



# THE DATASHEET OF INA823DT



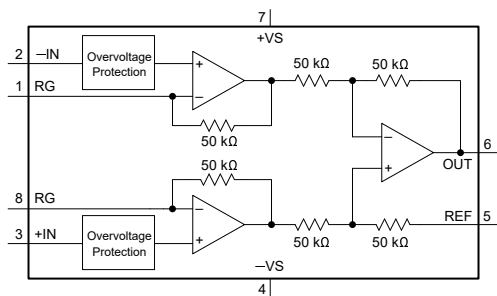
# INA823 Precision, Low-Power, Wide-Supply (2.7-V to 36-V) Instrumentation Amplifier

## 1 Features

- Input overvoltage protection up to  $\pm 60$  V
- Input voltage extends 150 mV below negative supply
- Low power supply current: 180  $\mu$ A (typ)
- Precision performance:
  - Low offset voltage: 20  $\mu$ V (typ), 100  $\mu$ V (max)
  - Low input bias current: 8 nA (max)
  - Common-mode rejection:
    - 84 dB,  $G = 1$  (min)
    - 104 dB,  $G = 10$  (min)
    - 120 dB,  $G \geq 100$  (min)
  - Power supply rejection: 100 dB,  $G = 1$  (min)
- Input voltage noise: 21 nV/ $\sqrt{\text{Hz}}$
- Bandwidth: 1.9 MHz ( $G = 1$ ), 60 kHz ( $G = 100$ )
- Stable with 1-nF capacitive loads
- Supply range:
  - Single-supply: 2.7 V to 36 V
  - Dual-supply:  $\pm 1.35$  V to  $\pm 18$  V
- Specified temperature range:  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$
- Packages: 8-pin SOIC and 8-pin VSSOP

## 2 Applications

- [Flow transmitter](#)
- [Wearable fitness and activity monitor](#)
- [Infusion pump](#)
- [Blood glucose monitor](#)
- [Electrocardiogram \(ECG\)](#)
- [Surgical equipment](#)
- [Weigh scale](#)
- [Analog input module](#)
- [Process analytics \(pH, gas, concentration, force and humidity\)](#)
- [Battery test](#)



**INA823 Simplified Internal Schematic**

## 3 Description

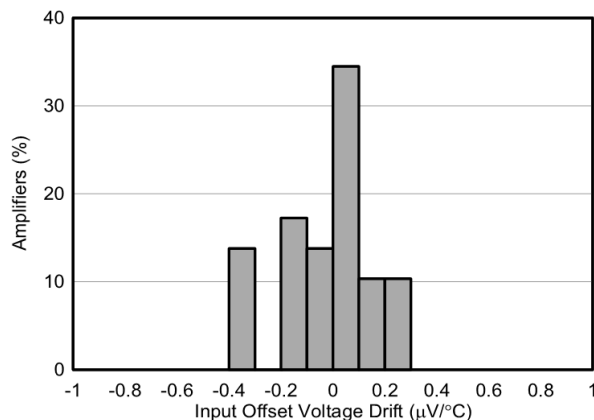
The INA823 is an integrated instrumentation amplifier that offers low power consumption and operates over a wide, single-supply or dual-supply range. A single external resistor sets any gain from 1 to 10,000. The device provides low input offset voltage, low offset voltage drift, low input bias current, and low current noise while remaining cost-effective. Additional circuitry protects the inputs against overvoltage up to  $\pm 60$  V.

The INA823 is optimized to provide a high common-mode rejection ratio. At  $G = 1$ , the common-mode rejection ratio exceeds 84 dB across the full input common-mode range. The INA823 has a wide common-mode voltage range as low as 150-mV below negative supply. The device is designed for low-voltage operation from a 2.7-V single supply, and dual supplies up to  $\pm 18$  V. The low power and single supply operation enable hand-held, battery-operated systems.

### Device Information

PART NUMBER	PACKAGE <sup>(1)</sup>	BODY SIZE (NOM)
INA823	SOIC (8)	4.90 mm × 3.91 mm
	VSSOP (8)	3.00 mm × 3.00 mm

- (1) For all available packages, see the package option addendum at the end of the data sheet.



**Typical Distribution of  
Input Stage Offset Voltage Drift**



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## 4 Revision History

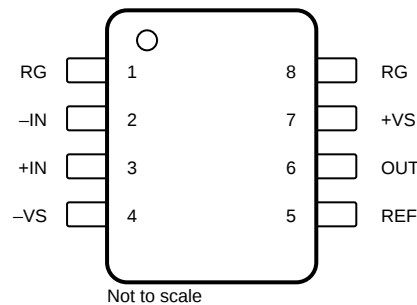
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision A (April 2019) to Revision B (November 2021)</b>	<b>Page</b>
• Changed device from advanced information (preview) to production data (active) .....	<b>1</b>

## 5 Device Comparison Table

DEVICE	DESCRIPTION	GAIN EQUATION	RG AT PINS
INA849	1-nV/ $\sqrt{\text{Hz}}$ Noise, 35- $\mu\text{V}$ Offset, 0.4 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 28-MHz Bandwidth, Precision Instrumentation Amplifier	$G = 1 + 6 \text{ k}\Omega / \text{RG}$	2, 3
INA821	35- $\mu\text{V}$ Offset, 0.4 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 7-nV/ $\sqrt{\text{Hz}}$ Noise, High-Bandwidth, Precision Instrumentation Amplifier	$G = 1 + 49.4 \text{ k}\Omega / \text{RG}$	2, 3
INA819	35- $\mu\text{V}$ Offset, 0.4 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 8-nV/ $\sqrt{\text{Hz}}$ Noise, Low-Power, Precision Instrumentation Amplifier	$G = 1 + 50 \text{ k}\Omega / \text{RG}$	2, 3
INA826	200- $\mu\text{A}$ Supply Current, 3-V to 36-V Supply Instrumentation Amplifier With Rail-to-Rail Output	$G = 1 + 49.4 \text{ k}\Omega / \text{RG}$	2, 3
INA818	35- $\mu\text{V}$ Offset, 0.4 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 8-nV/ $\sqrt{\text{Hz}}$ Noise, Low-Power, Precision Instrumentation Amplifier	$G = 1 + 50 \text{ k}\Omega / \text{RG}$	1, 8
INA828	50- $\mu\text{V}$ Offset, 0.5 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 7-nV/ $\sqrt{\text{Hz}}$ Noise, Low-Power, Precision Instrumentation Amplifier	$G = 1 + 50 \text{ k}\Omega / \text{RG}$	1, 8
INA333	25- $\mu\text{V}$ $V_{\text{OS}}$ , 0.1 $\mu\text{V}/^\circ\text{C}$ $V_{\text{OS}}$ Drift, 1.8-V to 5-V, RRO, 50- $\mu\text{A}$ $I_{\text{Q}}$ , Chopper-Stabilized INA	$G = 1 + 100 \text{ k}\Omega / \text{RG}$	1, 8
PGA280	1/8 V/V to 128 V/V Programmable Gain Instrumentation Amplifier With 3-V or 5-V Differential Output; Analog Supply up to $\pm 18$ V	Digital programmable	N/A
INA159	$G = 0.2$ V Differential Amplifier for $\pm 10$ -V to 3-V and 5-V Conversion	$G = 0.2 \text{ V/V}$	N/A
PGA112	Precision Programmable Gain Op Amp With SPI	Digital programmable	N/A

## 6 Pin Configuration and Functions



**Figure 6-1. D (8-Pin SOIC) and DGK (8-Pin VSSOP) Packages, Top View**

**Table 6-1. Pin Functions**

PIN		TYPE	DESCRIPTION
NAME	NO.		
-IN	2	Input	Negative (inverting) input
+IN	3	Input	Positive (noninverting) input
OUT	6	Output	Output
REF	5	Input	Reference input. This pin must be driven by a low impedance source.
RG	1, 8	—	Gain setting pin. Place a gain resistor between pin 1 and pin 8.
-VS	4	Power	Negative supply
+VS	7	Power	Positive supply

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>S</sub>	-V <sub>S</sub> , +V <sub>S</sub> pins voltage	Dual supply, V <sub>S</sub> = (+V <sub>S</sub> ) – (-V <sub>S</sub> )	± 20	V
		Single supply, V <sub>S</sub> = (+V <sub>S</sub> )	40	
	IN pins voltage	(-V <sub>S</sub> ) – 60	(+V <sub>S</sub> ) + 60	V
	RG, REF, OUT pins voltage	(-V <sub>S</sub> ) – 0.5	(+V <sub>S</sub> ) + 0.5	V
	RG pins current	-10	10	mA
	OUT pin current	-50	50	mA
I <sub>SC</sub>	Output short-circuit current <sup>(2)</sup>	Continuous		
T <sub>A</sub>	Operating temperature	-50	150	°C
T <sub>J</sub>	Junction temperature		175	°C
T <sub>stg</sub>	Storage temperature	-65	150	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) Short-circuit to V<sub>S</sub> / 2.

### 7.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±750

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
V <sub>S</sub>	Supply voltage	Single supply, V <sub>S</sub> = (+V <sub>S</sub> )	2.7	36
		Dual supply, V <sub>S</sub> = (+V <sub>S</sub> ) – (-V <sub>S</sub> )	±1.35	±18
T <sub>A</sub>	Specified temperature	-40	125	°C

### 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		INA823		UNIT
		D (SOIC)	DGK (VSSOP)	
		8 PINS	8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	126.7	167.5	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	67.0	60.3	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	70.1	88.7	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	18.6	7.9	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	69.4	87.1	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	n/a	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

## 7.5 Electrical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>INPUT</b>							
$V_{OSI}$	Input stage offset voltage <sup>(1) (3)</sup>	$T_A = -40^\circ\text{C to } +125^\circ\text{C}^{(2)}$			20	100	$\mu\text{V}$
						190	
$V_{OSO}$	Output stage offset voltage <sup>(1) (3)</sup>	$T_A = -40^\circ\text{C to } +125^\circ\text{C}^{(2)}$			0.2	1.2	$\mu\text{V}/^\circ\text{C}$
					140	450	$\mu\text{V}$
PSRR	Power-supply rejection ratio	$V_S = \pm 1.35\text{ V to } \pm 18\text{ V}$		G = 1, RTI	100	130	dB
				G = 10, RTI	115	148	
				G = 100, RTI	120	148	
				G = 1000, RTI	120	148	
$Z_{IN}$	Input impedance			12    8.5		$\text{G}\Omega$    pF	
	RFI filter, -3-dB frequency			20		MHz	
$V_{CM}$	Operating input voltage <sup>(4)</sup>	$V_S = \pm 1.35\text{ V to } \pm 18\text{ V}$ $T_A = -40^\circ\text{C to } +125^\circ\text{C}$		$(-V_S) - 0.15$		$(+V_S) - 1$	V
				See <a href="#">Figure 7-53</a>			
	Input overvoltage	$T_A = -40^\circ\text{C to } +125^\circ\text{C}^{(2)}$				$\pm 60$	V
CMRR	Common-mode rejection ratio	At dc to 60 Hz, RTI, $V_{CM} = (V_-) - 0.15\text{ V to } (V_+) - 1\text{ V}$ , G = 1		84	110	dB	
		At dc to 60 Hz, RTI, $V_{CM} = (V_-) - 0.15\text{ V to } (V_+) - 1\text{ V}$ , G = 10		104	136		
		At dc to 60 Hz, RTI, $V_{CM} = (V_-) - 0.15\text{ V to } (V_+) - 1\text{ V}$ , G $\geq 100$		120	149		
<b>BIAS CURRENT</b>							
$I_B$	Input bias current	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$			1.2	8	nA
					2.4		
					15	$\text{pA}/^\circ\text{C}$	
$I_{OS}$	Input offset current	$T_A = -40^\circ\text{C to } +125^\circ\text{C}$			0.4	4	nA
					0.8		
					4	$\text{pA}/^\circ\text{C}$	
<b>NOISE VOLTAGE</b>							
$e_{NI}$	Input stage voltage noise density <sup>(6)</sup>	f = 1 kHz, G = 1000, $R_S = 0\ \Omega$			21		$\text{nV}/\sqrt{\text{Hz}}$
	Input stage voltage noise <sup>(6)</sup>	$f_B = 0.1\text{ Hz to } 10\text{ Hz}$ , G = 1000, $R_S = 0\ \Omega$			0.4		$\mu\text{V}_{PP}$
$e_{NO}$	Output stage voltage noise density <sup>(6)</sup>	f = 1 kHz, $R_S = 0\ \Omega$			120		$\text{nV}/\sqrt{\text{Hz}}$
	Output stage voltage noise <sup>(6)</sup>	$f_B = 0.1\text{ Hz to } 10\text{ Hz}$ , $R_S = 0\ \Omega$			5		$\mu\text{V}_{PP}$
$i_n$	Current noise density	f = 1 kHz			160		$\text{fA}/\sqrt{\text{Hz}}$
	Current noise	$f_B = 0.1\text{ Hz to } 10\text{ Hz}$ , G = 100			5		$\text{pA}_{PP}$

