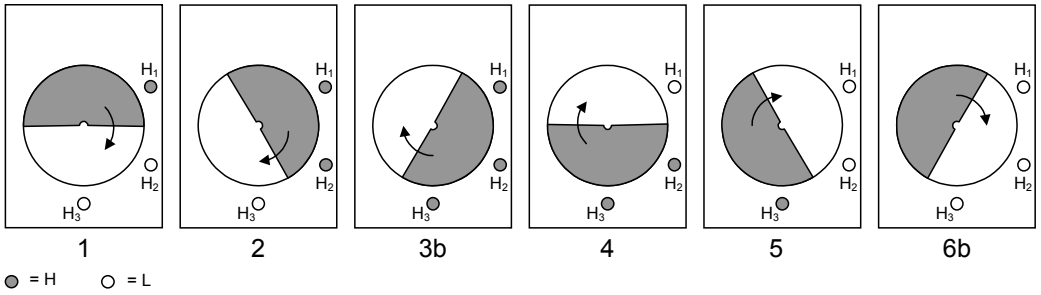


Figure 15. 60° hall sensor sequence



5.6 Tacho

A tachometer function consists of a monostable, with constant off time (t_{PULSE}), whose input is one hall effect signal (H_1). It allows developing an easy speed control loop by using an external op amp, as shown in *Figure 17*. For component values refer to Application Information section.

The monostable output drives an open drain output pin (TACHO). At each rising edge of the hall effect sensors H_1, the monostable is triggered and the MOSFET connected to pin TACHO is turned off for a constant time t_{PULSE} (see *Figure 16*). The off time t_{PULSE} can be set using the external RC network (R_{PUL}, C_{PUL}) connected to the pin RCPULSE. *Figure 18* gives the relation between t_{PULSE} and C_{PUL}, R_{PUL}. We have approximately:

$t_{PULSE} = 0.6 \cdot R_{PUL} \cdot C_{PUL}$

where C_{PUL} should be chosen in the range 1 nF … 100 nF and R_{PUL} in the range 20 kΩ … 100 kΩ.

By connecting the tachometer pin to an external pull-up resistor, the output signal average value V_M is proportional to the frequency of the hall effect signal and, therefore, to the motor speed. This realizes a simple frequency-to-voltage converter. An op amp, configured as an integrator, filters the signal and compares it with a reference voltage V_{REF}, which sets the speed of the motor.

