



# THE DATASHEET OF LMV552MM/NOPB



## LMV55x 3-MHz, Micropower RRO Amplifiers

### 1 Features

- Specified 3-V and 5-V Performance
- High Unity Gain Bandwidth 3 MHz
- Supply Current (Per Amplifier) 37  $\mu$ A
- CMRR 93 dB
- PSRR 90 dB
- Slew Rate 1 V/ $\mu$ s
- Output Swing With 100-k $\Omega$  Load 70 mV From Rail
- Total Harmonic Distortion: 0.003% at 1 kHz, 2 k $\Omega$
- Temperature Range:  $-40^{\circ}$ C to  $125^{\circ}$ C

### 2 Applications

- Active Filters
- Portable Equipment
- Automotive
- Battery Powered Systems
- Sensors and Instrumentation

### 3 Description

The LMV55x are high-performance, low-power operational amplifiers implemented with TI's advanced VIP50 process. They feature 3 MHz of bandwidth while consuming only 37  $\mu$ A of current per amplifier, which is an exceptional bandwidth to power ratio in this op amp class. These ultra-low power amplifiers are unity gain stable and provide an excellent solution for ultra-low power applications requiring a wide bandwidth.

The LMV55x have a rail-to-rail output stage and an input common mode range that extends below ground.

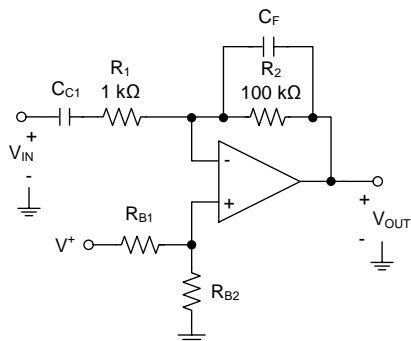
The LMV55x have an operating supply voltage range from 2.7 V to 5.5 V. These amplifiers can operate over a wide temperature range ( $-40^{\circ}$ C to  $125^{\circ}$ C), making them a great choice for automotive applications, sensor applications as well as portable instrumentation applications. The LMV551 is offered in the ultra tiny 5-Pin SC70 and 5-Pin SOT-23 package. The LMV552 is offered in an 8-Pin VSSOP package. The LMV554 is offered in the 14-Pin TSSOP.

#### Device Information<sup>(1)</sup>

PART NUMBER	PACKAGE	BODY SIZE (NOM)
LM551	SOT-23 (5)	2.90 mm x 1.60 mm
	SC70 (5)	2.00 mm x 1.25 mm
LMV552	VSSOP (8)	3.00 mm x 3.00 mm
LMV554	TSSOP (14)	5.00 mm x 4.40 mm

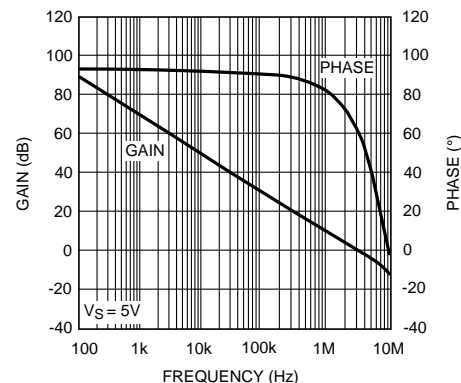
(1) For all available packages, see the orderable addendum at the end of the data sheet.

#### Typical Application Schematic



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#### Open Loop Gain and Phase vs Frequency



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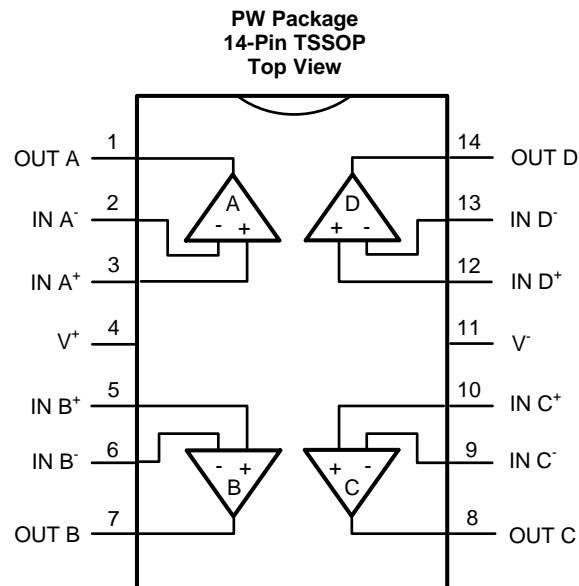
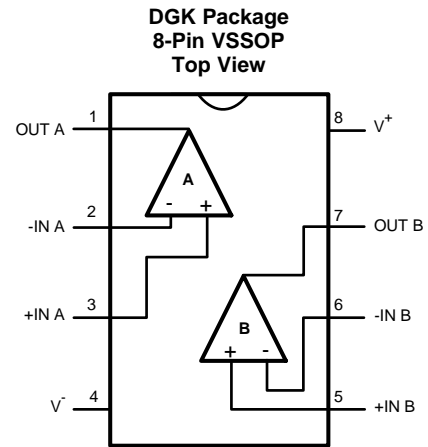
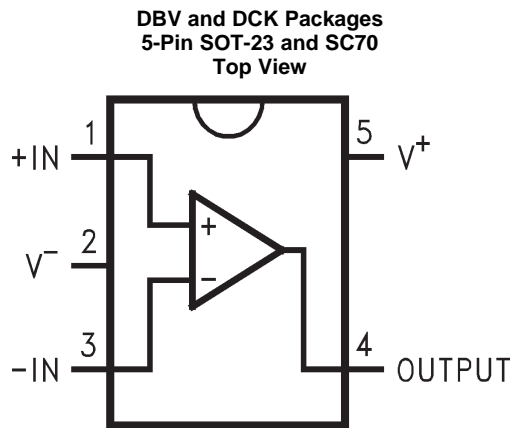
## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision G (February 2013) to Revision H</b>	<b>Page</b>
<ul style="list-style-type: none"> <li>• Added <i>ESD Ratings</i> table, <i>Feature Description</i> section, <i>Device Functional Modes</i>, <i>Application and Implementation</i> section, <i>Power Supply Recommendations</i> section, <i>Layout</i> section, <i>Device and Documentation Support</i> section, and <i>Mechanical, Packaging, and Orderable Information</i> section ..... 1</li> <li>• Changed values in the <i>Thermal Information</i> table to align with JEDEC standards ..... 5</li> </ul>	

<b>Changes from Revision F (February 2013) to Revision G</b>	<b>Page</b>
<ul style="list-style-type: none"> <li>• Changed layout of National Semiconductor Data Sheet to TI format. .... 18</li> </ul>	

## 5 Pin Configuration and Functions



**LMV551, LMV552, LMV554**

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[www.ti.com](http://www.ti.com)
**Pin Functions: LMV551**

PIN		TYPE <sup>(1)</sup>	DESCRIPTION
NAME	LMV551		
		SOT-23, SC70	
+IN	1	I	Noninverting Input
-IN	3	I	Inverting Input
OUT	4	O	Output
V-	2	P	Negative Supply
V+	5	P	Positive Supply

(1) I = Input; O = Output; P = Power

**Pin Functions: LMV552 and LMV554**

PIN			TYPE <sup>(1)</sup>	DESCRIPTION
NAME	LMV552	LMV554		
		SOIC, VSSOP	SOIC, TSSOP	
+IN A	3	3	I	Noninverting input, channel A
+IN B	5	5	I	Noninverting input, channel B
+IN C	—	10	I	Noninverting input, channel C
+IN D	—	12	I	Noninverting input, channel D
-IN A	2	2	I	Inverting input, channel A
-IN B	6	6	I	Inverting input, channel B
-IN C	—	9	I	Inverting input, channel C
-IN D	—	13	I	Inverting input, channel D
OUT A	1	1	O	Output, channel A
OUT B	7	7	O	Output, channel B
OUT C	—	8	O	Output, channel C
OUT D	—	14	O	Output, channel D
V+	8	4	P	Positive (highest) power supply
V-	4	11	P	Negative (lowest) power supply

(1) I = Input; O = Output; P = Power

## 6 Specifications

### 6.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted)<sup>(1)(2)</sup>

	MIN	MAX	UNIT
V <sub>IN</sub> Differential (at V <sup>+</sup> = 5 V)		±2.5	V
Supply voltage (V <sup>+</sup> – V <sup>-</sup> )		6	V
Voltage at input/output pins	V <sup>-</sup> –0.3	V <sup>+</sup> +0.3	V
Junction temperature, T <sub>J</sub> <sup>(3)</sup>		150	°C
Storage temperature, T <sub>stg</sub>	–65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office / Distributors for availability and specifications.
- (3) The maximum power dissipation is a function of T<sub>J(MAX)</sub>, θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is P<sub>D</sub> = (T<sub>J(MAX)</sub> – T<sub>A</sub>) / θ<sub>JA</sub>. All numbers apply for packages soldered directly onto a PC board.