## 7.5 Electrical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>GAIN</b>							
	Gain equation			1 + (100 k $\Omega$ / R <sub>G</sub> )			V/V
G	Gain			1		10000	V/V
GE	Gain error <sup>(5)</sup>	V <sub>O</sub> = $\pm 10\text{ V}$	G = 1		$\pm 0.01$	$\pm 0.04$	%
			G = 10		$\pm 0.025$	$\pm 0.2$	
			G = 100		$\pm 0.025$	$\pm 0.2$	
			G = 1000		$\pm 0.05$	$\pm 0.2$	
	Gain drift <sup>(5)</sup>	T <sub>A</sub> = $-40^\circ\text{C}$ to $+125^\circ\text{C}$	G = 1		$\pm 0.2$	$\pm 5$	ppm/ $^\circ\text{C}$
			G > 1		$\pm 12$	$\pm 35$	
	Gain nonlinearity	G = 1 to 10			2	10	ppm
		G > 10			5		
		G = 1 to 100, R <sub>L</sub> = 2 k $\Omega$			15		
<b>OUTPUT</b>							
	Output voltage swing			(-V <sub>S</sub> ) + 0.15		(+V <sub>S</sub> ) - 0.15	V
	Load capacitance	Stable operation			1000		pF
Z <sub>OUT</sub>	Closed-loop output impedance			See Figure 7-37			$\Omega$
I <sub>SC</sub>	Short-circuit current	Continuous to V <sub>S</sub> / 2			$\pm 20$		mA
<b>FREQUENCY RESPONSE</b>							
BW	Bandwidth, -3 dB	G = 1			1.9		MHz
		G = 10			350		kHz
		G = 100			60		
		G = 1000			6		
SR	Slew rate	G = 1, V <sub>O</sub> = $\pm 10\text{ V}$			0.9		V/ $\mu\text{s}$
t <sub>S</sub>	Settling time	To 0.01%	G = 1 to 10, V <sub>STEP</sub> = 10 V			12	$\mu\text{s}$
			G = 100, V <sub>STEP</sub> = 10 V			28	
			G = 1000, V <sub>STEP</sub> = 10 V			260	
		To 0.001%	G = 1 to 10, V <sub>STEP</sub> = 10 V			14	
			G = 100, V <sub>STEP</sub> = 10 V			33	
			G = 1000, V <sub>STEP</sub> = 10 V			290	
<b>REFERENCE INPUT</b>							
R <sub>IN</sub>	Input impedance				100		k $\Omega$
	Reference input voltage			(-V <sub>S</sub> )		(+V <sub>S</sub> )	V
	Gain to output				1		V/V
	Reference gain error	inside the output voltage swing			0.01	0.05	%
<b>POWER SUPPLY</b>							
I <sub>Q</sub>	Quiescent current	V <sub>IN</sub> = 0 V			180	250	$\mu\text{A}$
			T <sub>A</sub> = $-40^\circ\text{C}$ to $+125^\circ\text{C}$			300	

- (1) Total offset, referred-to-input (RTI):  $V_{OS} = (V_{OSI}) + (V_{OSO} / G)$ .
- (2) Specified by characterization.
- (3) Offset drifts are uncorrelated. Input-referred offset drift is calculated using:  $\Delta V_{OS(RTI)} = \sqrt{[\Delta V_{OSI}]^2 + (\Delta V_{OSO} / G)^2}$ .
- (4) Input voltage range of the instrumentation amplifier input stage. The input range depends on the common-mode voltage, differential voltage, gain, and reference voltage. See *Typical Characteristic* curves for more information.
- (5) The values specified for  $G > 1$  do not include the effects of the external gain-setting resistor, R<sub>G</sub>.
- (6) Total RTI voltage noise is equal to:  $e_{N(RTI)} = \sqrt{[e_{NI}]^2 + (e_{NO} / G)^2}$ .

## 7.6 Typical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

**Table 7-1. Table of Graphs**

FIGURE TITLE	FIGURE NUMBER
<b>Typical Distribution Graphs</b>	
Typical Distribution of Input Stage Offset Voltage	<a href="#">Figure 7-1</a>
Typical Distribution of Input Stage Offset Voltage Drift	<a href="#">Figure 7-2</a>
Typical Distribution of Output Stage Offset Voltage	<a href="#">Figure 7-3</a>
Typical Distribution of Output Stage Offset Voltage Drift	<a href="#">Figure 7-4</a>
Typical Distribution of Inverting Input Bias Current	<a href="#">Figure 7-5</a>
Typical Distribution of Noninverting Input Bias Current	<a href="#">Figure 7-6</a>
Typical Distribution of Input Offset Current	<a href="#">Figure 7-7</a>
Typical CMRR Distribution, $G = 1$	<a href="#">Figure 7-8</a>
Typical CMRR Distribution, $G = 10$	<a href="#">Figure 7-9</a>
Typical Gain Error Distribution	<a href="#">Figure 7-10</a>
<b>vs Temperature Graphs</b>	
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Output Stage Offset Voltage vs Temperature	<a href="#">Figure 7-12</a>
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Input Offset Current vs Temperature	<a href="#">Figure 7-14</a>
CMRR vs Temperature, $G = 1$	<a href="#">Figure 7-15</a>
CMRR vs Temperature, $G = 10$	<a href="#">Figure 7-16</a>
Gain Error vs Temperature, $G = 1$	<a href="#">Figure 7-17</a>
Gain Error vs Temperature, $G = 100$	<a href="#">Figure 7-18</a>
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Large-Signal Step Response	<a href="#">Figure 7-34</a>
Settling Time vs Step Size	<a href="#">Figure 7-35</a>
Large-Signal Frequency Response	<a href="#">Figure 7-36</a>
Closed-Loop Output Impedance vs Frequency	<a href="#">Figure 7-37</a>

## 7.6 Typical Characteristics

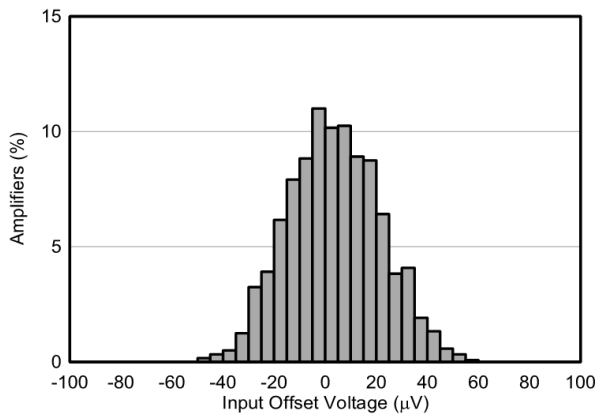
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**Table 7-1. Table of Graphs (continued)**

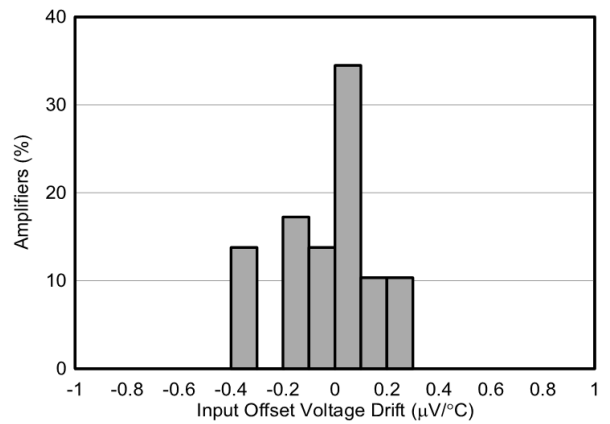
FIGURE TITLE	FIGURE NUMBER
<b>Input and Output Voltage Graphs</b>	
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Negative Output Voltage Swing vs Output Current, $V_S = 2.7\text{ V}$	<a href="#">Figure 7-52</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 2.7\text{ V}$ , $G = 1$	<a href="#">Figure 7-53</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 2.7\text{ V}$ , $G = 1$	<a href="#">Figure 7-54</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 5\text{ V}$ , $G = 1$	<a href="#">Figure 7-55</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 5\text{ V}$ , $G = 100$	<a href="#">Figure 7-56</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 24\text{ V}$ and $V_S = 30\text{ V}$ , $G = 1$	<a href="#">Figure 7-57</a>
Input Common-Mode Voltage vs Output Voltage, $V_S = 24\text{ V}$ and $V_S = 30\text{ V}$ , $G = 10$	<a href="#">Figure 7-58</a>

## 7.6 Typical Characteristics

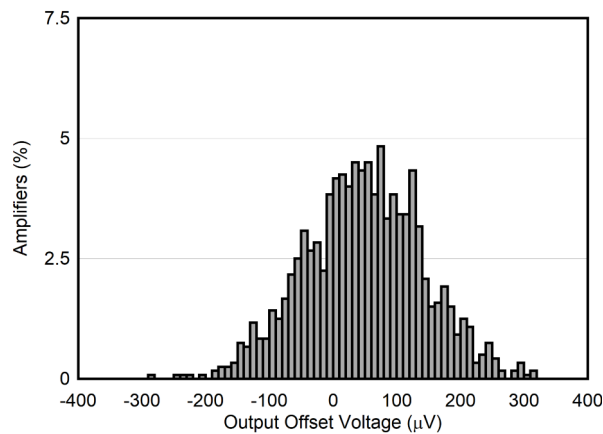
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)



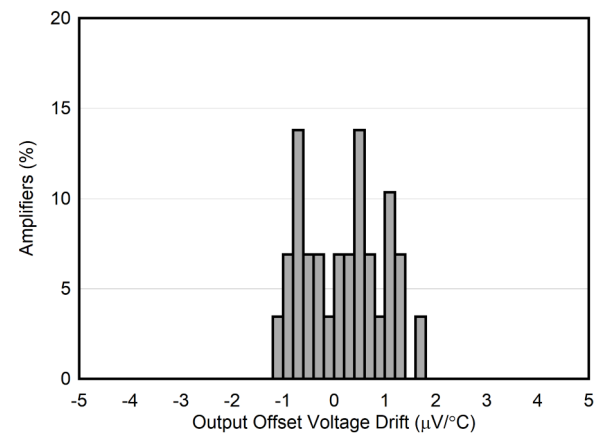
**Figure 7-1. Typical Distribution of Input Stage Offset Voltage**



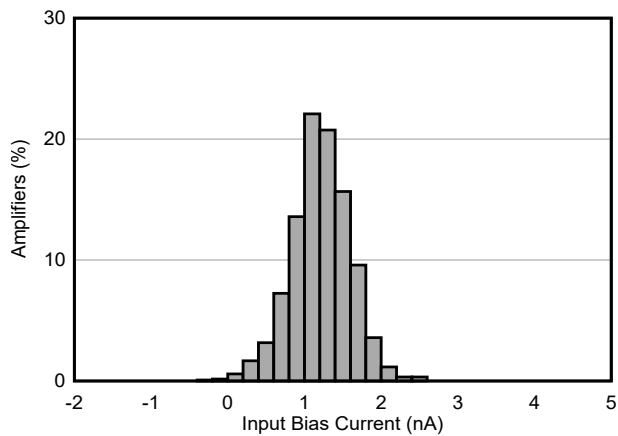
**Figure 7-2. Typical Distribution of Input Stage Offset Voltage Drift**



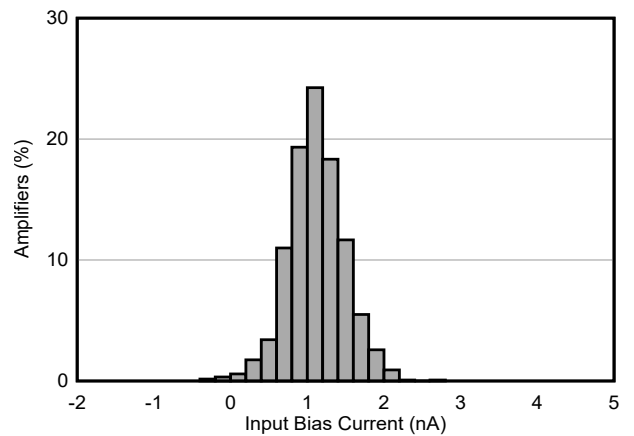
**Figure 7-3. Typical Distribution of Output Stage Offset Voltage**