$$V_M = \frac{t_{PULSE}}{T} \cdot V_{DD}$$

Figure 16. Tacho operation waveforms

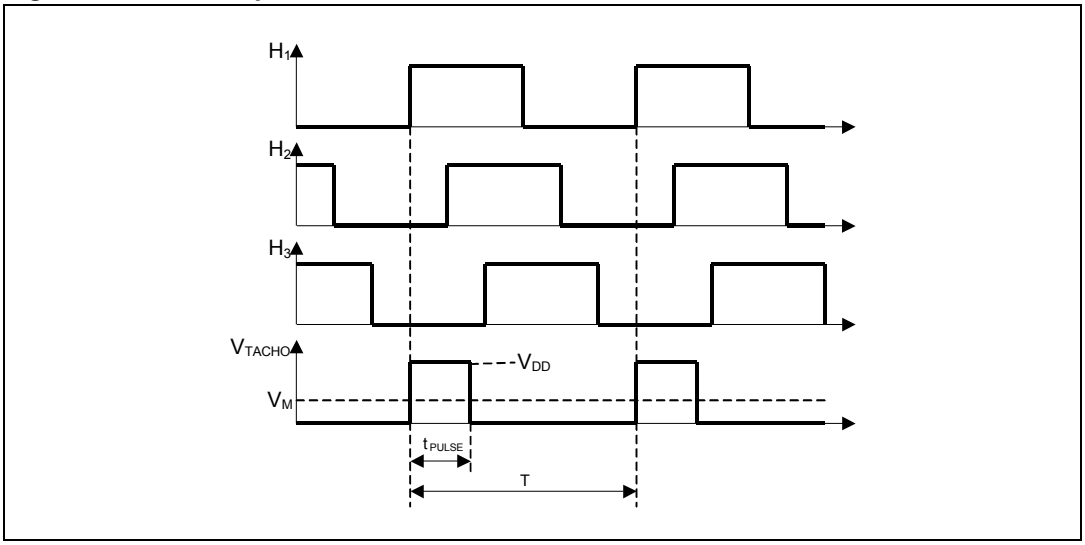


Figure 17. Tachometer speed control loop

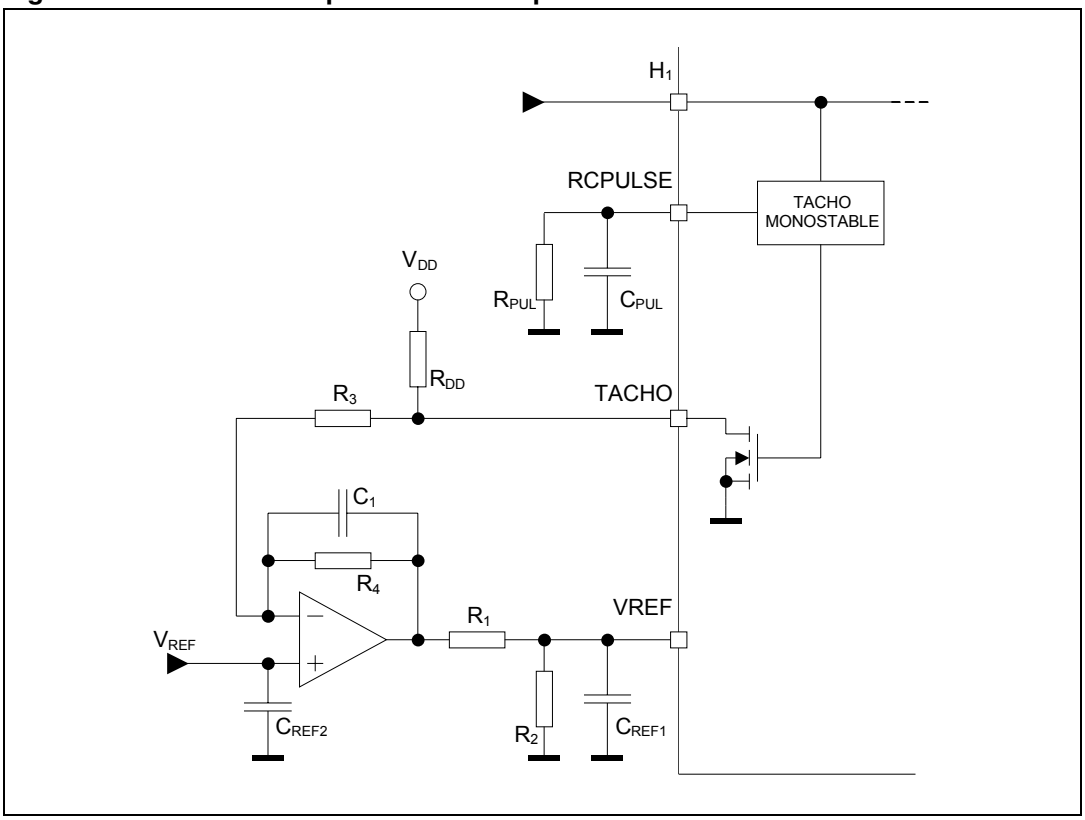
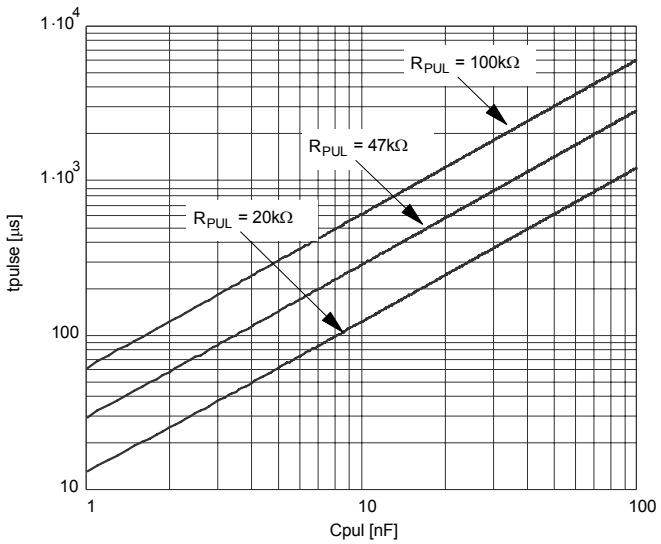