### 6.2 ESD Ratings

		VALUE	UNIT	
V <sub>(ESD)</sub> Electrostatic discharge	Human-body model (HBM) <sup>(1)</sup>	±2000	V	
	Machine model (MM) <sup>(2)</sup>	LMV551		±100
		LMV552 / LMV554		±250

- (1) Human Body Model, applicable std. MIL-STD-883, Method 3015.7.
- (2) Machine Model, applicable std. JESD22-A115-A (ESD MM std. of JEDEC) Field-Induced Charge-Device Model, applicable std. JESD22-C101-C (ESD FICDM std. of JEDEC).

### 6.3 Recommended Operating Conditions

Over operating free-air temperature range (unless otherwise noted)

	MIN	NOM	MAX	UNIT
Temperature <sup>(1)</sup>	–40		125	°C
Supply voltage (V <sup>+</sup> – V <sup>-</sup> )	2.7		5.5	V

- (1) The maximum power dissipation is a function of T<sub>J(MAX)</sub>, θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is P<sub>D</sub> = (T<sub>J(MAX)</sub> – T<sub>A</sub>) / θ<sub>JA</sub>. All numbers apply for packages soldered directly onto a PC board.

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		LMV551		LMV552	LMV554	UNIT
		DBV (SOT-23)	DCK (SC70)	DGK (VSSOP)	PW (TSSOP)	
		5 PINS	5 PINS	8 PINS	14 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	213.6	303.5	200.3	134.9	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	174.8	135.5	89.1	60.9	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	72.6	81.1	120.9	77.3	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	56.6	8.4	21.7	11.5	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	72.2	80.4	119.4	76.7	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	n/a	n/a	n/a	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

## 6.5 Electrical Characteristics: 3 V

Unless otherwise specified, all limits are ensured for  $T_A = 25^\circ\text{C}$ ,  $V^+ = 3\text{ V}$ ,  $V^- = 0\text{ V}$ ,  $V_{\text{CM}} = V^+/2 = V_O$ . <sup>(1)</sup>

PARAMETER		TEST CONDITIONS		MIN <sup>(2)</sup>	TYP <sup>(2)</sup>	MAX <sup>(2)</sup>	UNIT	
$V_{\text{OS}}$	Input offset voltage	$T_A = 25^\circ\text{C}$			1	3	mV	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$				4.5		
TC $V_{\text{OS}}$	Input offset average drift	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			3.3		$\mu\text{V}/^\circ\text{C}$	
$I_B$	Input bias current <sup>(3)</sup>	$T_A = 25^\circ\text{C}$			20	38	nA	
$I_{\text{OS}}$	Input offset current	$T_A = 25^\circ\text{C}$			1	20	nA	
CMRR	Common mode rejection ratio	$0\text{ V} \leq V_{\text{CM}} \leq 2\text{ V}$	$T_A = 25^\circ\text{C}$		74	92	dB	
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		72			
PSRR	Power supply rejection ratio	$3 \leq V^+ \leq 5\text{ V}$ , $V_{\text{CM}} = 0.5\text{ V}$	LMV551 and LMV552	$T_A = 25^\circ\text{C}$		80	92	dB
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		78		
			LMV554	$T_A = 25^\circ\text{C}$		78	92	
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		76		
		$2.7 \leq V^+ \leq 5.5\text{ V}$ , $V_{\text{CM}} = 0.5\text{ V}$	LMV551 and LMV552	$T_A = 25^\circ\text{C}$		80	92	
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		78		
			LMV554	$T_A = 25^\circ\text{C}$		78	92	
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		76		
CMVR	Input common-mode voltage	CMRR $\geq 68\text{ dB}$	$T_A = 25^\circ\text{C}$		0	2.1	V	
		CMRR $\geq 60\text{ dB}$	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		0	2.1		
$A_{\text{VOL}}$	Large signal voltage gain	$0.4 \leq V_O \leq 2.6$ , $R_L = 100\text{ k}\Omega$ to $V^+/2$	LMV551 and LMV552	$T_A = 25^\circ\text{C}$		81	90	dB
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		78		
			LMV554	$T_A = 25^\circ\text{C}$		79	90	
				$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		77		
		$0.4 \leq V_O \leq 2.6$ , $R_L = 10\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$		71	80		
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		68			
$V_O$	Output swing high	$R_L = 100\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$		40	48	mV from rail	
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			58		
		$R_L = 10\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$		85	100		
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			120		
	Output swing low	$R_L = 100\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$		50	65		
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			77		
		$R_L = 10\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$		95	110		
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			130		
$I_{\text{SC}}$	Output short circuit current	Sourcing <sup>(4)</sup>			10		mA	
		Sinking <sup>(4)</sup>			25			
$I_S$	Supply current per amplifier	$T_A = 25^\circ\text{C}$			34	42	$\mu\text{A}$	
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$				52		
SR	Slew rate	$A_V = +1$ , 10% to 90% <sup>(5)</sup>			1		V/ $\mu\text{s}$	

- (1) Electrical Table values apply only for factor testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No guarantee of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J = T_A$ .
- (2) Limits are 100% production tested at  $25^\circ\text{C}$ . Limits over the operating temperature range are ensured through correlations using statistical quality control (SQC) method.
- (3) Positive current corresponds to current flowing into the device.
- (4) The part is not short-circuit protected and is not recommended for operation with heavy resistive loads.
- (5) Slew rate is the average of the rising and falling slew rates.

## Electrical Characteristics: 3 V (continued)

Unless otherwise specified, all limits are ensured for  $T_A = 25^\circ\text{C}$ ,  $V^+ = 3\text{ V}$ ,  $V^- = 0\text{ V}$ ,  $V_{\text{CM}} = V^+/2 = V_O$ .<sup>(1)</sup>

PARAMETER		TEST CONDITIONS	MIN <sup>(2)</sup>	TYP <sup>(2)</sup>	MAX <sup>(2)</sup>	UNIT
$\Phi_m$	Phase margin	$R_L = 10\text{ k}\Omega$ , $C_L = 20\text{ pF}$		75		°
GBW	Gain bandwidth product			3		MHz
$e_n$	Input-referred voltage noise	$f = 100\text{ kHz}$		70		$\text{nV}/\sqrt{\text{Hz}}$
		$f = 1\text{ kHz}$		70		
$i_n$	Input-referred current noise	$f = 100\text{ kHz}$		0.1		$\text{pA}/\sqrt{\text{Hz}}$
		$f = 1\text{ kHz}$		0.15		
THD	Total harmonic distortion	$f = 1\text{ kHz}$ , $A_V = 2$ , $R_L = 2\text{ k}\Omega$		0.003%		

## 6.6 Electrical Characteristics: 5 V

Unless otherwise specified, all limits are ensured for  $T_A = 25^\circ\text{C}$ ,  $V^+ = 5\text{ V}$ ,  $V^- = 0\text{ V}$ ,  $V_{\text{CM}} = V^+/2 = V_O$ .<sup>(1)</sup>

PARAMETER		TEST CONDITIONS	MIN <sup>(2)</sup>	TYP <sup>(3)</sup>	MAX <sup>(2)</sup>	UNIT
$V_{\text{OS}}$	Input offset voltage	$T_A = 25^\circ\text{C}$		1	3	mV
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			4.5	
TC $V_{\text{OS}}$	Input offset average drift	$T_A = 25^\circ\text{C}$		3.3		$\mu\text{V}/^\circ\text{C}$
$I_B$	Input bias current <sup>(4)</sup>	$T_A = 25^\circ\text{C}$		20	38	nA
$I_{\text{OS}}$	Input offset current			1	20	nA
CMRR	Common mode rejection ratio	$T_A = 25^\circ\text{C}$	76	93		nA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	74			
PSRR	Power supply rejection ratio	$3\text{ V} \leq V^+ \leq 5\text{ V}$ to $V_{\text{CM}} = 0.5\text{ V}$	$T_A = 25^\circ\text{C}$	78	90	dB
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	75		
		$2.7\text{ V} \leq V^+ \leq 5.5\text{ V}$ to $V_{\text{CM}} = 0.5\text{ V}$	$T_A = 25^\circ\text{C}$	78	90	
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	75		
CMVR	Input common-mode voltage	CMRR $\geq 68\text{ dB}$	$T_A = 25^\circ\text{C}$	0	4.1	V
		CMRR $\geq 60\text{ dB}$	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	0	4.1	
$A_{\text{VOL}}$	Large signal voltage gain	$0.4 \leq V_O \leq 4.6$ , $R_L = 100\text{ k}\Omega$ to $V^+/2$		78	90	dB
				75		
		$0.4 \leq V_O \leq 4.6$ , $R_L = 10\text{ k}\Omega$ to $V^+/2$		75	80	
$V_O$	Output swing high	$R_L = 100\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$	70	92	mV from rail
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		122	
		$R_L = 10\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$	125	155	
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		210	
	Output swing low	$R_L = 100\text{ k}\Omega$ to $V^+/2$	$T_A = 25^\circ\text{C}$	60	70	
			$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		82	
$I_{\text{SC}}$	Output short-circuit current	Sourcing <sup>(5)</sup>		10		mA
		Sinking <sup>(5)</sup>		25		
$I_S$	Supply current per amplifier	$T_A = 25^\circ\text{C}$		37	46	$\mu\text{A}$
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			54	