**Figure 7-4. Typical Distribution of Output Stage Offset Voltage Drift**



**Figure 7-5. Typical Distribution of Inverting Input Bias Current**



**Figure 7-6. Typical Distribution of Noninverting Input Bias Current**

### 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

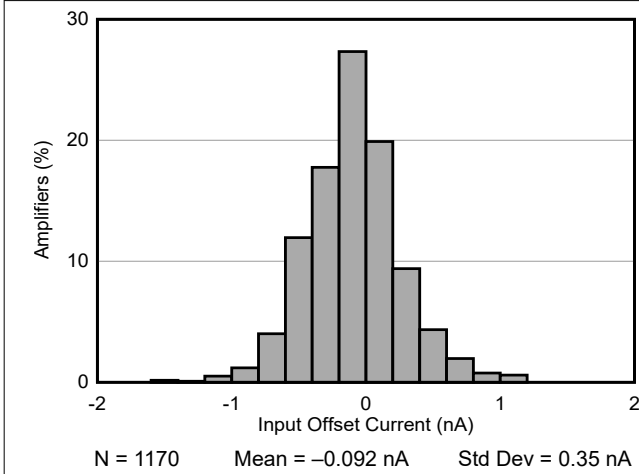


Figure 7-7. Typical Distribution of Input Offset Current

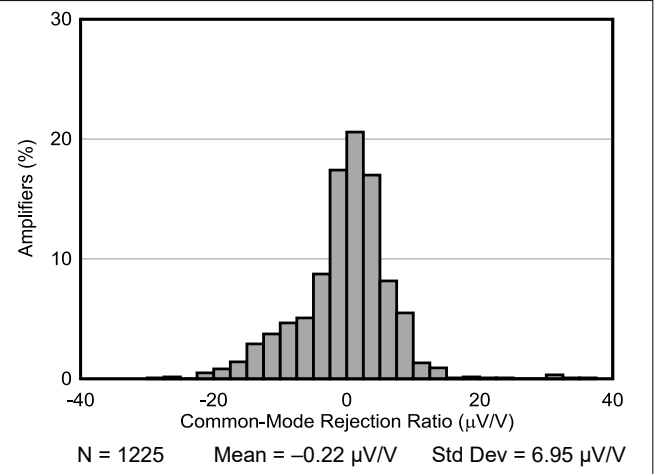


Figure 7-8. Typical CMRR Distribution

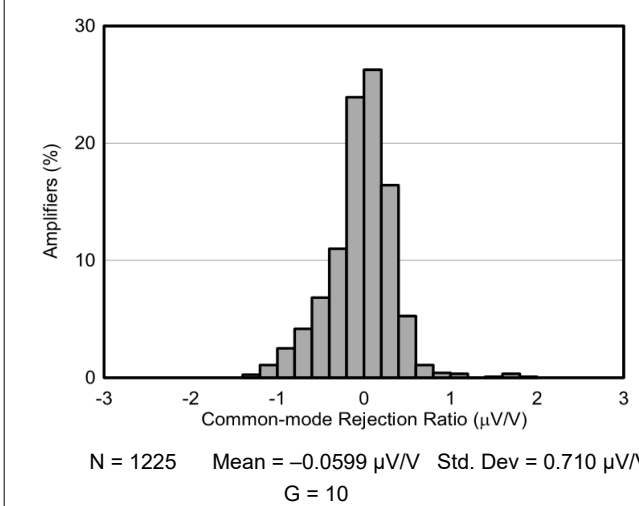


Figure 7-9. Typical CMRR Distribution

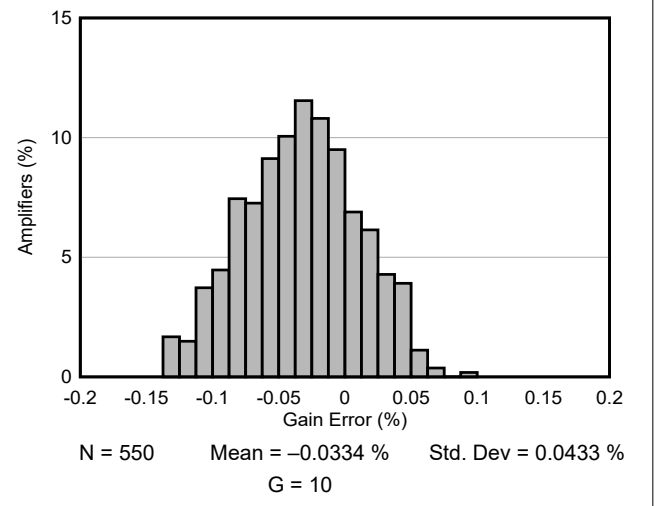


Figure 7-10. Typical Gain Error Distribution

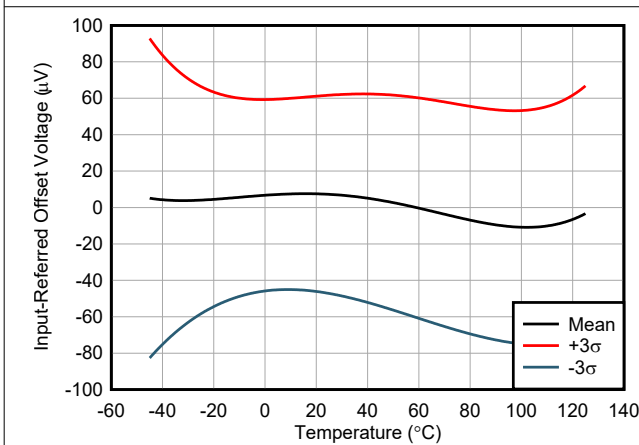


Figure 7-11. Input Stage Offset Voltage vs Temperature

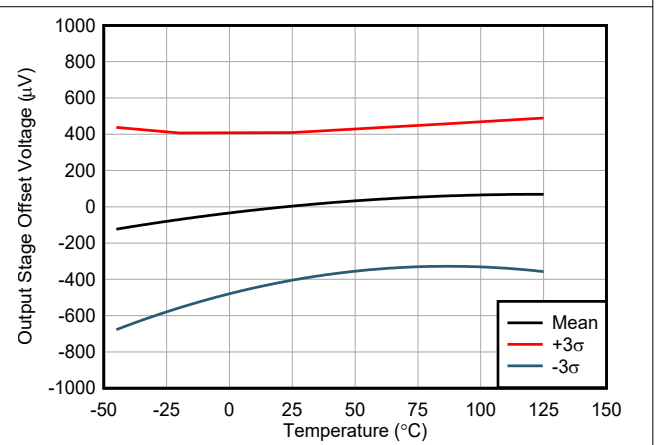
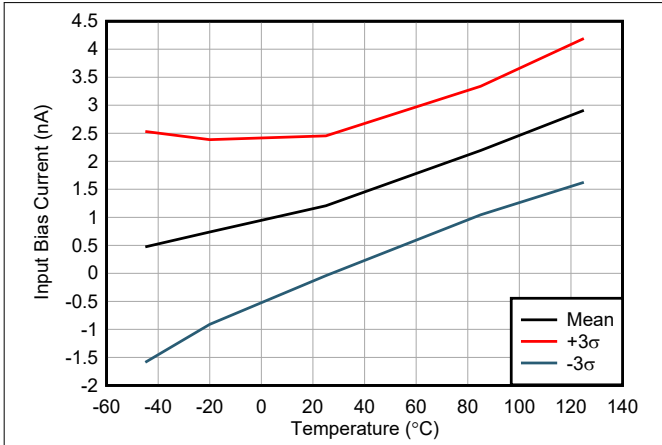


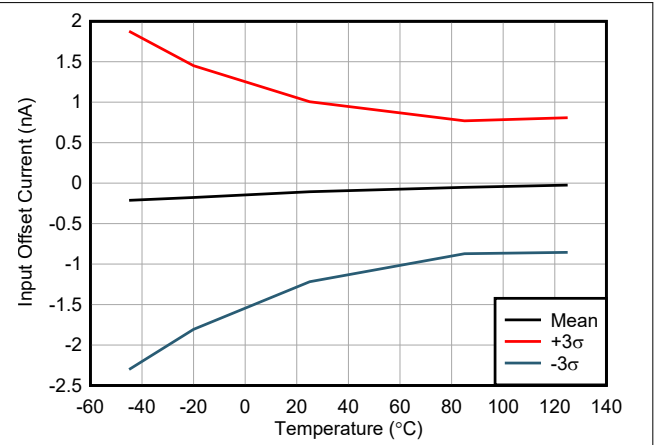
Figure 7-12. Output Stage Offset Voltage vs Temperature

### 7.6 Typical Characteristics (continued)

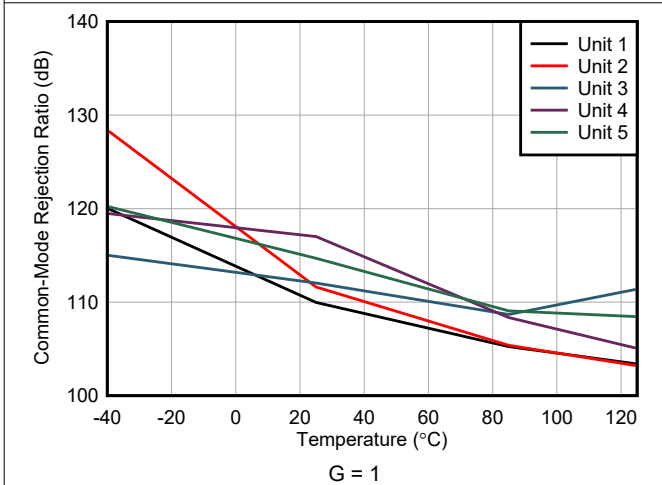
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)



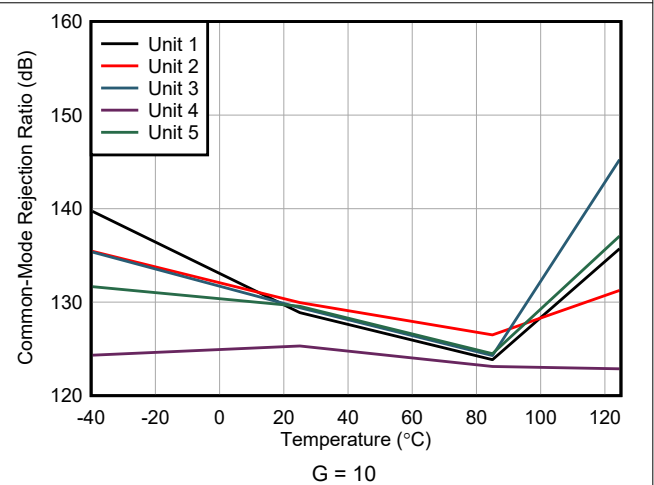
**Figure 7-13. Input Bias Current vs Temperature**



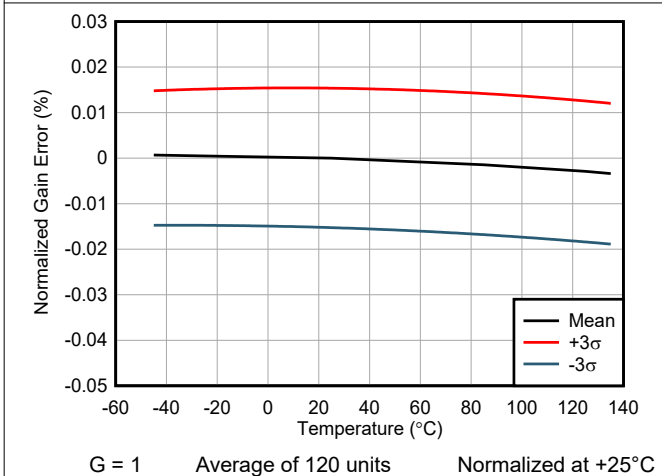
**Figure 7-14. Input Offset Current vs Temperature**



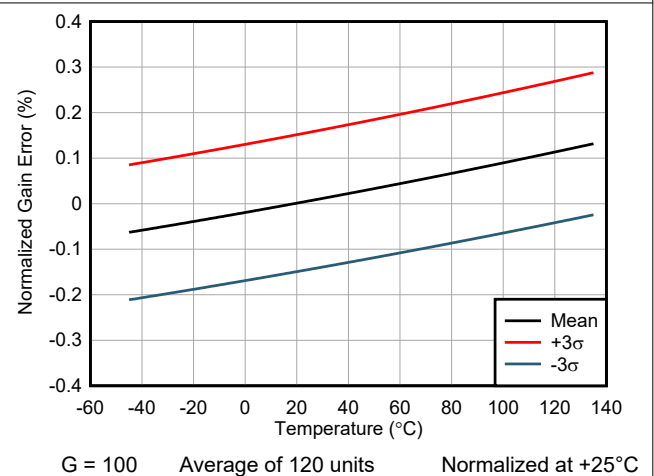
**Figure 7-15. CMRR vs Temperature**  
G = 1



**Figure 7-16. CMRR vs Temperature**  
G = 10



**Figure 7-17. Gain Error vs Temperature**  
G = 1 Average of 120 units Normalized at +25°C



**Figure 7-18. Gain Error vs Temperature**  
G = 100 Average of 120 units Normalized at +25°C

### 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

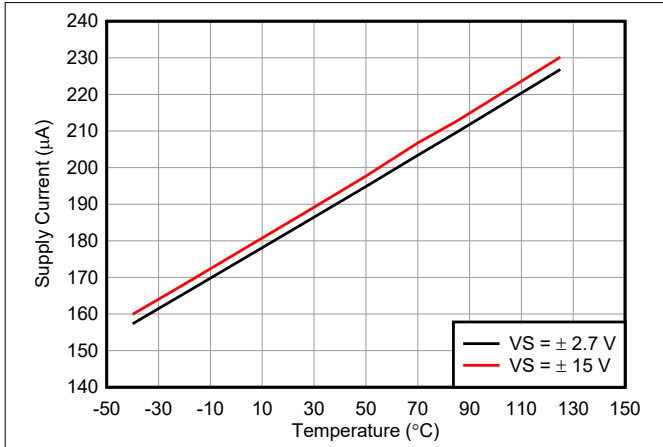


Figure 7-19. Supply Current vs Temperature

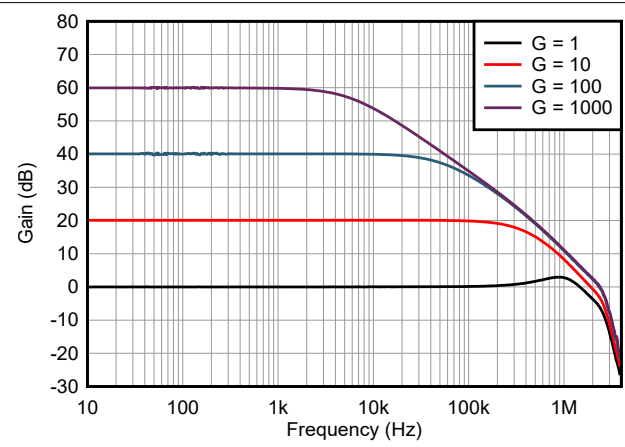


Figure 7-20. Closed-Loop Gain vs Frequency

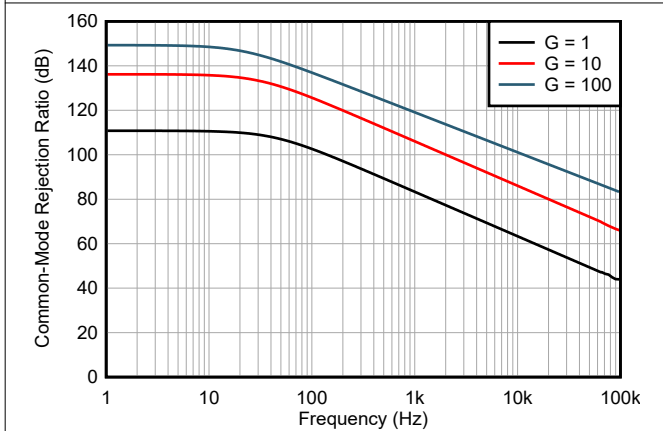


Figure 7-21. CMRR vs Frequency (RTI)