Figure 18. t_{PULSE} versus C_{PUL} and R_{PUL}



5.7 Non-dissipative overcurrent detection and protection

The L6229Q integrates an overcurrent detection circuit (OCD) for full protection. This circuit provides output-to-output and output-to-ground short circuit protection as well. With this internal over current detection, the external current sense resistor normally used and its associated power dissipation are eliminated. *Figure 19* shows a simplified schematic for the overcurrent detection circuit.

To implement the over current detection, a sensing element that delivers a small but precise fraction of the output current is implemented with each high side power MOS. Since this current is a small fraction of the output current there is very little additional power dissipation. This current is compared with an internal reference current I_{REF}. When the output current reaches the detection threshold (typically I_{SOVER} = 2.8 A) the OCD comparator signals a fault condition. When a fault condition is detected, an internal open drain MOS with a pull down capability of 4 mA connected to pin DIAG is turned on.

The pin DIAG can be used to signal the fault condition to a µC or to shut down the three-phase bridge simply by connecting it to pin EN and adding an external R-C (see R_{EN}, C_{EN}).

Figure 19. Overcurrent protection simplified schematic

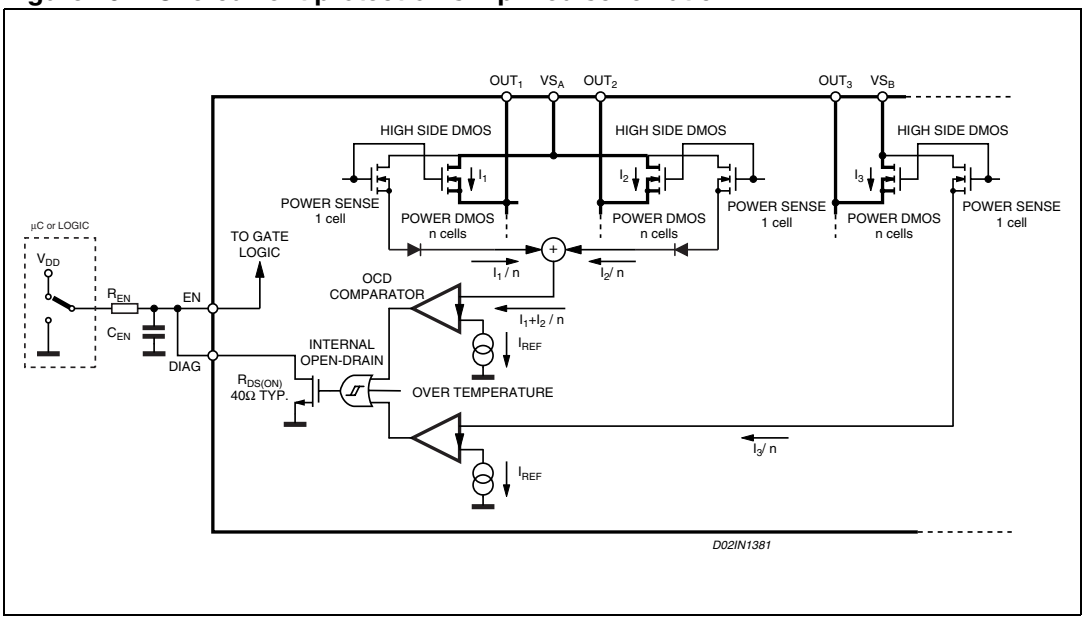


Figure 20 shows the overcurrent detection operation. The disable time $t_{DISABLE}$ before recovering normal operation can be easily programmed by means of the accurate thresholds of the logic inputs. It is affected whether by C_{EN} and R_{EN} values and its magnitude is reported in *Figure 21*. The delay time t_{DELAY} before turning off the bridge when an overcurrent has been detected depends only by C_{EN} value. Its magnitude is reported in *Figure 22*

C_{EN} is also used for providing immunity to pin EN against fast transient noises. Therefore the value of C_{EN} should be chosen as big as possible according to the maximum tolerable delay time and the R_{EN} value should be chosen according to the desired disable time.