- (1) Electrical Table values apply only for factor testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No guarantee of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J = T_A$ .
- (2) Limits are 100% production tested at  $25^\circ\text{C}$ . Limits over the operating temperature range are ensured through correlations using statistical quality control (SQC) method.
- (3) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and also depend on the application and configuration. The typical values are not tested and are not ensured on shipped production material.
- (4) Positive current corresponds to current flowing into the device.
- (5) The part is not short-circuit protected and is not recommended for operation with heavy resistive loads.

**Electrical Characteristics: 5 V (continued)**

 Unless otherwise specified, all limits are ensured for  $T_A = 25^\circ\text{C}$ ,  $V^+ = 5\text{ V}$ ,  $V^- = 0\text{ V}$ ,  $V_{CM} = V^+/2 = V_O$ .<sup>(1)</sup>

PARAMETER		TEST CONDITIONS	MIN <sup>(2)</sup>	TYP <sup>(3)</sup>	MAX <sup>(2)</sup>	UNIT
SR	Slew rate	$A_V = +1$ , $V_O = 1\text{ V}_{PP}$ 10% to 90% <sup>(6)</sup>		1		V/ $\mu\text{s}$
$\Phi_m$	Phase margin	$R_L = 10\text{ k}\Omega$ , $C_L = 20\text{ pF}$		75		°
GBW	Gain bandwidth product			3		MHz
$e_n$	Input-referred voltage noise	$f = 100\text{ kHz}$		70		nV/ $\sqrt{\text{Hz}}$
		$f = 1\text{ kHz}$		70		
$I_n$	Input-referred current noise	$f = 100\text{ kHz}$		0.1		pA/ $\sqrt{\text{Hz}}$
		$f = 1\text{ kHz}$		0.15		
THD	Total harmonic distortion	$f = 1\text{ kHz}$ , $A_V = 2$ , $R_L = 2\text{ k}\Omega$		0.003%		

(6) Slew rate is the average of the rising and falling slew rates.