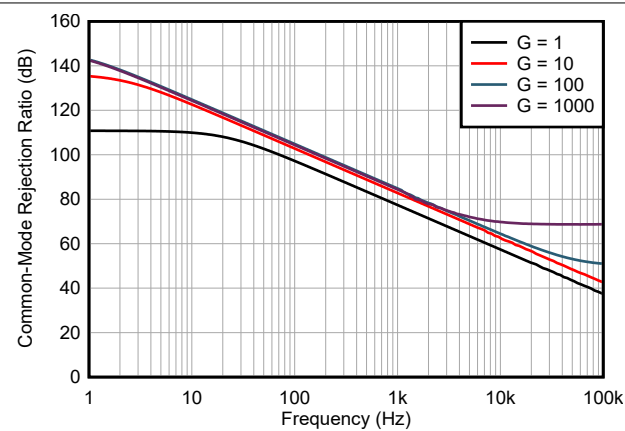


Figure 7-22. CMRR vs Frequency (RTI, 1-kΩ source imbalance)

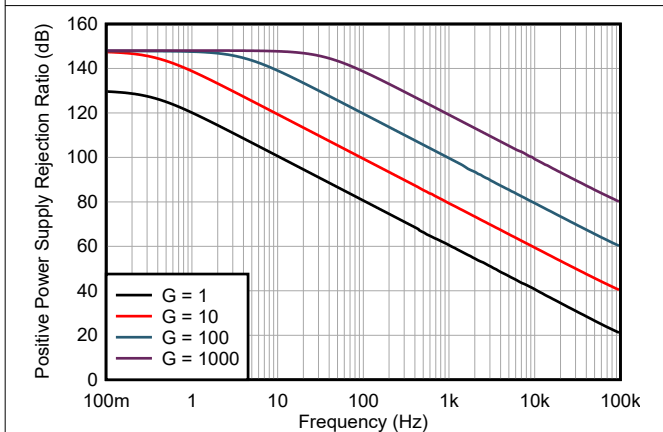


Figure 7-23. Positive PSRR vs Frequency (RTI)

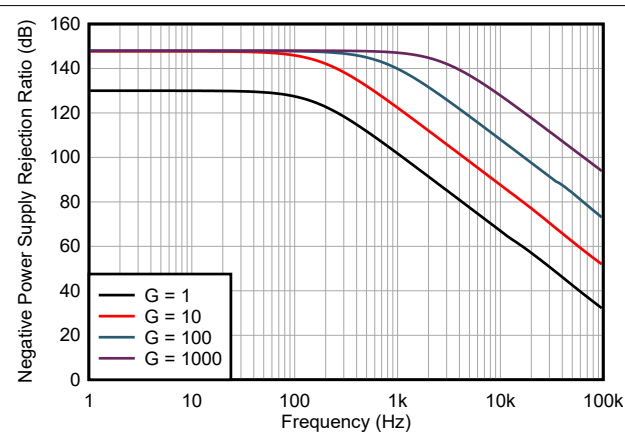
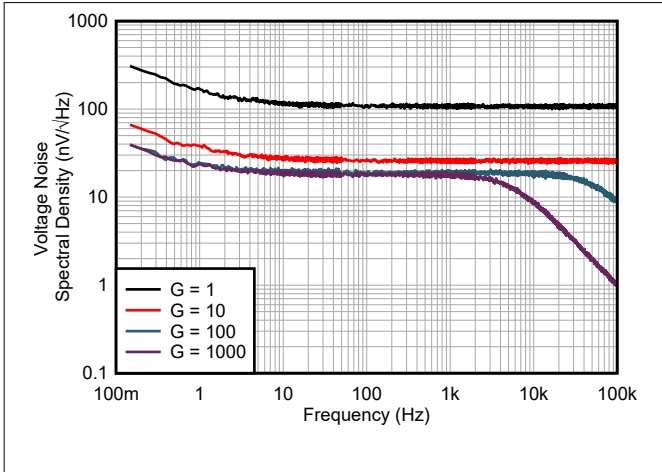


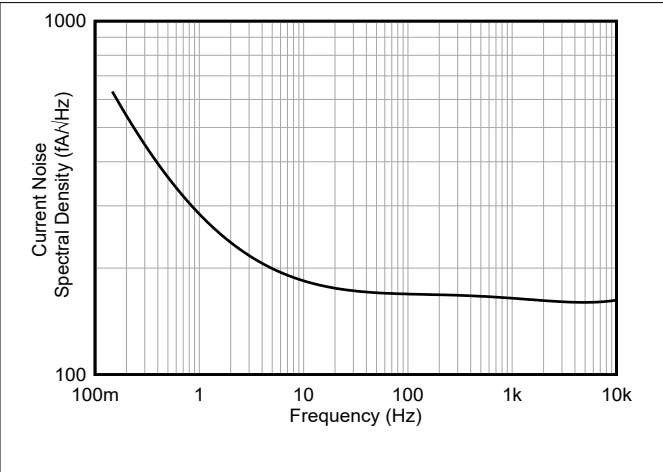
Figure 7-24. Negative PSRR vs Frequency (RTI)

### 7.6 Typical Characteristics (continued)

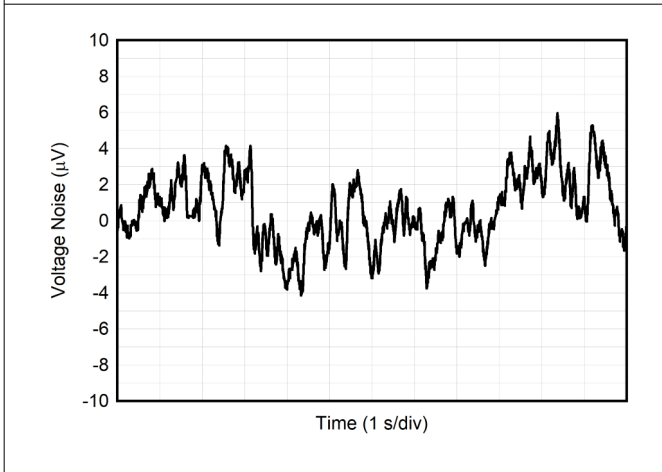
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)



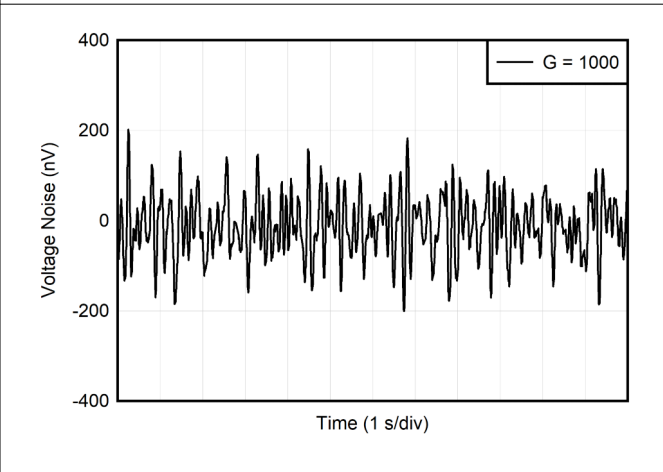
**Figure 7-25. Voltage Noise Spectral Density vs Frequency (RTI)**



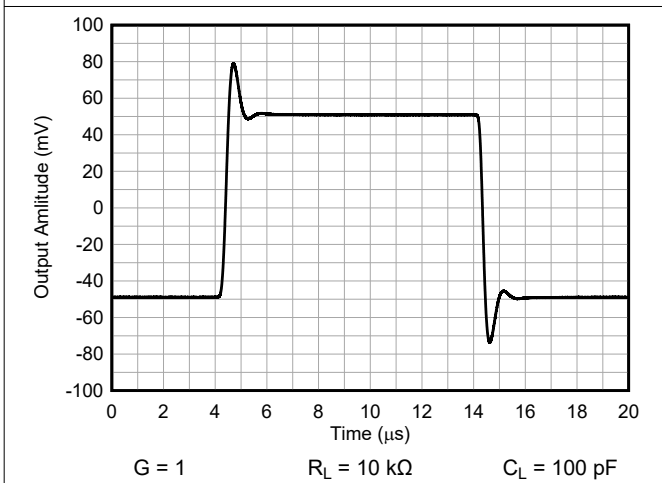
**Figure 7-26. Current Noise Spectral Density vs Frequency (RTI)**



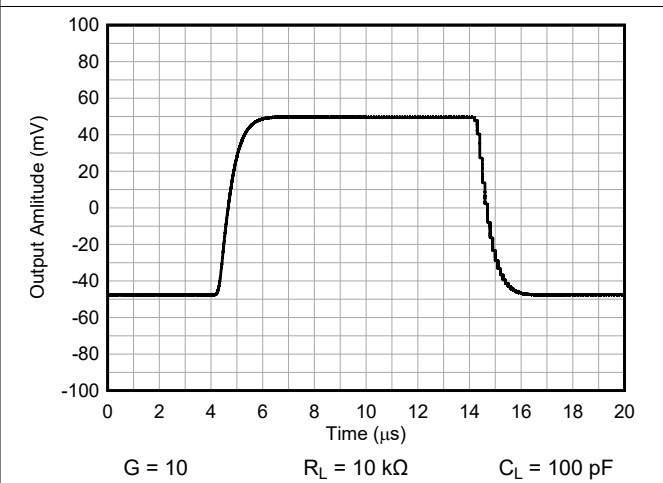
**Figure 7-27. 0.1-Hz to 10-Hz RTI Voltage Noise**