The resistor R_{EN} should be chosen in the range from 2.2 kΩ to 180 kΩ. Recommended values for R_{EN} and C_{EN} are respectively 100 kΩ and 5.6 nF that allow obtaining 200 µs disable time.

Figure 20. Overcurrent protection waveforms

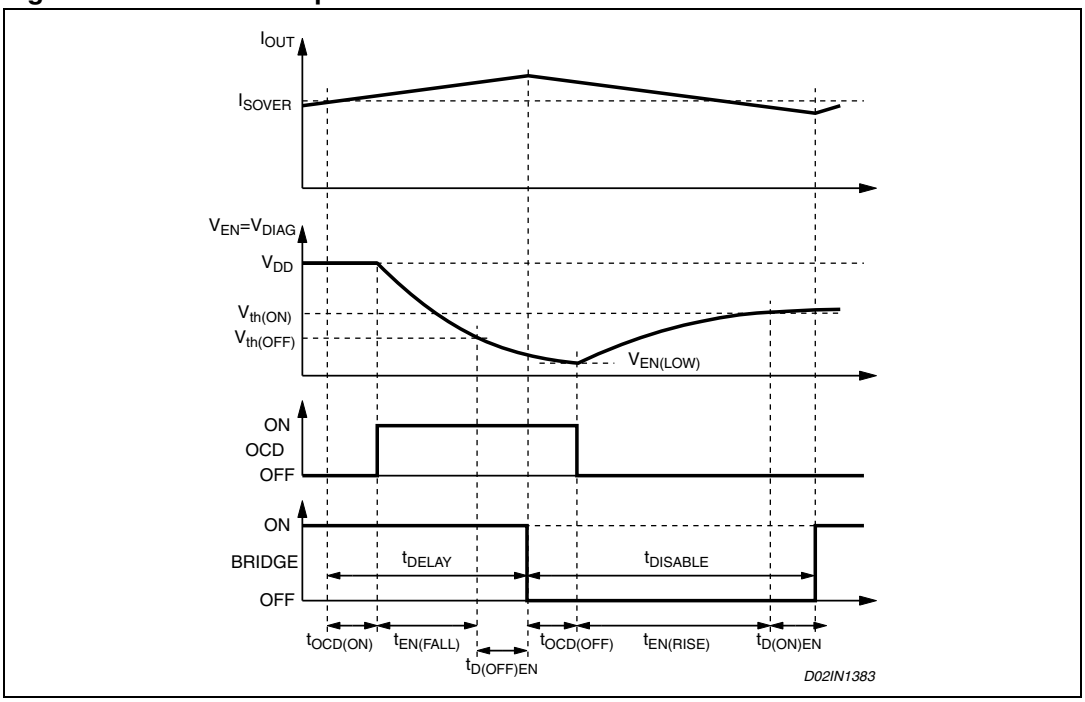


Figure 21. $t_{DISABLE}$ versus C_{EN} and R_{EN}

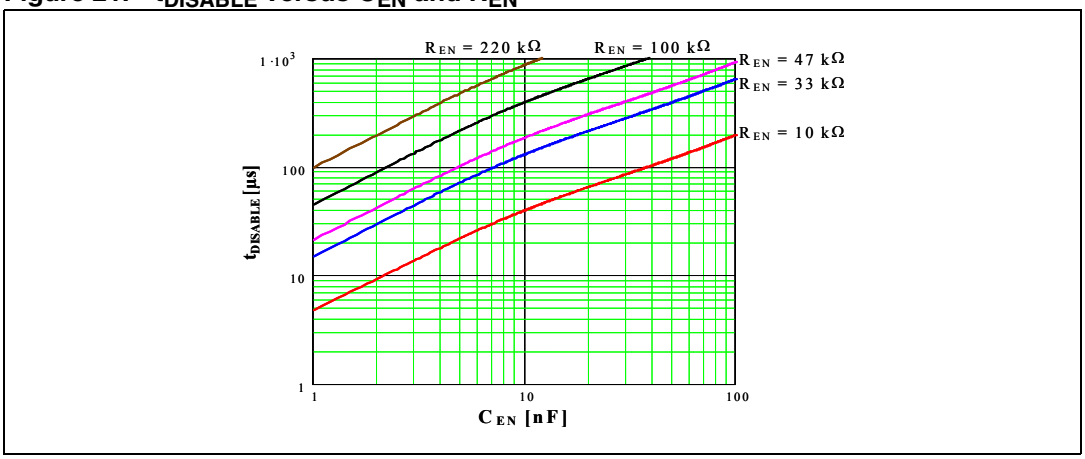
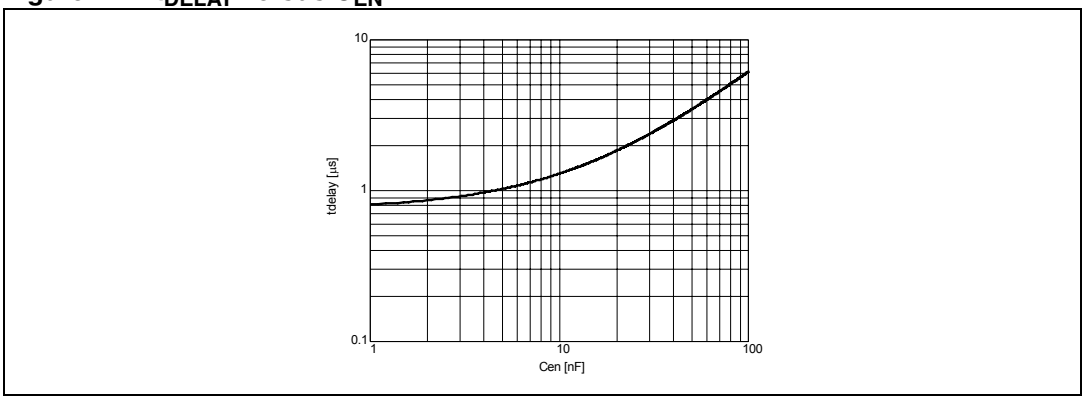


Figure 22. t_{DELAY} versus C_{EN}.



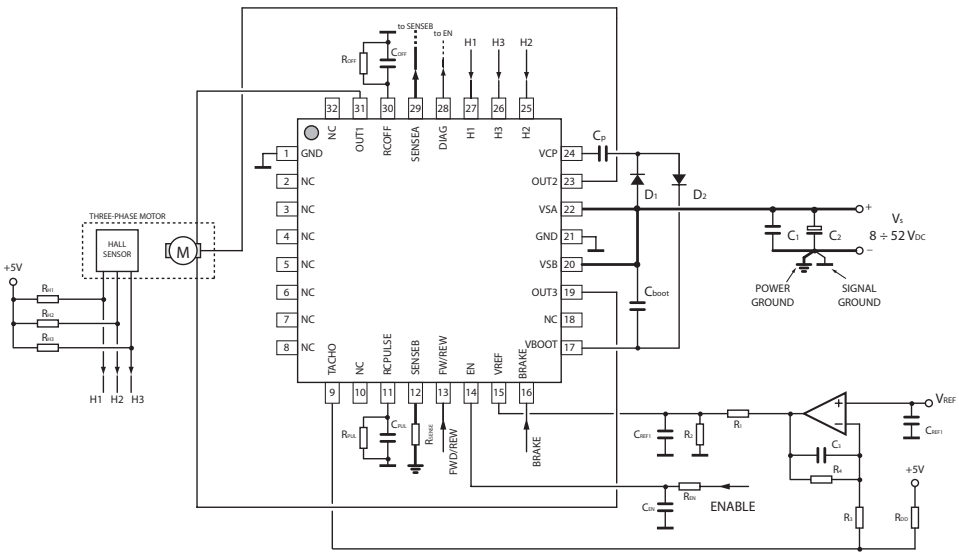
6 Application information

A typical application using L6229Q is shown in *Figure 23*. Typical component values for the application are shown in *Table 9*. A high quality ceramic capacitor (C_2) in the range of 100 nF to 200 nF should be placed between the power pins VS_A and VS_B and ground near the L6229Q to improve the high frequency filtering on the power supply and reduce high frequency transients generated by the switching. The capacitor (C_{EN}) connected from the EN input to ground sets the shut down time when an over current is detected (see overcurrent protection). The two current sensing inputs ($SENSE_A$ and $SENSE_B$) should be connected to the sensing resistor R_{SENSE} with a trace length as short as possible in the layout. The sense resistor should be non-inductive resistor to minimize the dI/dt transients across the resistor. To increase noise immunity, unused logic pins are best connected to 5 V (high logic level) or GND (low logic level) (see pin description). It is recommended to keep power ground and signal ground separated on PCB.