6.7 Typical Characteristics

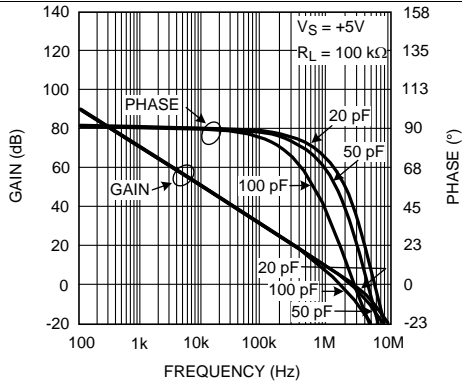


Figure 1. Open-Loop Gain and Phase With Capacitive Load

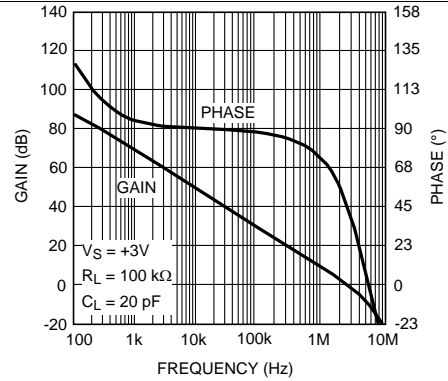


Figure 2. Open-Loop Gain and Phase With Resistive Load

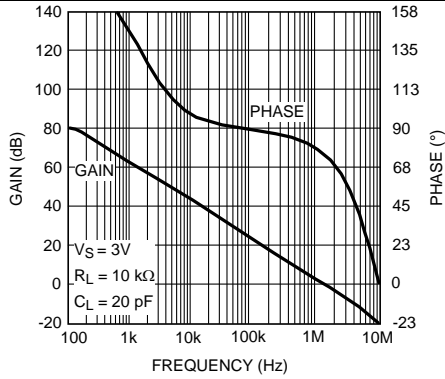


Figure 3. Open-Loop Gain and Phase With Resistive Load

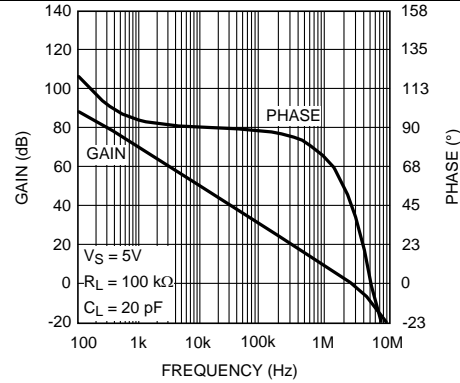


Figure 4. Open-Loop Gain and Phase With Resistive Load

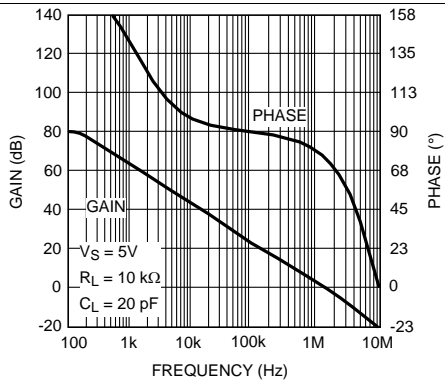


Figure 5. Open-Loop Gain and Phase With Resistive Load

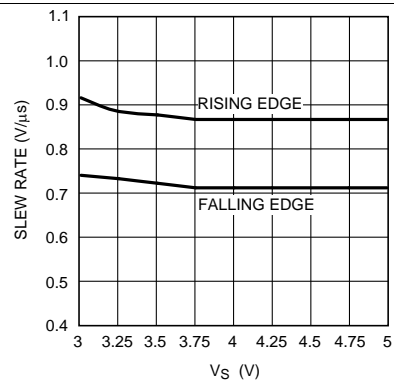
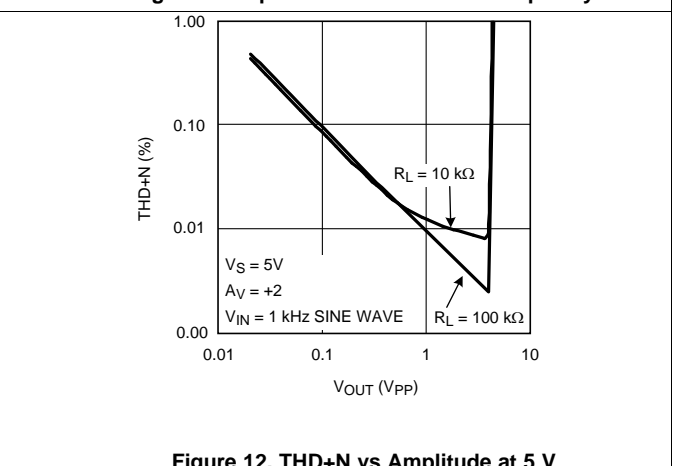
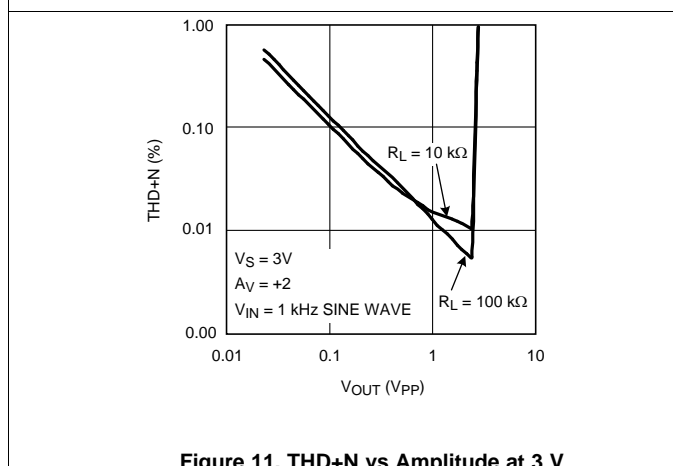
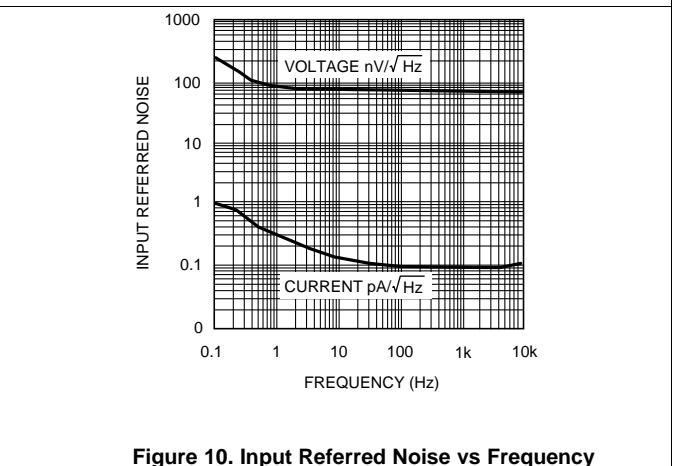
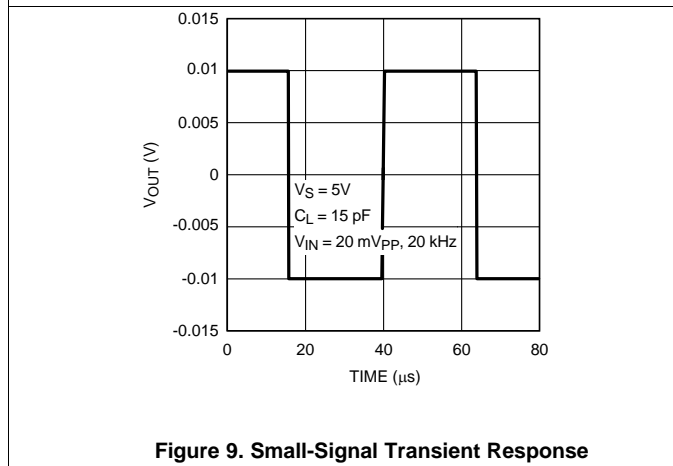
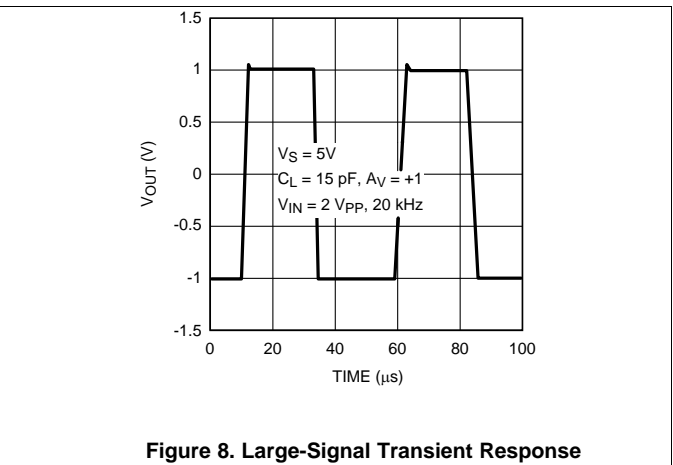
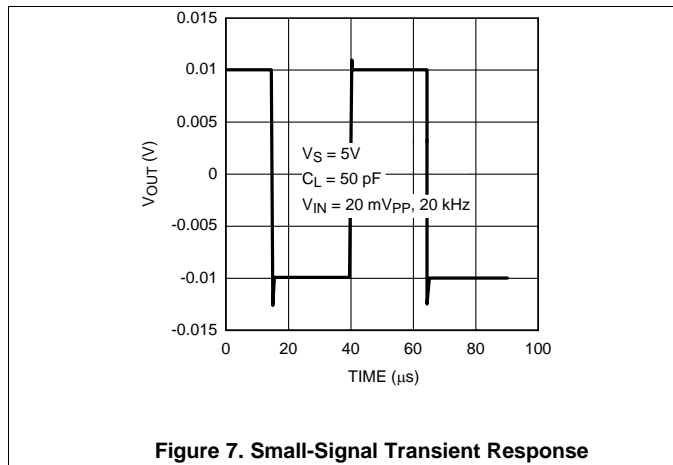


Figure 6. Slew Rate vs Supply voltage

Typical Characteristics (continued)



Typical Characteristics (continued)