**Figure 7-28. 0.1-Hz to 10-Hz RTI Voltage Noise**



**Figure 7-29. Small-Signal Response**



**Figure 7-30. Small-Signal Response**

## 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

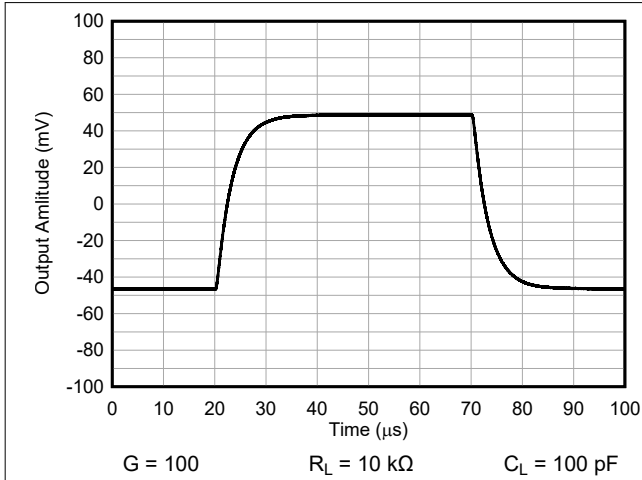


Figure 7-31. Small-Signal Response

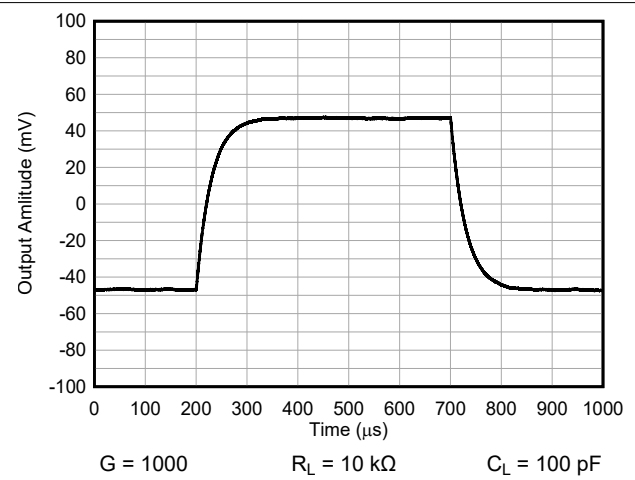


Figure 7-32. Small-Signal Response

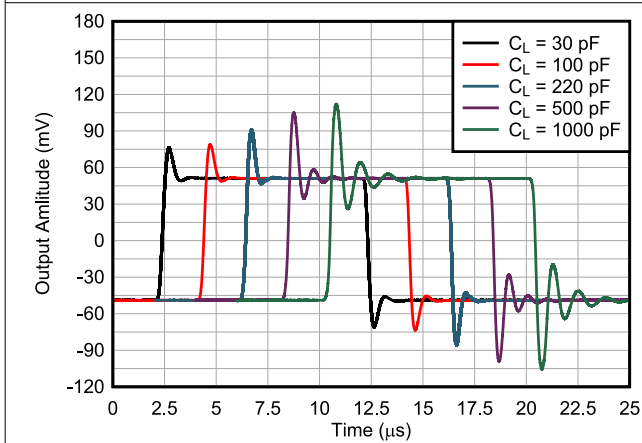


Figure 7-33. Overshoot vs Capacitive Loads

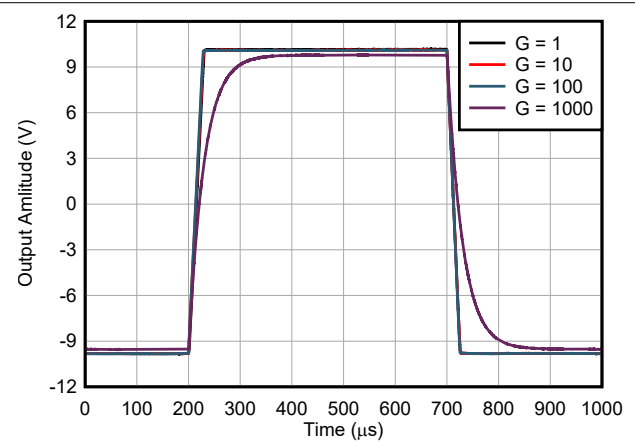


Figure 7-34. Large-Signal Step Response

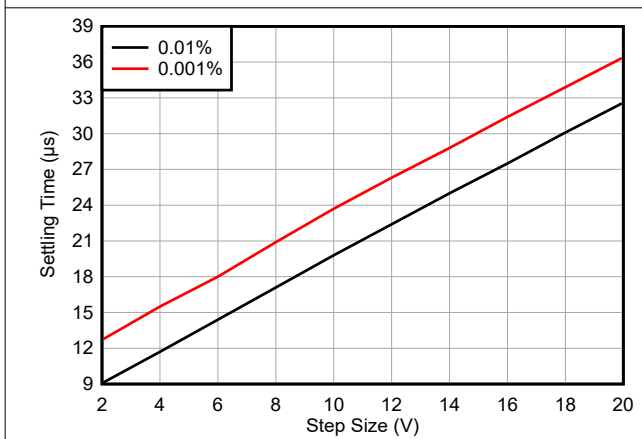


Figure 7-35. Settling Time vs Step Size

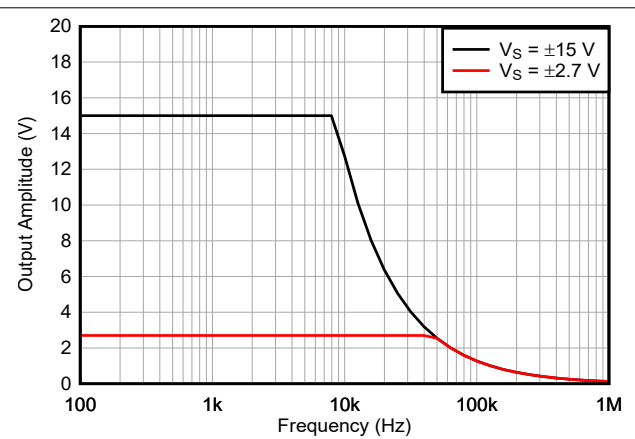
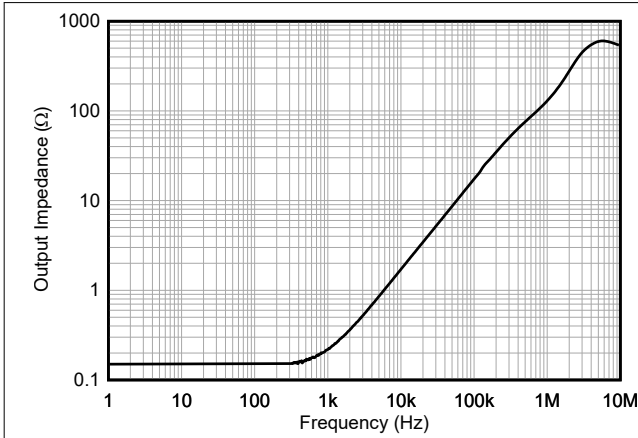


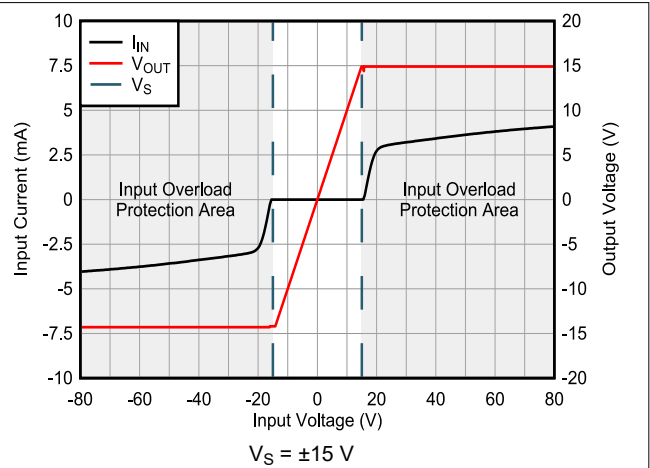
Figure 7-36. Large-Signal Frequency Response

### 7.6 Typical Characteristics (continued)

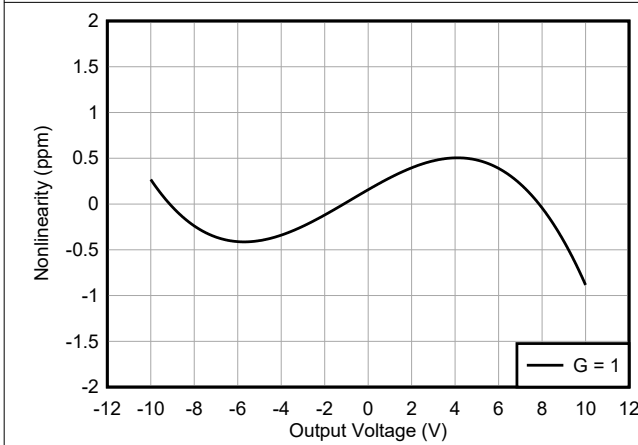
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)



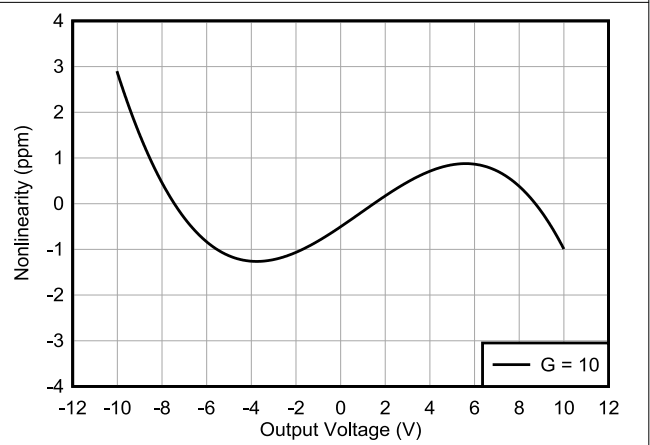
**Figure 7-37. Closed-Loop Output Impedance vs Frequency**



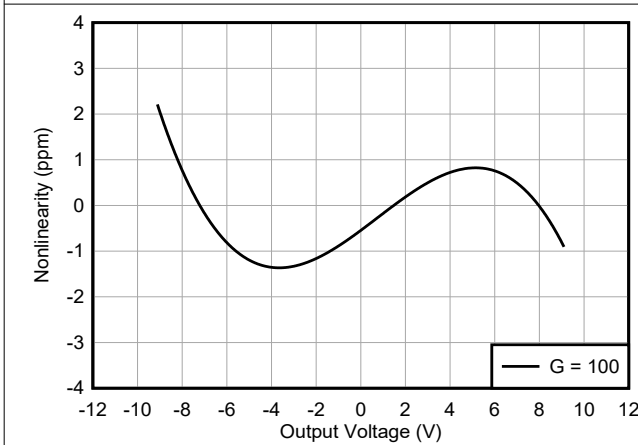
**Figure 7-38. Input Current vs Input Overvoltage**



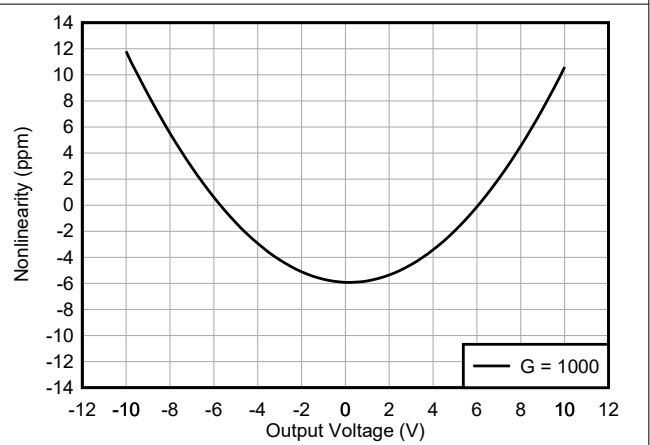
**Figure 7-39. Gain Nonlinearity**



**Figure 7-40. Gain Nonlinearity**



**Figure 7-41. Gain Nonlinearity**



**Figure 7-42. Gain Nonlinearity**

### 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

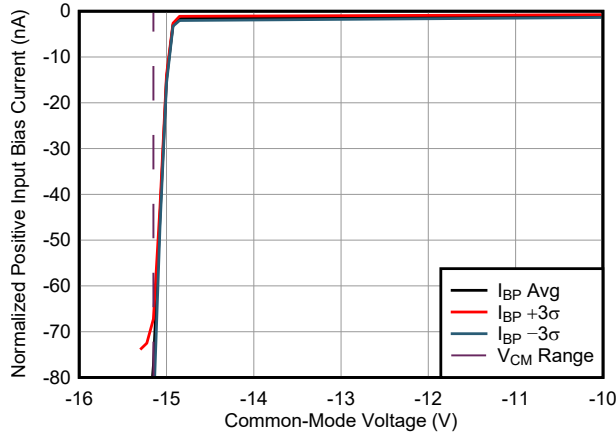


Figure 7-43. Positive Input Bias Current vs Common-Mode Voltage ( $V_{S-}$ )

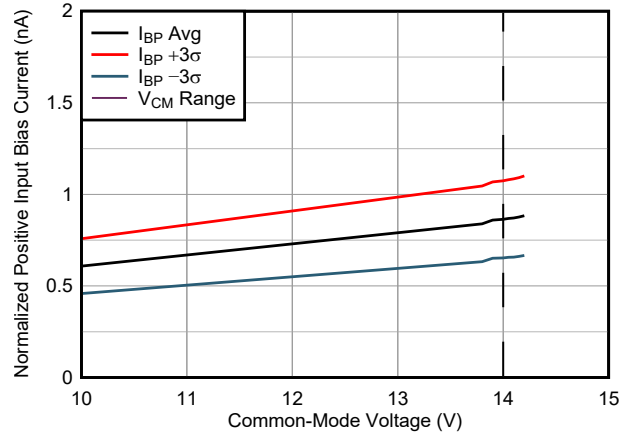


Figure 7-44. Positive Input Bias Current vs Common-Mode Voltage ( $V_{S+}$ )

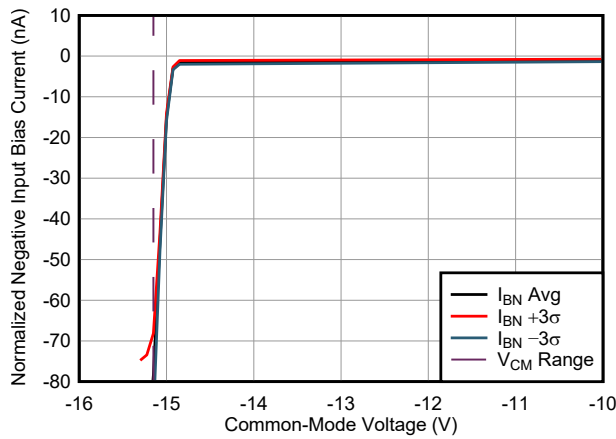


Figure 7-45. Negative Input Bias Current vs Common-Mode Voltage ( $V_{S-}$ )

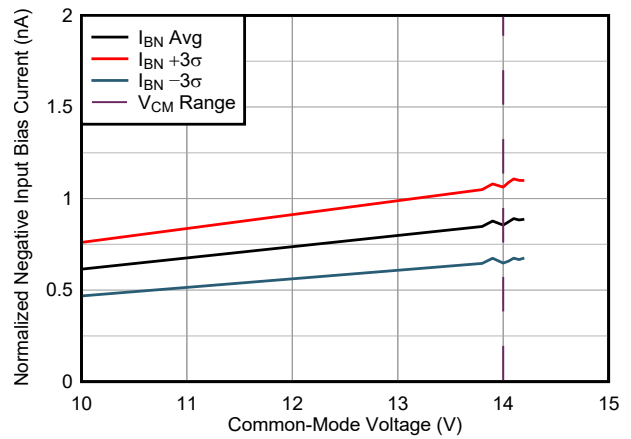


Figure 7-46. Negative Input Bias Current vs Common-Mode Voltage ( $V_{S+}$ )