Table 9. Component values for typical application

Component	Value
C_1	100 µF
C_2	100 nF
C_3	220 nF
C_{BOOT}	220 nF
C_{OFF}	1 nF
C_{PUL}	10 nF
C_{REF1}	33 nF
C_{REF2}	100 nF
C_{EN}	5.6 nF
C_P	10 nF
D_1	1N4148
D_2	1N4148
R_1	5 k6Ω
R_2	1 k8Ω
R_3	4 k7Ω
R_4	1 MΩ
R_{DD}	1 kΩ
R_{EN}	100 kΩ
R_{SENSE}	0.6 Ω
R_{OFF}	33 kΩ
R_{PUL}	47 kΩ
R_{H1}, R_{H2}, R_{H3}	10 kΩ

Figure 23. Typical application

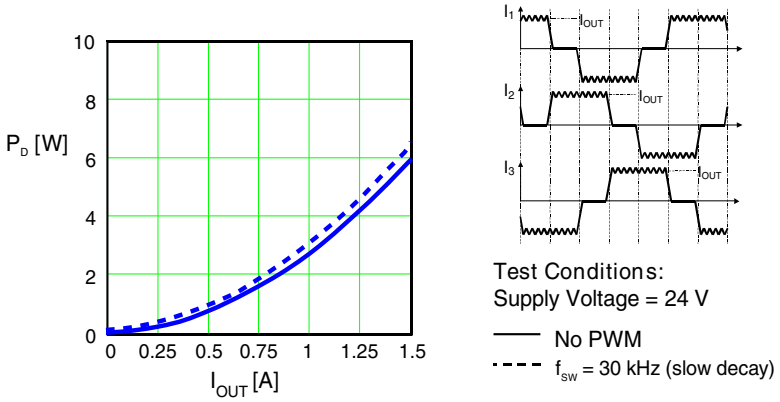


6.1 Output current capability and ic power dissipation

In *Figure 24* is shown the approximate relation between the output current and the IC power dissipation using PWM current control.

For a given output current the power dissipated by the IC can be easily evaluated, in order to establish which package should be used and how large must be the on-board copper dissipating area to guarantee a safe operating junction temperature (125 °C maximum).

Figure 24. IC power dissipation versus output power



6.2 Thermal management

In most applications the power dissipation in the IC is the main factor that sets the maximum current that can be delivered by the device in a safe operating condition. Therefore, it has to be taken into account very carefully. Besides the available space on the PCB, the right package should be chosen considering the power dissipation. Heat sinking can be achieved using copper on the PCB with proper area and thickness.

For instance, using a VFQFPN32L 5 x 5 package the typical $R_{th(JA)}$ is about 42 °C/W when mounted on a double-layer FR4 PCB with a dissipating copper area of 0.5 cm^2 on the top side plus 6 cm^2 ground layer connected through 18 via holes (9 below the IC).

7 Package mechanical data

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK® specifications, grade definitions and product status are available at: www.st.com. ECOPACK® is an ST trademark.