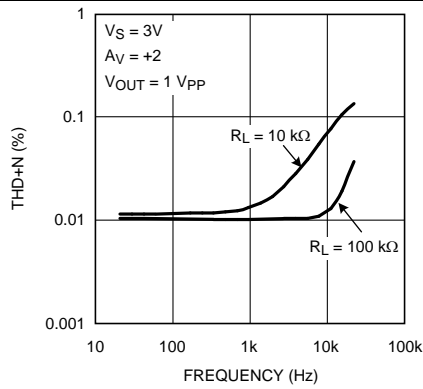


Figure 13. THD+N vs Amplitude

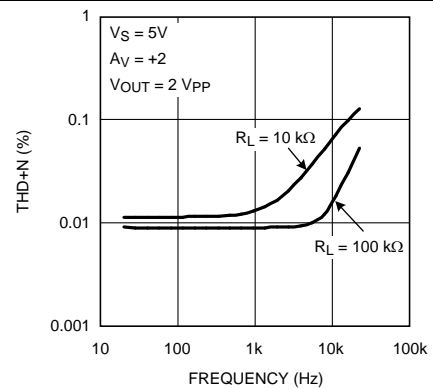


Figure 14. THD+N vs Amplitude

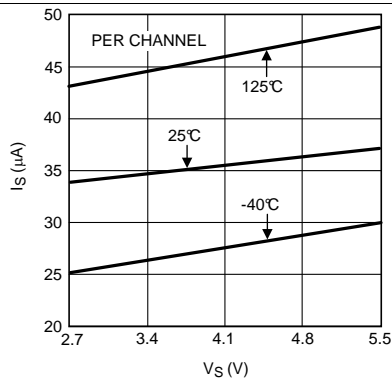


Figure 15. Supply Current vs Supply Voltage

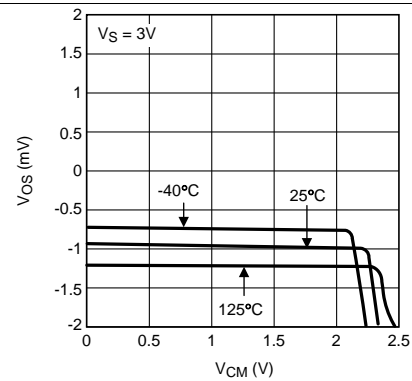


Figure 16. Vos vs VCM

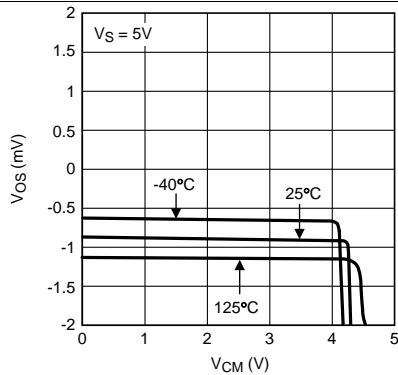


Figure 17. Vos vs VCM

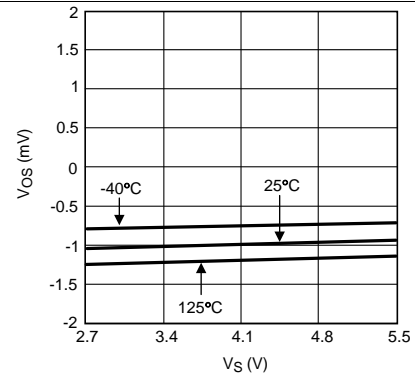
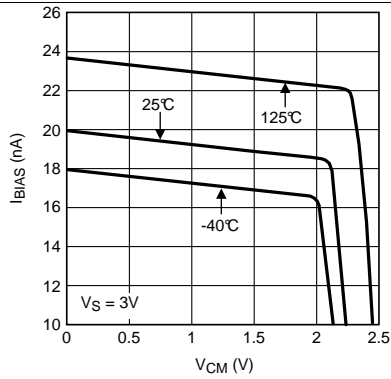
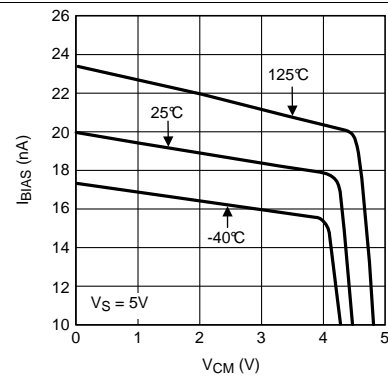
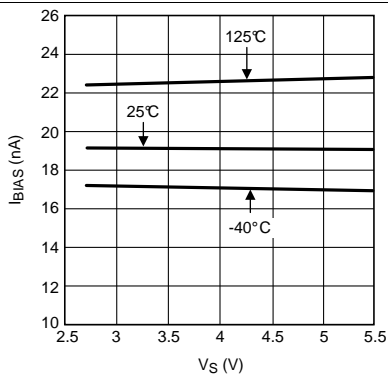
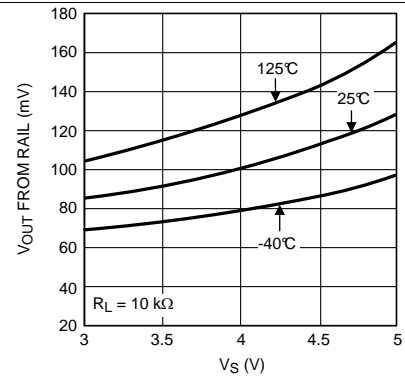
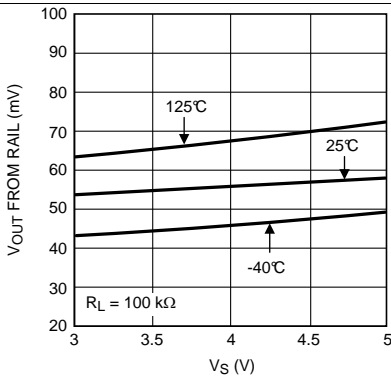
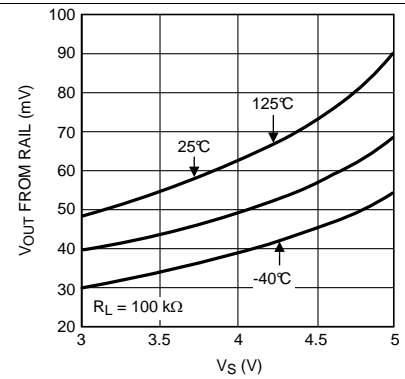
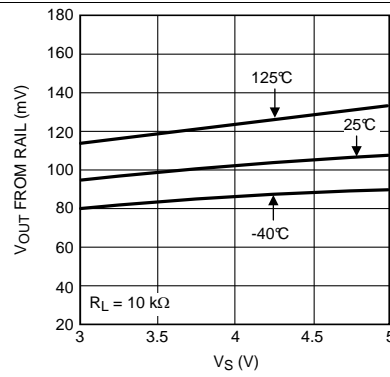


Figure 18. Vos vs Supply Voltage

**Typical Characteristics (continued)**

**Figure 19.  $I_{BIAS}$  vs  $V_{CM}$** 

**Figure 20.  $I_{BIAS}$  vs  $V_{CM}$** 

**Figure 21.  $I_{BIAS}$  vs Supply Voltage**

**Figure 22. Positive Output Swing vs Supply Voltage**

**Figure 23. Negative Output Swing vs Supply Voltage**

**Figure 24. Positive Output Swing vs Supply Voltage**

**Typical Characteristics (continued)**



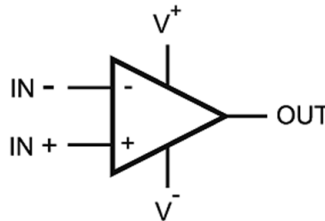
**Figure 25. Negative Output Swing vs Supply Voltage**

## 7 Detailed Description

### 7.1 Overview

The LMV55x are high performance, low power operational amplifiers implemented with TI's advanced VIP50 process. They feature 3 MHz of bandwidth while consuming only 37  $\mu\text{A}$  of current per amplifier, which is an exceptional bandwidth to power ratio in this op amp class. These amplifiers are unity gain stable and provide an excellent solution for low power applications requiring a wide bandwidth.

### 7.2 Functional Block Diagram



(Each Amplifier)

### 7.3 Feature Description

The differential inputs of the amplifier consist of a noninverting input (+IN) and an inverting input (–IN). The amplifier amplifies only the difference in voltage between the two inputs, which is called the differential input voltage. The output voltage of the op-amp  $V_{\text{OUT}}$  is given by [Equation 1](#):

$$V_{\text{OUT}} = A_{\text{OL}} (IN^+ - IN^-)$$

where

- $A_{\text{OL}}$  is the open-loop gain of the amplifier, typically around 100 dB (100,000x, or 10  $\mu\text{V}$  per volt). (1)

#### 7.3.1 Low Voltage and Low Power Operation

The LMV55x have performance ensured at supply voltages of 3 V and 5 V and are ensured to be operational at all supply voltages from 2.7 V to 5.5 V. For this supply voltage range, the LMV55x draw the extremely low supply current of less than 37  $\mu\text{A}$  per amp.

#### 7.3.2 Wide Bandwidth

The bandwidth to power ratio of 3 MHz to 37  $\mu\text{A}$  per amplifier is one of the best bandwidth to power ratios ever achieved. This makes these devices ideal for low power signal processing applications such as portable media players and instrumentation.

#### 7.3.3 Low Input Referred Noise

The LMV55x provide a flatband input referred voltage noise density of  $70 \text{ nV}/\sqrt{\text{Hz}}$ , which is significantly better than the noise performance expected from an ultra low power op amp. They also feature the exceptionally low 1/f noise corner frequency of 4 Hz. This noise specification makes the LMV55x ideal for low power applications such as PDAs and portable sensors.

#### 7.3.4 Ground Sensing and Rail-to-Rail Output

The LMV55x each have a rail-to-rail output stage, which provides the maximum possible output dynamic range. This is especially important for applications requiring a large output swing. The input common mode range includes the negative supply rail which allows direct sensing at ground in a single supply operation.

## Feature Description (continued)

### 7.3.5 Small Size

The small footprints of the LMV55x packages save space on printed circuit boards, and enable the design of smaller and more compact electronic products. Long traces between the signal source and the op amp make the signal path susceptible to noise. By using a physically smaller package, the amplifiers can be placed closer to the signal source, reducing noise pickup and enhancing signal integrity.

## 7.4 Device Functional Modes

### 7.4.1 Stability Of Op Amp Circuits

#### 7.4.1.1 Stability and Capacitive Loading

As seen in the Phase Margin vs Capacitive Load graph, the phase margin reduces significantly for  $C_L$  greater than 100 pF. This is because the op amp is designed to provide the maximum bandwidth possible for a low supply current. Stabilizing them for higher capacitive loads would have required either a drastic increase in supply current, or a large internal compensation capacitance, which would have reduced the bandwidth of the op amp. Hence, if the LMV55x are to be used for driving higher capacitive loads, they must be externally compensated.

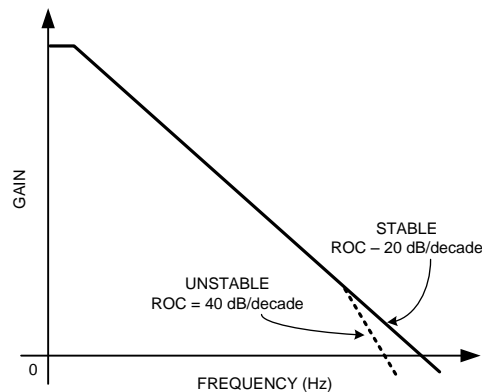


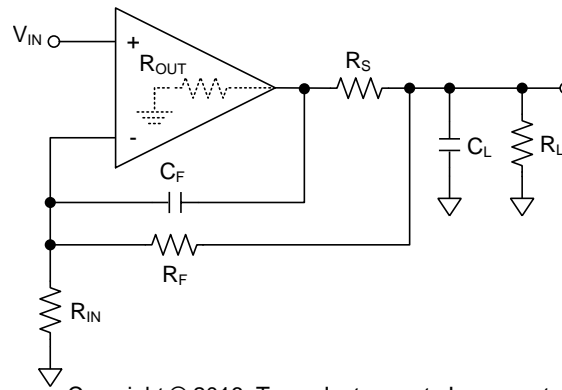
Figure 26. Gain vs Frequency for an Op Amp

An op amp, ideally, has a dominant pole close to DC, which causes its gain to decay at the rate of 20 dB/decade with respect to frequency. If this rate of decay, also known as the rate of closure (ROC), remains the same until the op amp's unity gain bandwidth, the op amp is stable. If, however, a large capacitance is added to the output of the op amp, it combines with the output impedance of the op amp to create another pole in its frequency response before its unity gain frequency (Figure 26). This increases the ROC to 40 dB/decade and causes instability.

In such a case a number of techniques can be used to restore stability to the circuit. The idea behind all these schemes is to modify the frequency response such that it can be restored to an ROC of 20 dB/decade, which ensures stability.