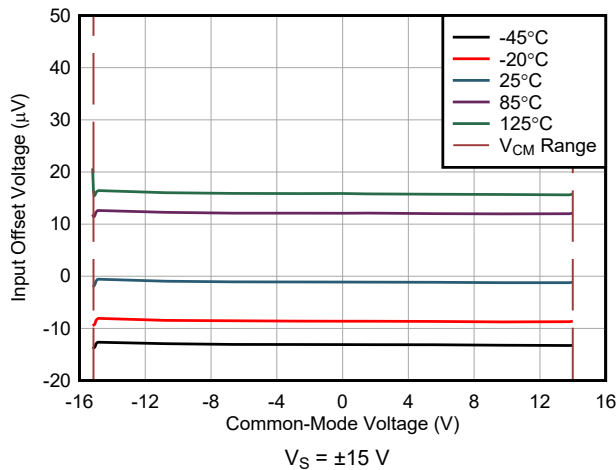


Figure 7-47. Offset Voltage vs Common-Mode Voltage

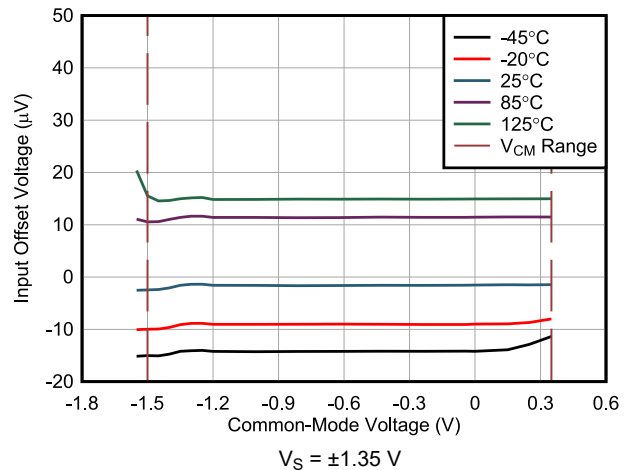


Figure 7-48. Offset Voltage vs Common-Mode Voltage

## 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

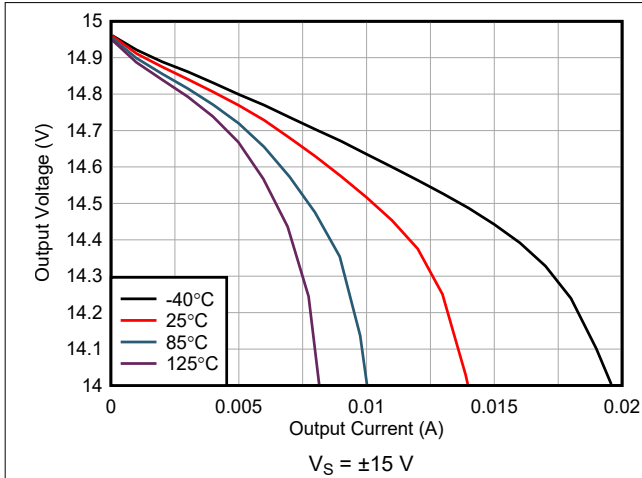


Figure 7-49. Positive Output Voltage Swing vs Output Current

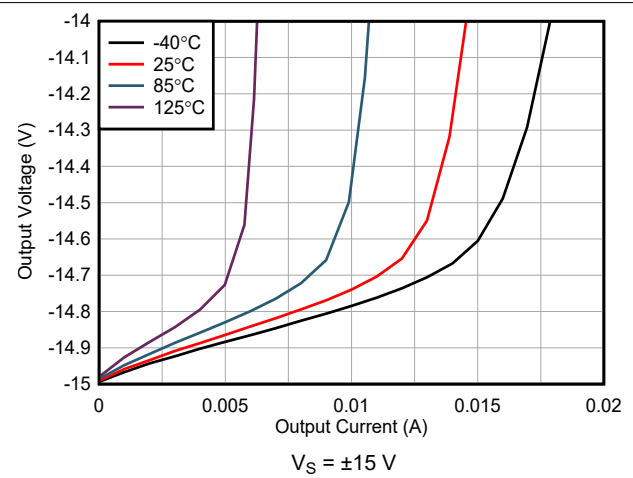


Figure 7-50. Negative Output Voltage Swing vs Output Current

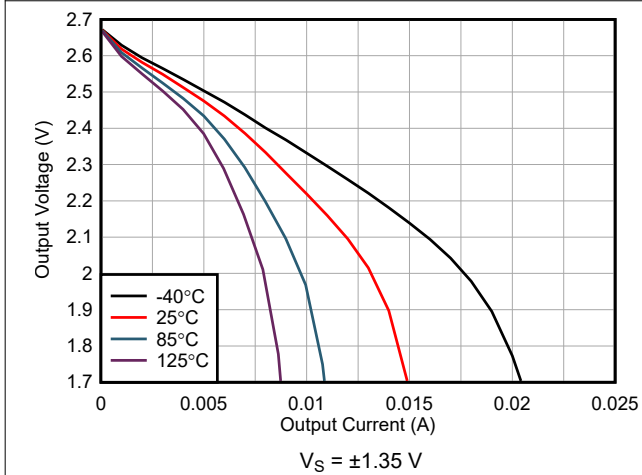


Figure 7-51. Positive Output Voltage Swing vs Output Current

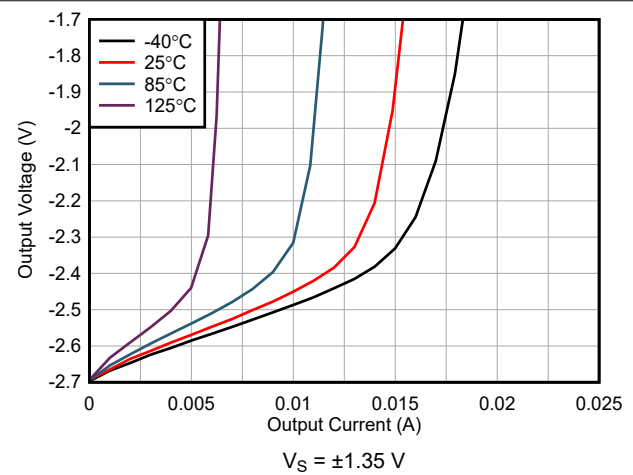


Figure 7-52. Negative Output Voltage Swing vs Output Current

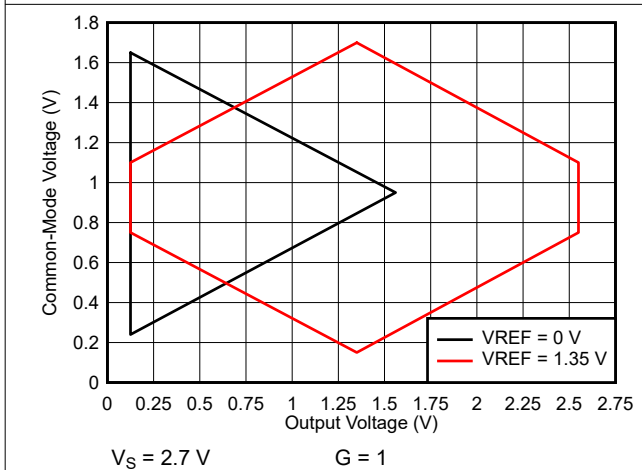


Figure 7-53. Input Common-Mode Voltage vs Output Voltage

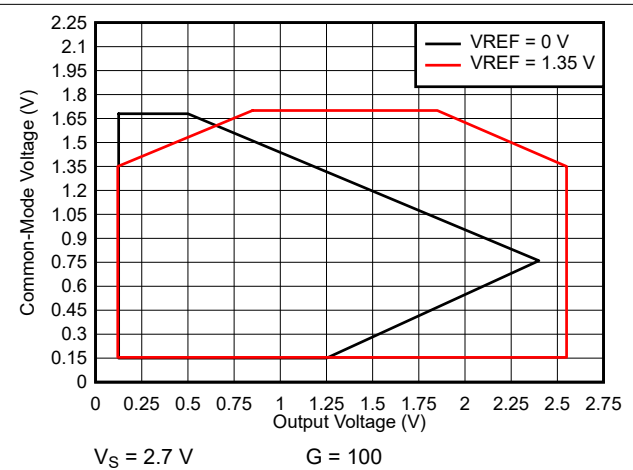


Figure 7-54. Input Common-Mode Voltage vs Output Voltage

### 7.6 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{ V}$ ,  $R_L = 10\text{ k}\Omega$ ,  $C_L = 0\text{ pF}$ ,  $V_{CM} = V_{REF} = 0\text{ V}$ , and  $G = 1$  (unless otherwise noted)

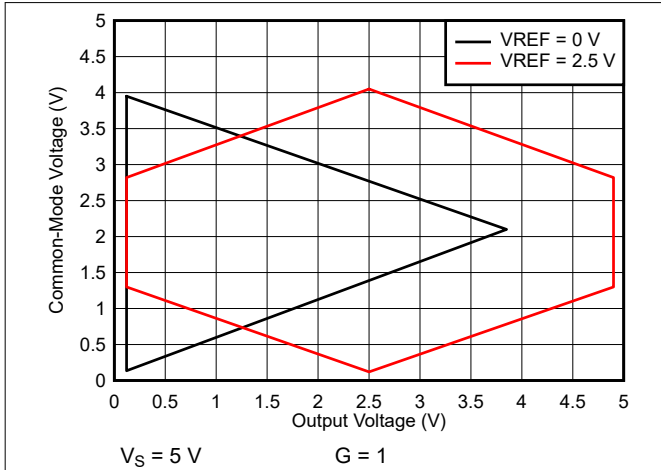


Figure 7-55. Input Common-Mode Voltage vs Output Voltage

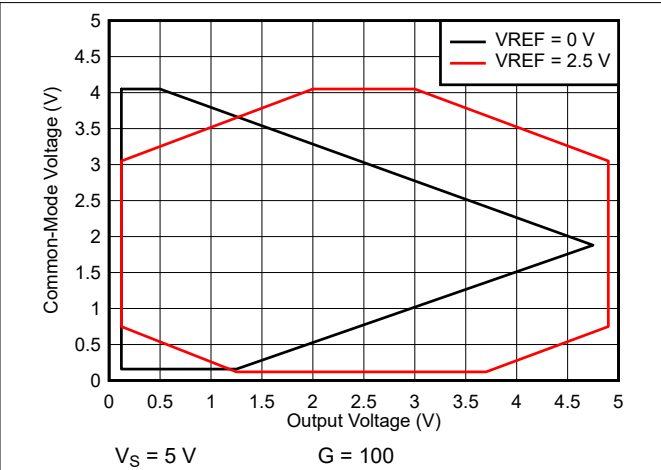


Figure 7-56. Input Common-Mode Voltage vs Output Voltage

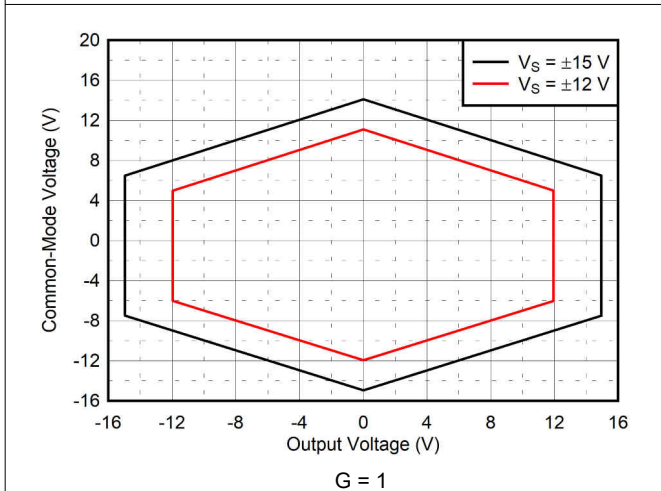


Figure 7-57. Input Common-Mode Voltage vs Output Voltage

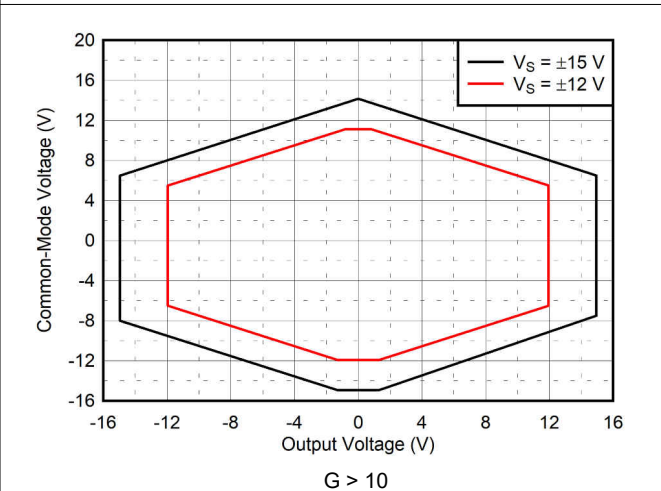


Figure 7-58. Input Common-Mode Voltage vs Output Voltage

## 8 Detailed Description

### 8.1 Overview

The INA823 is a monolithic precision instrumentation amplifier that incorporates a current-feedback input stage and a four-resistor difference-amplifier output stage. One of the features of an instrumentation amplifier (IA) is that the gain is set by placing an external resistor across the  $R_G$  pins, as described in Section 8.3.1. The three-op-amp IA topology in the INA823 limits the maximum input voltage applied to the input terminal. The maximum input voltage depends on the common-mode voltage, differential voltage, gain, and the reference voltage; for more information, see Section 8.3.2. The INA823 also features protection at each input by two junction field-effect transistors (JFETs) that provide a low series resistance under normal signal conditions, and preserve excellent noise performance. When excessive voltage is applied, these transistors limit the input current, as described in Section 8.3.3.