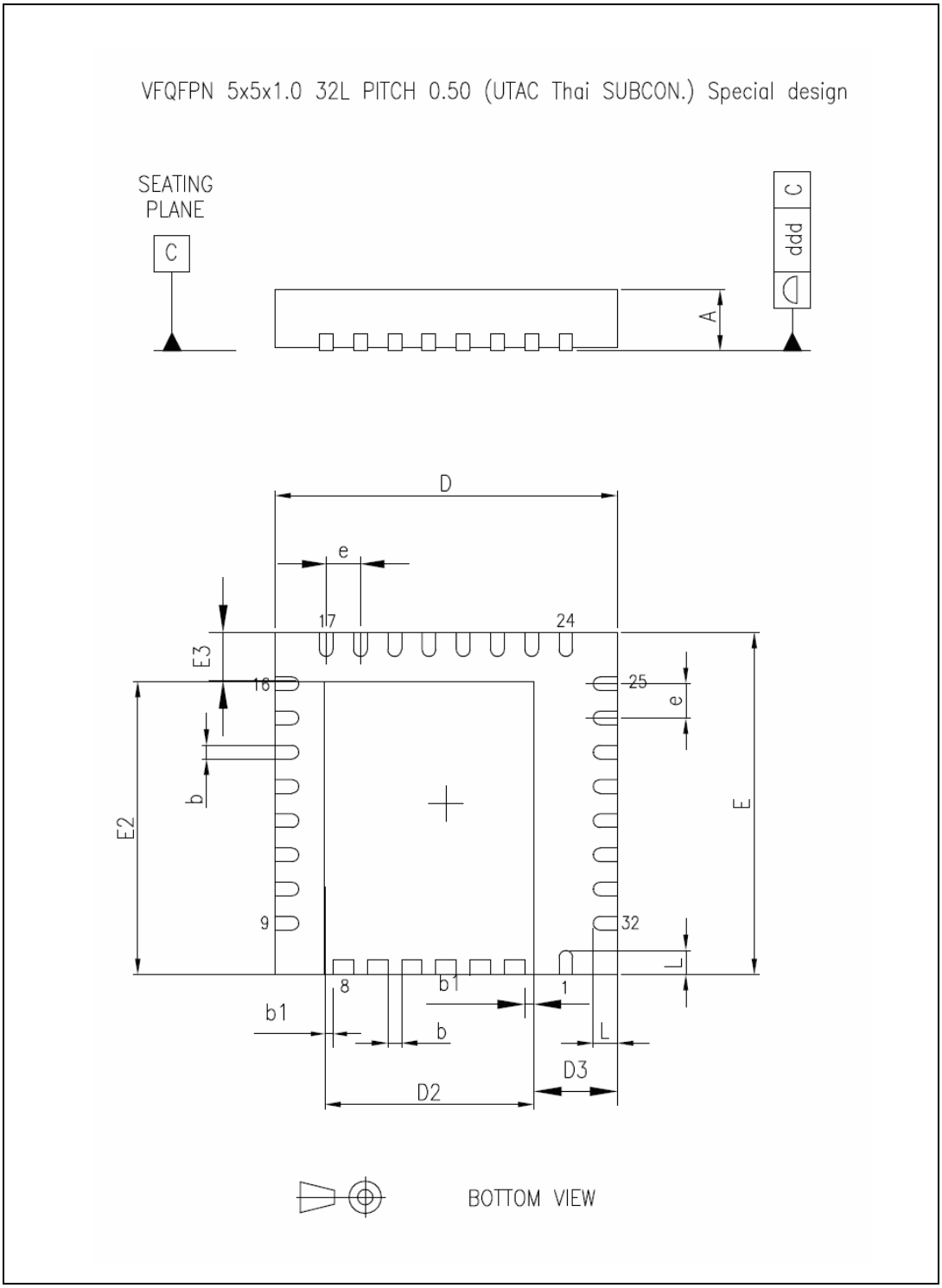
Table 10. VFQFPN 5 x 5 x 1.0, 32 lead, pitch 0.50

Dim.	Databook (mm)		
	Min	Typ	Max
A	0.80	0.85	0.95
b	0.18	0.25	0.30
b1	0.165	0.175	0.185
D	4.85	5.00	5.15
D2	3.00	3.10	3.20
D3	1.10	1.20	1.30
E	4.85	5.00	5.15
E2	4.20	4.30	4.40
E3	0.60	0.70	0.80
e		0.50	
L	0.30	0.40	0.50
ddd			0.08

Note: VFQFPN stands for thermally enhanced very thin profile fine pitch quad flat package no lead. Very thin profile: 0.80 < A < 1.00 mm.

Details of terminal 1 are optional but must be located on the top surface of the package by using either a mold or marked features.

Figure 25. Package dimensions



8 Revision history

Table 11. Document revision history

Date	Revision	Changes
25-Nov-2008	1	First release
26-Feb-2009	2	Updated *Table 4 on page 5*
30-Aug-2010	3	Updated *Table 1 on page 1*

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