#### 7.4.1.1.1 In the Loop Compensation

Figure 27 illustrates a compensation technique, known as 'in the loop' compensation, that employs an RC feedback circuit within the feedback loop to stabilize a non-inverting amplifier configuration. A small series resistance,  $R_S$ , is used to isolate the amplifier output from the load capacitance,  $C_L$ , and a small capacitance,  $C_F$ , is inserted across the feedback resistor to bypass  $C_L$  at higher frequencies.

**Device Functional Modes (continued)**


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**Figure 27. In the Loop Compensation**

The values for  $R_S$  and  $C_F$  are decided by ensuring that the zero attributed to  $C_F$  lies at the same frequency as the pole attributed to  $C_L$ . This ensures that the effect of the second pole on the transfer function is compensated for by the presence of the zero, and that the ROC is maintained at 20 dB/decade. For the circuit shown in [Figure 27](#) the values of  $R_S$  and  $C_F$  are given by [Equation 2](#). Values of  $R_S$  and  $C_F$  required for maintaining stability for different values of  $C_L$ , as well as the phase margins obtained, are shown in [Table 1](#).  $R_F$ ,  $R_{IN}$ , and  $R_L$  are to be 10 k $\Omega$ , while  $R_{OUT}$  is 340 $\Omega$ .

$$R_S = \frac{R_{OUT}R_{IN}}{R_F}$$

$$C_F = \left(1 + \frac{1}{A_{CL}}\right) \left(\frac{R_F + 2R_{IN}}{R_F^2}\right) C_L R_{OUT} \quad (2)$$

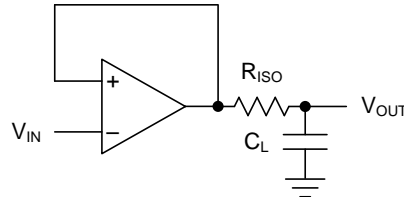
**Table 1. Phase Margins**

$C_L$ (pF)	$R_S$ ( $\Omega$ )	$C_F$ (pF)	PHASE MARGIN ( $^\circ$ )
50	340	8	47
100	340	15	42
150	340	22	40

Although this methodology provides circuit stability for any load capacitance, it does so at the price of bandwidth. The closed loop bandwidth of the circuit is now limited by  $R_F$  and  $C_F$ .

#### 7.4.1.1.2 Compensation by External Resistor

In some applications it is essential to drive a capacitive load without sacrificing bandwidth. In such a case, in the loop compensation is not viable. A simpler scheme for compensation is shown in [Figure 28](#). A resistor,  $R_{ISO}$ , is placed in series between the load capacitance and the output. This introduces a zero in the circuit transfer function, which counteracts the effect of the pole formed by the load capacitance and ensures stability. The value of  $R_{ISO}$  to be used should be decided depending on the size of  $C_L$  and the level of performance desired. Values ranging from 5  $\Omega$  to 50  $\Omega$  are usually sufficient to ensure stability. A larger value of  $R_{ISO}$  results in a system with less ringing and overshoot, but also limits the output swing and the short-circuit current of the circuit.



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**Figure 28. Compensation by Isolation Resistor**

## 8 Application and Implementation

### NOTE

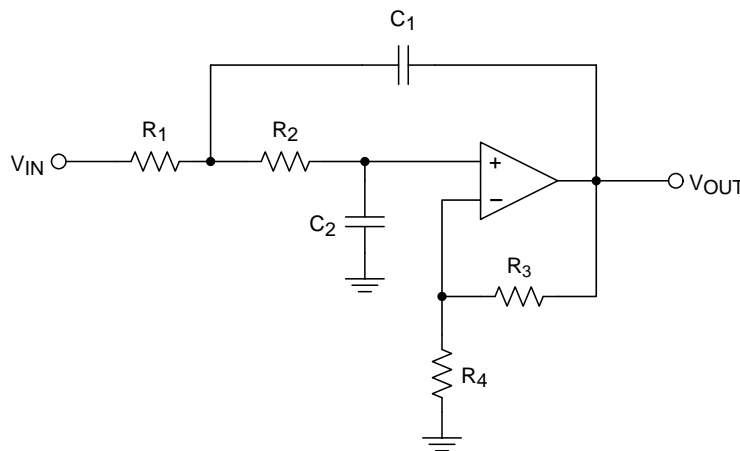
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The LMV55x have an operating supply voltage range from 2.7 V to 5.5 V. These amplifiers can operate over a wide temperature range ( $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ ), making them a great choice for automotive applications, sensor applications as well as portable instrumentation applications.

With a wide unity gain bandwidth of 3 MHz, low input referred noise density and an excellent BW to supply current ratio, the LMV55x are well suited for low-power filtering applications. Active filter topologies, such as the Sallen-Key low pass filter shown in Figure 29, are very versatile, and can be used to design a wide variety of filters (Chebyshev, Butterworth or Bessel). For best results, the amplifier must have a bandwidth that is eight to ten times the filter frequency bandwidth. Failure to follow this guideline can result in phase shift of the amplifier and premature roll-off. The Sallen-Key topology, in particular, can be used to attain a wide range of Q, by using positive feedback to reject the undesired frequency range.

### 8.2 Typical Application



**Figure 29. Two Pole Sallen-Key Low Pass Filter**

#### 8.2.1 Design Requirements

As a design example:

Require:  $A_{LP} = 10$ , less than 1dB passband ripple, and a cutoff frequency of 1kHz.

#### 8.2.2 Detailed Design Procedure

There are many resources discussing the Sallen-Key lowpass filter topology.

Texas Instruments has made filter design easy by creating on-line and stand alone design tools, such as Webench Filter Designer and Filter Pro Desktop.

For this design, the stand-alone Filter Pro Desktop is used.

For the design, the following parameters are entered into the Filterpro software:

1. Filter Type = Lowpass
2. Gain = 10 V/V (20dB)
3. Passband Frequency = 1 kHz

## Typical Application (continued)

4. Allowable Ripple = 1 dB
5. Filter Order = Checked and set to 2
6. Response Type = Butterworth
7. Filter Topology = Sallen-Key
8. Component Tolerance - Resistor = E96 1%
9. Component Tolerance - Capacitor = E6 20%

After entering these values, FilterPro returns the following recommended values:

1. R1 = 44.2 kΩ
2. R2 = 38.3 kΩ
3. R3 = 2.49 kΩ
4. R4 = 22.6 kΩ
5. C1 = 10 nF
6. C2 = 1.5 nF

The LMV55x is targeted for low power operation. The above resistor values are assumed for a *standard* power application. To save power, both quiescent and dynamic, the values of the resistors can be increased.

The largest consumer of power is the gain setting feedback resistors R3 and R4, as these are DC coupled and represent a constant DC load to the amplifier. If the output is biased at 2.5 V, then  $2.5 \text{ V} / (22.6 \text{ k} + 2.49 \text{ k}) = 99.6 \text{ } \mu\text{A}$  is flowing through the feedback network. This is significantly more than the 37uA quiescent current of the amplifier alone! Increasing the size of the feedback resistors by a decade from 22.6k to 226k, the current in the feedback network can be reduced down to 9.9uA.

Increasing the resistor values requires a proportional decrease in the values of the capacitors. If a resistor value is increased 10x, then the corresponding capacitor value must be decreased 10x. However, note that increasing the resistor values increases the contributed noise, and decreasing the capacitors to small values increases the sensitivity to stray capacitance.

There is a decision to be made about also scaling the filter components (R1, R2, C1 & C2). R1 and R2 are AC coupled to the output, so the only DC current flowing through these resistors is the input bias current of the LMV55x (typically 20 nA). However, large AC currents can flow through C2 and C1 during large signal swings. Scaling the filter components also reduces the peak AC signal currents. If the AC signals are expected to large (several Vpp) and frequent, then scaling the filter values may be beneficial to overall power consumption. If the expected AC signals are small, it may not be worth the noise tradeoff to scale these values.

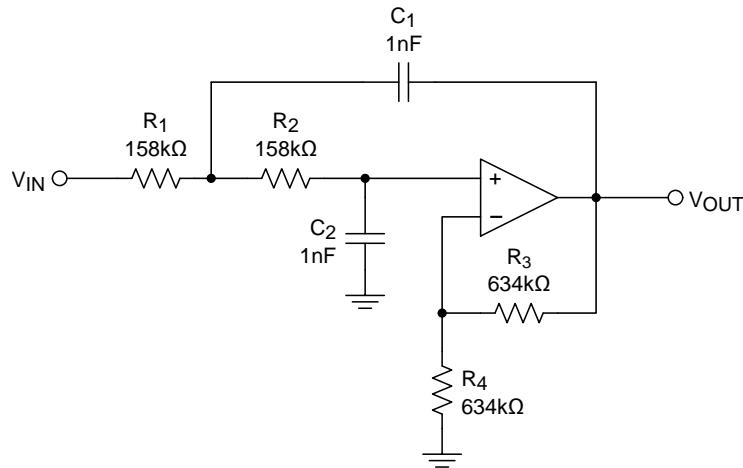
Because the LMV55x has a bipolar input, to maintain DC accuracy, the equivalent resistance seen by each amplifier input should be equal to cancel the bias current effects.