The INA823 is developed for medical-sector applications such as infusion pumps (see Section 9.2.1), and industrial applications such as programmable logic controllers (see Section 9.2.2)

The schematic in Figure 8-1 shows how the INA823 operates. A differential input voltage is buffered by the input transistors,  $Q_1$  and  $Q_2$ , and is forced across  $R_G$ . This causes a signal current through  $R_G$ ,  $R_1$ , and  $R_2$ . The output difference amplifier,  $A_3$ , removes the common-mode component of the input signal and refers the output signal to the REF pin. The threshold voltage of  $Q_1$  and  $Q_2$  (defined as  $V_{BE}$ ) along with the voltage drop across  $R_1$  and  $R_2$  produce output voltages on  $A_1$  and  $A_2$ , respectively, that are approximately 0.8 V less than the input voltages.

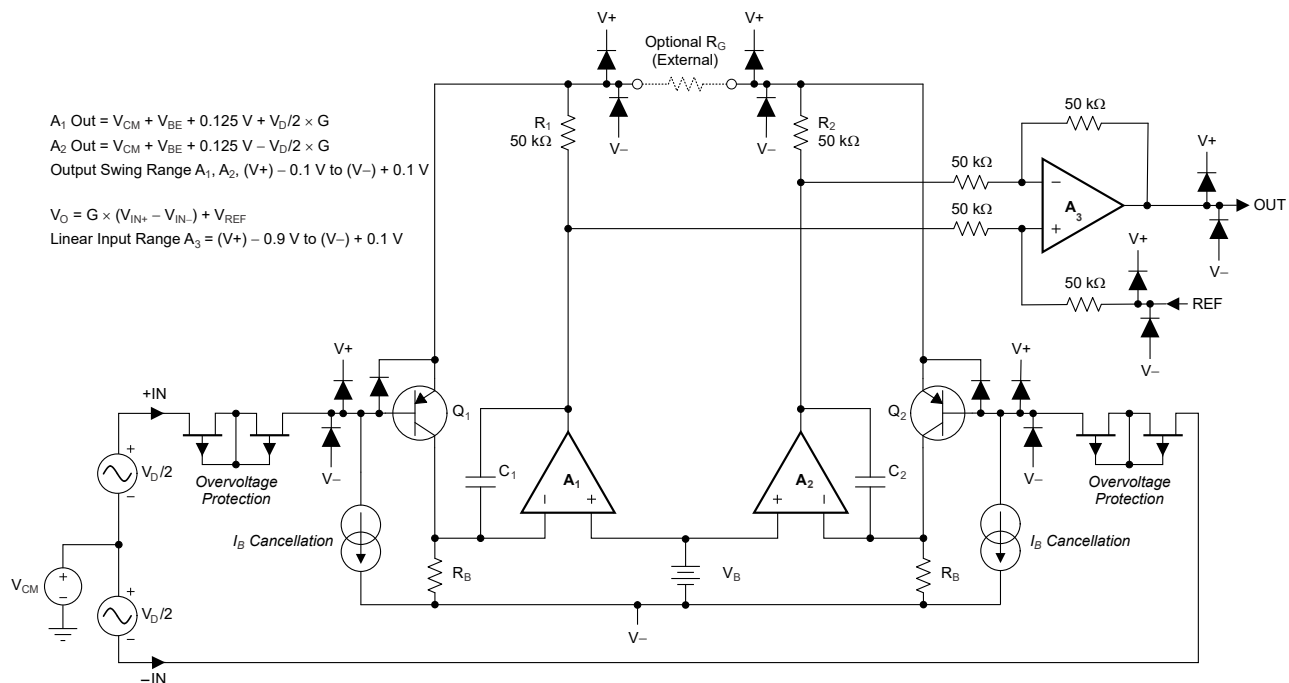
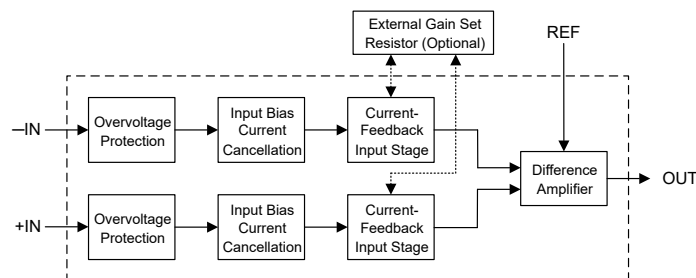


Figure 8-1. Detailed Schematic

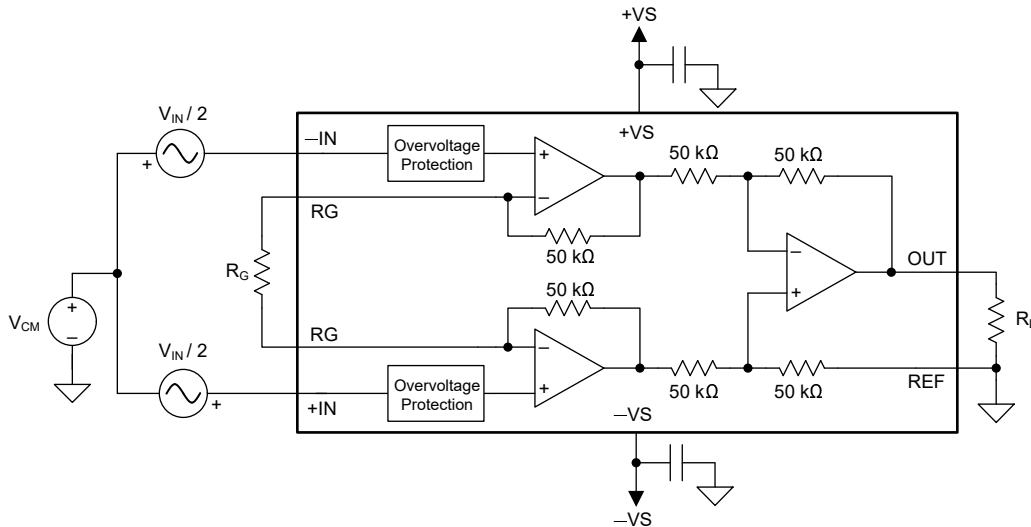
### 8.2 Functional Block Diagram



### 8.3 Feature Description

#### 8.3.1 Gain-Setting Function

Figure 8-2 shows that the gain of the INA823 is set by a single external resistor ( $R_G$ ) connected between the RG pins (pins 1 and 8).



**Figure 8-2. Simplified Schematic of the INA823 With Gain and Output Equations**

The gain of the INA823 can be calculated with Equation 1:

$$G = 1 + \frac{100 \text{ k}\Omega}{R_G} \tag{1}$$

The value of the external gain resistor  $R_G$  is then derived from the gain equation:

$$R_G = \frac{100 \text{ k}\Omega}{G - 1} \tag{2}$$

Table 8-1 lists several commonly used gains and resistor values. The 100-kΩ term in Equation 1 is a result of the sum of the two internal 50-kΩ feedback resistors. These on-chip resistors are laser-trimmed to accurate absolute values. The accuracy and temperature coefficients of these resistors are included in the gain accuracy and drift specifications of the Section 7.5. As shown in Figure 8-2 and explained in more details in Section 11, make sure to connect low-ESR, 0.1-μF ceramic bypass capacitors between each supply pin and ground that are placed as close to the device as possible.

**Table 8-1. Commonly Used Gains and Resistor Values**

DESIRED GAIN	NEAREST 1% $R_G$ (Ω)	CALCULATED GAIN ERROR (%)
1	Not connected	Not connected
2	100 k	0
5	24.9 k	0.321
10	11 k	0.909
20	5.23 k	0.602
33	3.09 k	1.098
50	2.05 k	0.439
65	1.58 k	1.091
100	1.02 k	0.961
200	499	0.700
500	200	0.200
1000	100	0.100

### 8.3.1.1 Gain Drift

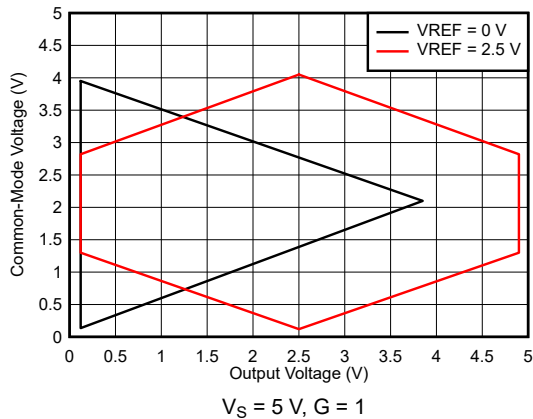
The stability and temperature drift of the external gain setting resistor ( $R_G$ ) also affects gain. The contribution of  $R_G$  to gain accuracy and drift is determined from [Equation 2](#).

The best gain drift of 5 ppm/°C (maximum) is achieved when the INA823 uses  $G = 1$  V/V without  $R_G$  connected. In this case, gain drift is limited by the slight mismatch of the temperature coefficient of the integrated 50-k $\Omega$  resistors in the differential amplifier ( $A_3$ ).

At gains greater than 1 V/V, gain drift increases as a result of the individual drift of the 50-k $\Omega$  resistors in the feedback of  $A_1$  and  $A_2$  relative to the drift of the external gain resistor ( $R_G$ .) The low temperature coefficient of the internal feedback resistors significantly improves the overall temperature stability of applications using gains greater than 1 V/V over alternate options.

### 8.3.2 Input Common-Mode Voltage Range

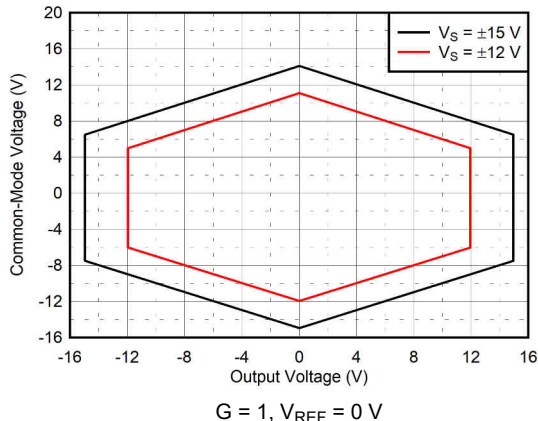
The INA823 linear input voltage range extends from 1 V less than the positive supply to 0.15 V less than the negative supply, and maintains excellent common-mode rejection throughout this range. The common-mode range for the most common operating conditions are shown in [Figure 8-3](#). While there are other methods to calculate the common-mode voltage range, the suggested tool is the [Analog Engineers Calculator](#).



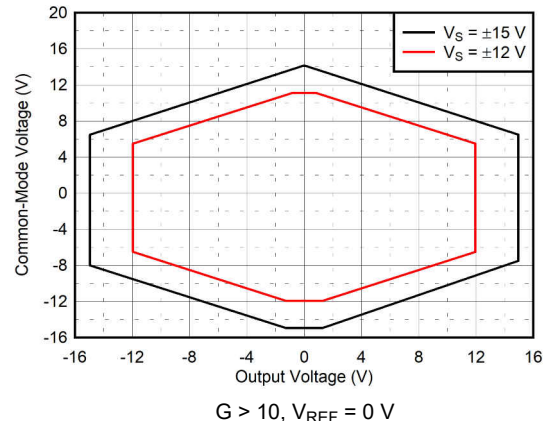
**Figure 8-3. Input Common-Mode Voltage vs Output Voltage**



**Figure 8-4. Input Common-Mode Voltage vs Output Voltage**



**Figure 8-5. Input Common-Mode Voltage vs Output Voltage**



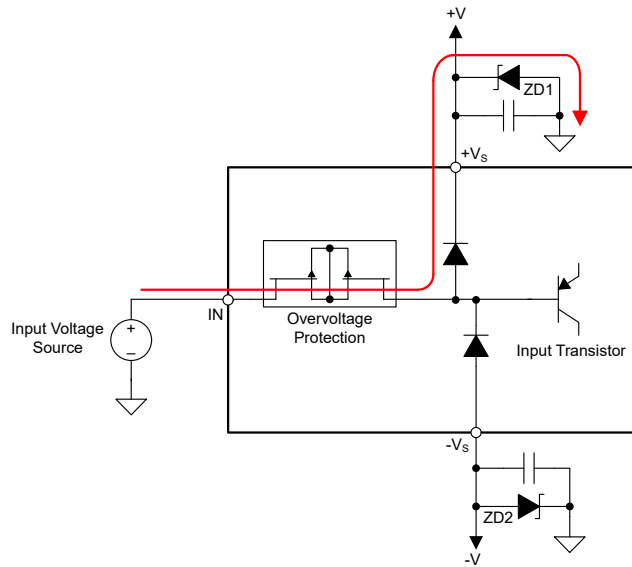
**Figure 8-6. Input Common-Mode Voltage vs Output Voltage**

A single-supply instrumentation amplifier has special design considerations. To achieve a common-mode range that extends to single-supply ground, the INA823 employs a current-feedback topology with PNP input

transistors. The matched PNP transistors, Q1 and Q2, shift the input voltages of both inputs up by a diode drop, and (through the feedback network) shift the output of A1 and A2 by approximately 0.6 V. The output of A1 and A2 is well within the linear range when the inputs are within the single-supply ground. When inputs are within the supply ground, differential measurements can be made at the ground level. As a result of this input level-shifting, the voltages at pin 1 and pin 8 are not equal to the respective input pin voltages. For most applications, this inequality is not important because only the gain-setting resistor connects to these pins.