To maintain DC accuracy through bias current cancelling, the following relationship should be maintained:

$$(R1 + R2) = (R3 // R4) \quad (3)$$

Fortunately, the filter Pro software makes changing and recalculating the values easy. By changing the value of any of the filter components (R1, R2, C1 & C2) in the schematic tab, the program automatically recalculates and scale these components. Conversely, changing the gain feedback components (R3 or R4) also causes the other feedback resistor to scale. However, Filter Pro does NOT maintain the relationship between the feedback and filter elements as described in [Equation 3](#) above. The feedback resistor values can be 'seeded' and scaled appropriately, as long as the original feedback resistor ratio is maintained.

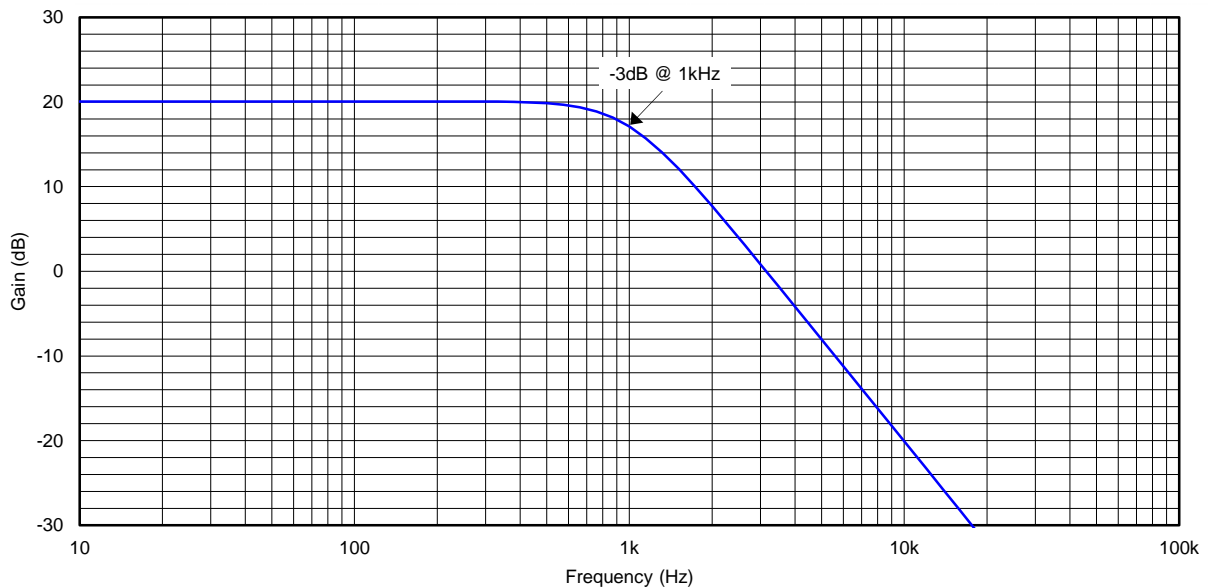
## Typical Application (continued)



**Figure 30. 1kHz Sallen-Key Low Pass Filter with Values**

### 8.2.3 Application Curve

Figure 31 shows the simulated results of the example 1-KHz Sallen-Key Low Pass Filter.



**Figure 31. 1KHz, 2-Pole Sallen-Key Low Pass Filter Results**

### 8.3 Do's and Don'ts

Do properly bypass the power supplies.

Do add series resistance to the output when driving capacitive loads, particularly cables, Muxes and ADC inputs.

Do add series current limiting resistors and external Schottky clamp diodes if input voltage is expected to exceed the supplies. Limit the current to 1 mA or less (1 kΩ per volt).

## 9 Power Supply Recommendations

For proper operation, the power supplies must be properly decoupled. For decoupling the supply lines, TI recommends that 10-nF capacitors be placed as close as possible to the op amp power supply pins. For single-supply, place a capacitor between  $V^+$  and  $V^-$  supply leads. For dual supplies, place one capacitor between  $V^+$  and ground, and one capacitor between  $V^-$  and ground.

## 10 Layout

### 10.1 Layout Guidelines

The  $V^+$  pin should be bypassed to ground with a low-ESR capacitor.

The optimum placement is closest to the  $V^+$  and ground pins.

Take care to minimize the loop area formed by the bypass capacitor connection between  $V^+$  and ground.

The ground pin should be connected to the PCB ground plane at the pin of the device.

The feedback components should be placed as close to the device as possible minimizing strays.

### 10.2 Layout Example

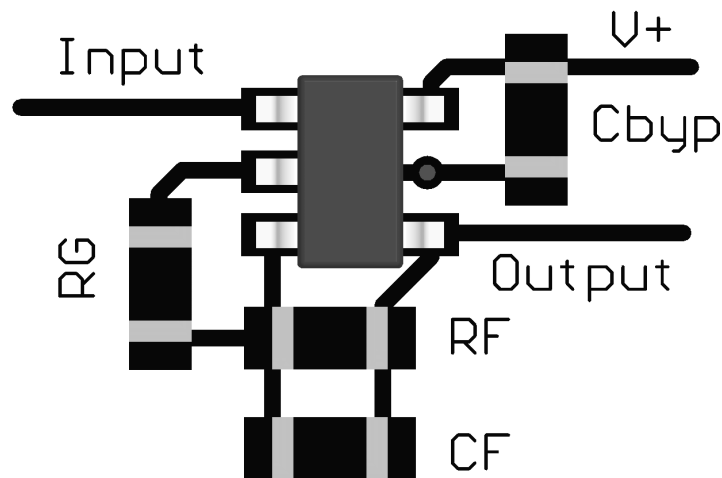


Figure 32. SOT-23 Layout Example

## 11 Device and Documentation Support

### 11.1 Device Support

#### 11.1.1 Development Support

[LMV551 PSPICE Model](#) (SNOM060)

[LMV552 PSPICE Model](#) (SNOM061)

[LMV554 PSPICE Model](#) (SNOM062)

[TINA-TI SPICE-Based Analog Simulation Program](#)

[DIP Adapter Evaluation Module](#)

[TI Universal Operational Amplifier Evaluation Module](#)

[TI Filterpro Software](#)

### 11.2 Documentation Support

#### 11.2.1 Related Documentation

For additional applications, see the following: [AN-31 Op Amp Circuit Collection](#) (SNLA140)

### 11.3 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

**Table 2. Related Links**

PARTS	PRODUCT FOLDER	SAMPLE & BUY	TECHNICAL DOCUMENTS	TOOLS & SOFTWARE	SUPPORT & COMMUNITY
LMV551	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>
LMV552	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>
LMV554	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>	<a href="#">Click here</a>

### 11.4 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 11.5 Community Resource

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 11.6 Trademarks

E2E is a trademark of Texas Instruments.

All other trademarks are the property of their respective owners.

## 11.7 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

## 11.8 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LMV551MF/NOPB	ACTIVE	SOT-23	DBV	5	1000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	AF3A	<a href="#">Samples</a>
LMV551MFX/NOPB	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	AF3A	<a href="#">Samples</a>
LMV551MG/NOPB	ACTIVE	SC70	DCK	5	1000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	A94	<a href="#">Samples</a>
LMV551MGX/NOPB	ACTIVE	SC70	DCK	5	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	A94	<a href="#">Samples</a>
LMV552MM/NOPB	ACTIVE	VSSOP	DGK	8	1000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	AH3A	<a href="#">Samples</a>
LMV552MMX/NOPB	ACTIVE	VSSOP	DGK	8	3500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	AH3A	<a href="#">Samples</a>
LMV554MT/NOPB	ACTIVE	TSSOP	PW	14	94	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	LMV55 4MT	<a href="#">Samples</a>
LMV554MTX/NOPB	ACTIVE	TSSOP	PW	14	2500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	LMV55 4MT	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMV551MF/NOPB	SOT-23	DBV	5	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LMV551MFX/NOPB	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LMV551MG/NOPB	SC70	DCK	5	1000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LMV551MGX/NOPB	SC70	DCK	5	3000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LMV552MM/NOPB	VSSOP	DGK	8	1000	178.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LMV552MMX/NOPB	VSSOP	DGK	8	3500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LMV554MTX/NOPB	TSSOP	PW	14	2500	330.0	12.4	6.95	5.6	1.6	8.0	12.0	Q1

**TAPE AND REEL BOX DIMENSIONS**

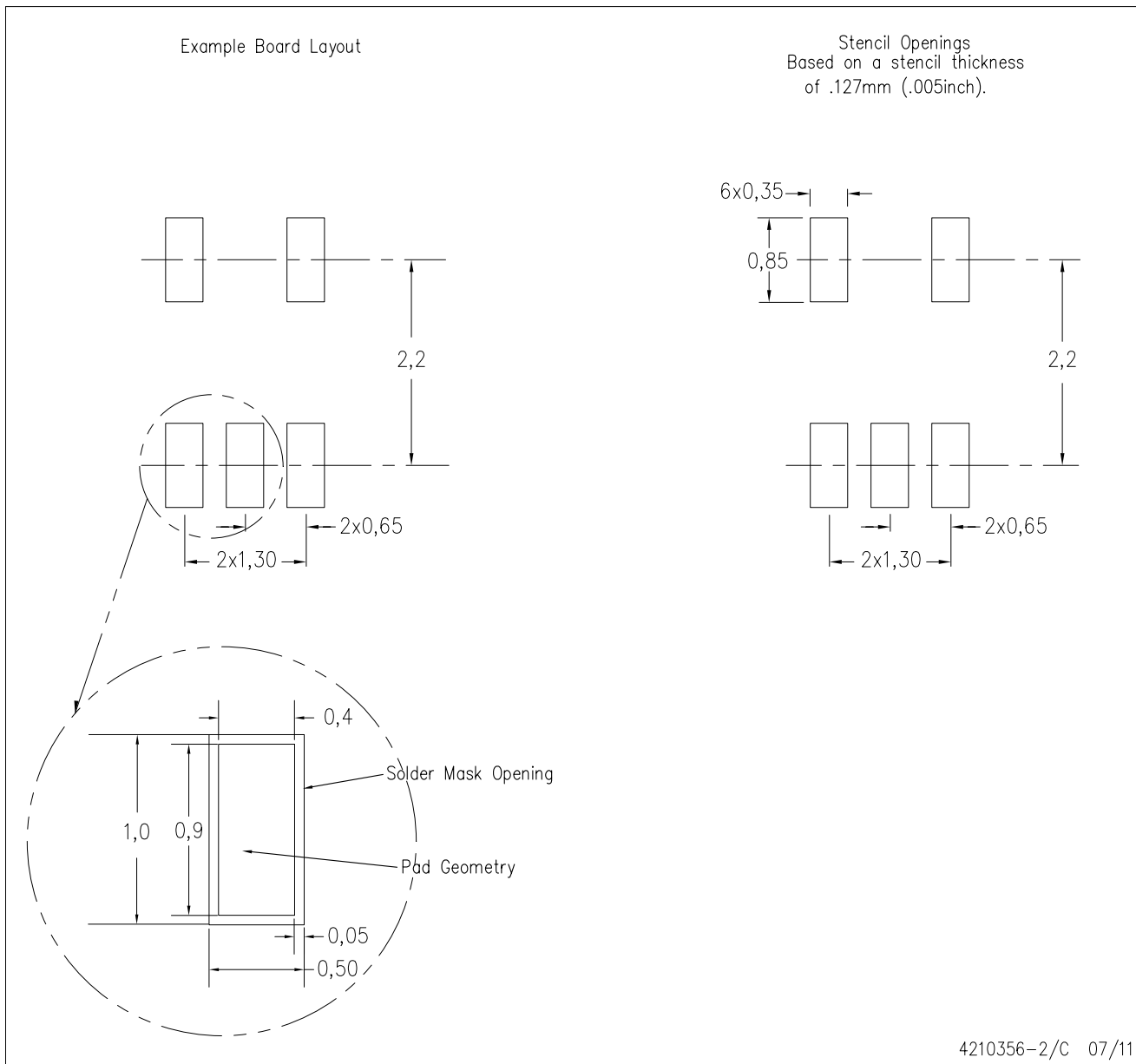

\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LMV551MF/NOPB	SOT-23	DBV	5	1000	210.0	185.0	35.0
LMV551MFX/NOPB	SOT-23	DBV	5	3000	210.0	185.0	35.0
LMV551MG/NOPB	SC70	DCK	5	1000	210.0	185.0	35.0
LMV551MGX/NOPB	SC70	DCK	5	3000	210.0	185.0	35.0
LMV552MM/NOPB	VSSOP	DGK	8	1000	210.0	185.0	35.0
LMV552MMX/NOPB	VSSOP	DGK	8	3500	367.0	367.0	35.0
LMV554MTX/NOPB	TSSOP	PW	14	2500	367.0	367.0	35.0



DCK (R-PDSO-G5)

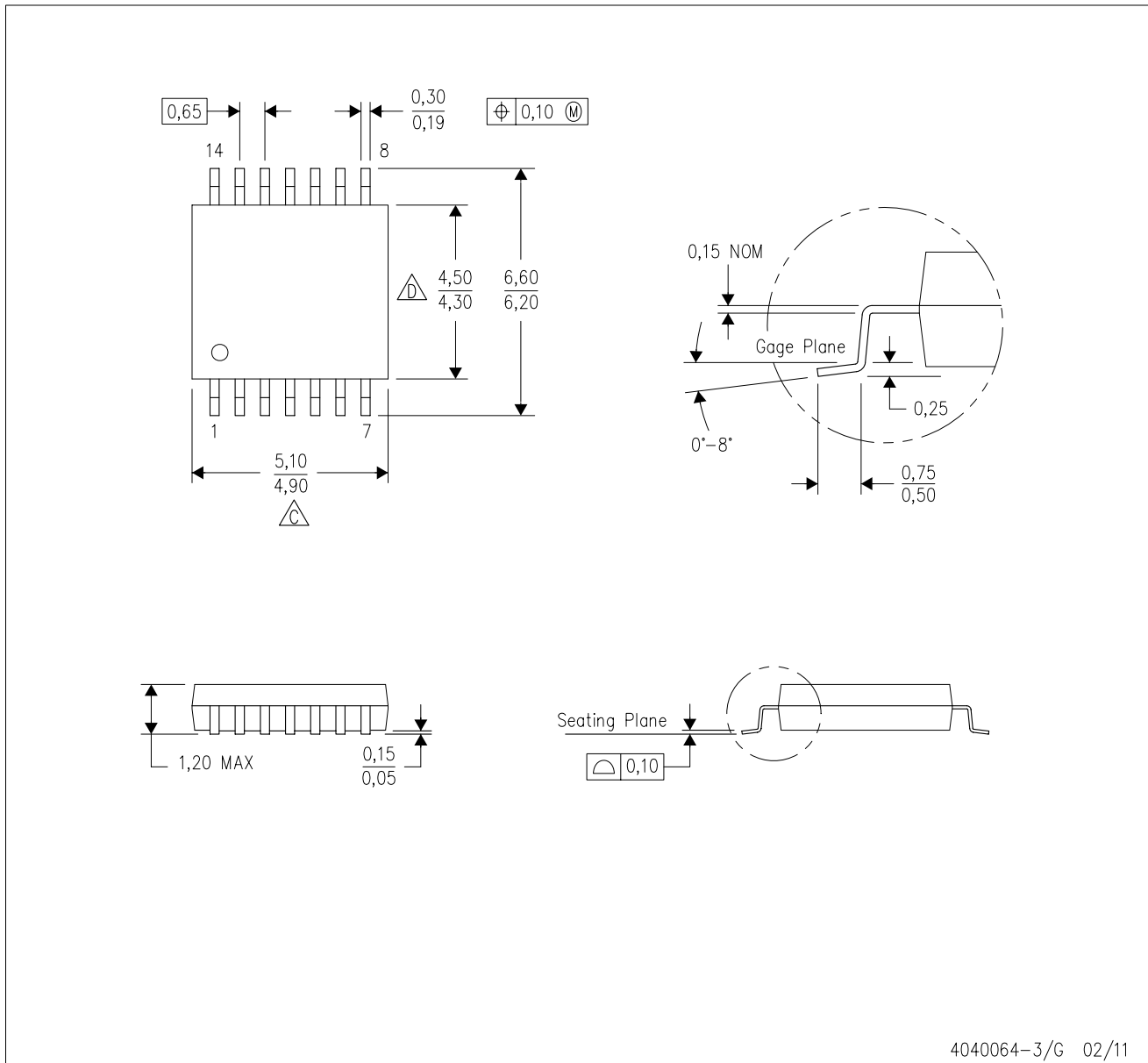
PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



4040064-3/G 02/11

- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  - C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
  - D. Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
  - E. Falls within JEDEC MO-153

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



4211284-2/G 08/15

- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.





# EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/D 11/2018

NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.





- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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