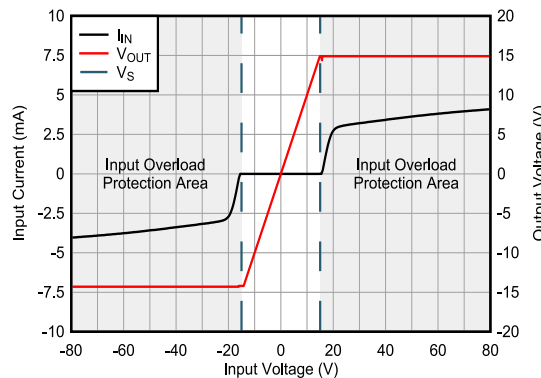
### 8.3.3 Input Protection

The inputs of the INA823 device are individually protected for voltages up to  $\pm 60$  V and for short transients up to  $\pm 80$  V. For example, a condition of  $-60$  V on one input and  $+60$  V on the other input does not cause damage. Internal circuitry on each input provides low series impedance under normal signal conditions. If the input is overloaded, the protection circuitry limits the input current to a value of approximately 4 mA.



**Figure 8-7. Input Current Path During an Overvoltage Condition**

During an input overvoltage condition, current flows through the input protection diodes into the power supplies, as shown in Figure 8-7. If the power supplies are unable to sink current, then Zener diode clamps (ZD1 and ZD2 in Figure 8-7) must be placed on the power supplies to provide a current pathway to ground. Figure 8-8 shows the input current for input voltages from  $-80$  V to  $+80$  V when the INA823 is powered by  $\pm 15$ -V supplies.



**Figure 8-8. Input Current vs Input Overvoltage**

## 8.4 Device Functional Modes

The INA823 has a single functional mode and is operational when the power supply voltage is greater than 2.7 V ( $\pm 1.35$  V). The maximum power-supply voltage for the INA823 is 36 V ( $\pm 18$  V).

## 9 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

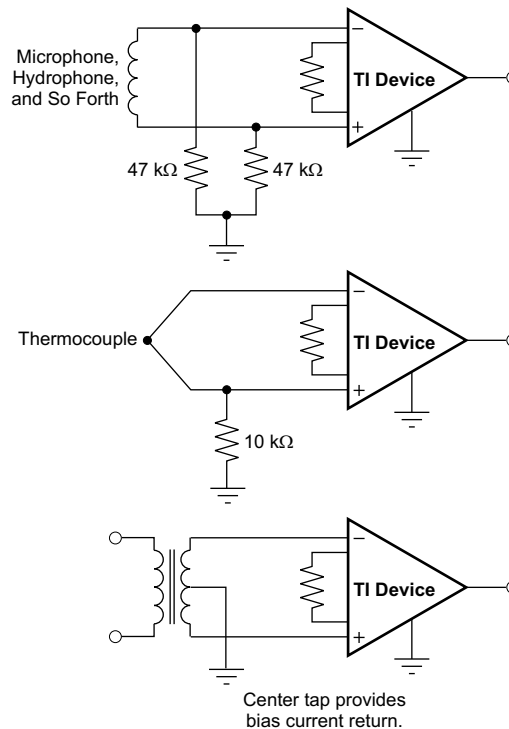
### 9.1 Application Information

#### 9.1.1 Input Bias Current Return Path

The input impedance of the INA823 is extremely high, but a path must be provided for the input bias current of both inputs. This input bias current is typically 1.2 nA. High input impedance means that this input bias current changes little with varying input voltage.

For proper operation, input circuitry must provide a path for this input bias current. [Figure 9-1](#) shows various provisions for an input bias current path. Without a bias current path, the inputs float to a potential that exceeds the common-mode range of the INA823, and the input amplifiers saturate. If the differential source resistance is low, the bias current return path connects to one input (as shown in the thermocouple example in [Figure 9-1](#)). With a higher source impedance, use two equal resistors to provide a balanced input, with the possible advantages of a lower input offset voltage as a result of bias current, and better high-frequency common-mode rejection. Furthermore, matched input impedances generally minimize the impact to performance in cases where the input common-mode voltage is very low and input bias current can increase as the  $I_B$  cancellation circuitry runs out of headroom. The input offset current typically remains low; therefore, well-matched input impedances reduce the differential error voltage that would otherwise arise.

For more details about why a valid input bias current return path is necessary, see the [Importance of Input Bias Current Return Paths in Instrumentation Amplifier Applications](#) application note.



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**Figure 9-1. Providing an Input Common-Mode Current Path**

## 9.2 Typical Applications

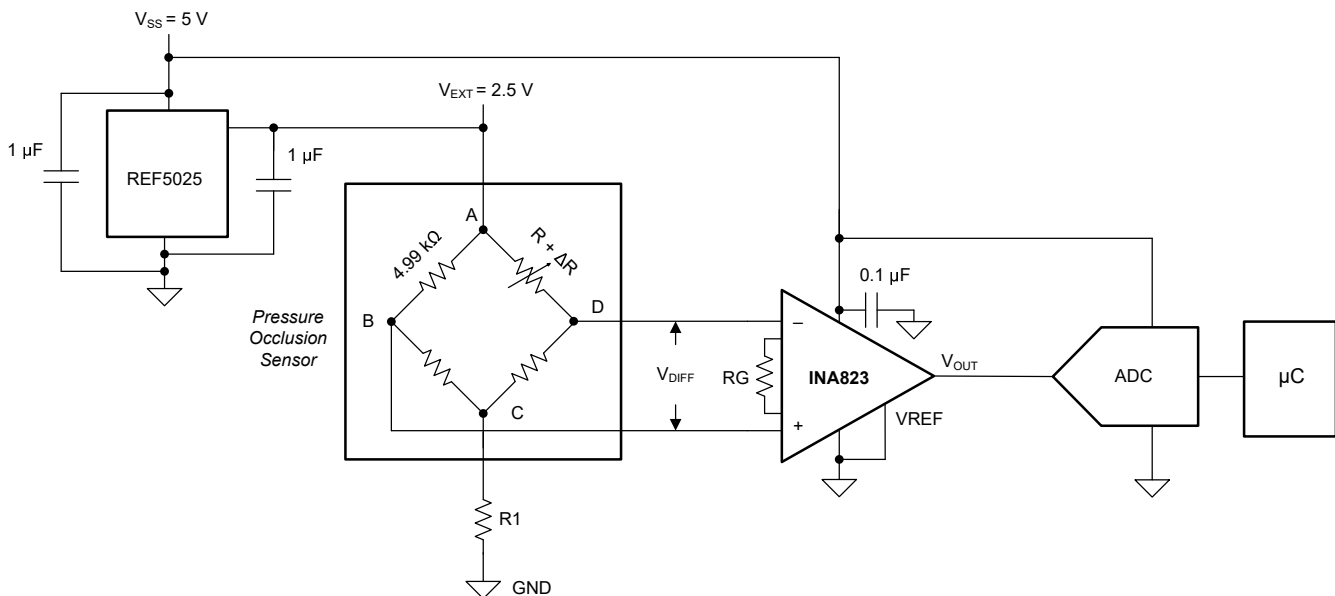
### 9.2.1 Resistive-Bridge Pressure Sensor

The INA823 is an integrated instrumentation amplifier that measures small differential voltages while simultaneously rejecting larger common-mode voltages. The device offers a low power consumption of 250  $\mu\text{A}$  (max) and high precision, thus minimizing errors with voltage offset, offset drift and gain error.

The device is designed for portable applications where sensors measure physical parameters, such as changes in fluid, pressure, temperature, or humidity. An example of a pressure sensor used in the medical sector is in portable infusion pumps or dialysis machines.

The pressure sensor is made of a piezo-resistive element that can be derived as a classical 4-resistor Wheatstone bridge. Occlusion (infusion of fluids, medication, or nutrients) happens only in one direction, and therefore, can only cause the resistive element ( $R$ ) to expand. This expansion causes a change in voltage on one leg of the Wheatstone bridge, which induces a differential voltage  $V_{\text{DIFF}}$ .

Figure 9-2 showcases an exemplary circuit for an occlusion pressure sensor application, as required in infusion pumps. When blockage (occlusion) occurs against a set-point value, the tubing depresses, thus causing the piezo-resistive element to expand (Node AD:  $R + \Delta R$ ). The signal chain connected to the bridge downstream processes the pressure change and can trigger an alarm.



**Figure 9-2. Resistive-Bridge Pressure Sensor**

Low-tolerance bridge resistors must be used to minimize the offset and gain errors.

Given that there is only a positive differential voltage applied, this circuit is laid out in single-ended supply mode. The excitation voltage,  $V_{\text{EXT}}$ , to the bridge must be precise and stable; otherwise, measurement error is introduced.

The REF5025 is a low-noise, low-drift (3 ppm/C), and high-precision (0.05%) voltage reference that is an excellent option to generate the excitation voltage  $V_{\text{EXT}}$ .

The following subsections give the design requirements and detailed design procedure for an application with a occlusion pressure sensor.

For more information and design tips to consider when using a resistive-bridge pressure sensor, see the [Design tips for a resistive-bridge pressure sensor in industrial process-control systems analog applications journal](#).

### 9.2.1.1 Design Requirements

For this application, the design requirements are as shown in Table 9-1.

Table 9-1. Design Requirements

DESCRIPTION	VALUE
Single supply voltage	$V_S = 5\text{ V}$
Excitation voltage	$V_{EXT} = 2.5\text{ V}$
Occlusion pressure range	$P = 1...10\text{ psi}$ , increments of $p = 0.5\text{ psi}$
Occlusion pressure sensitivity	$S = 2 \pm 0.5\text{ (25\%)}\text{ mV/V/psi}$
Occlusion pressure impedance (R)	$R = 4.99\text{ k}\Omega \pm 50\ \Omega\text{ (0.1\%)}\text{ }$
Total pressure sampling rate	$S_r = 20\text{ Hz}$
Full-scale range of ADC	$V_{ADC(fs)} = V_{OUT} = 4.5\text{ V}$

### 9.2.1.2 Detailed Design Procedure

This section provides basic calculations to lay out the instrumentation amplifier with respect to the given design requirements.

One of the key considerations in resistive-bridge sensors is the common-mode voltage,  $V_{CM}$ . If the bridge is balanced (no pressure, thus no voltage change),  $V_{CM(MAX)}$  is half of the bridge excitation ( $V_{EXT}$ ). As the pressure increases to the maximum value, the common-mode voltage decreases to  $V_{CM(MIN)}$ .

To achieve the output voltage of  $V_{OUT} = 4.5\text{ V}$  with the INA823, the limitation for the common-mode voltage is at  $V_{CM(INA823max)} = 1.8\text{ V}$ , as shown in Figure 7-56 and Figure 9-3 (where an initial gain value of 100 V/V is used as an approximation). An additional series resistor in the Wheatstone bridge string (R1) is required to shift the common-mode voltage to this value. However, be aware that shifting the common-mode voltage also changes the effective excitation voltage  $V_{EXT}$  across the bridge.

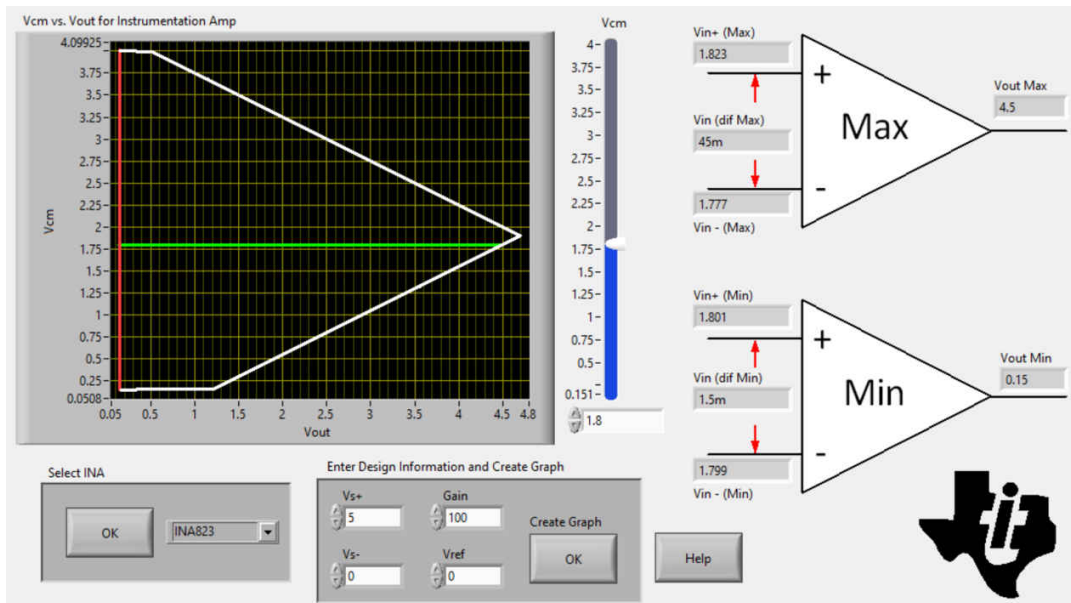


Figure 9-3. Screen Shot From Analog Engineer's Calculator

Calculate the new effective excitation voltage  $V_{EXT(NOM)}$  associated with a desired  $V_{CM(MIN)}$  value by solving the following:

$$V_{EXT(NOM)} = 2 * \left( \frac{V_{EXT} - V_{CM(MIN)}}{1 + S_{MAX} * P_{MAX}} \right) = 2 * \left( \frac{2.5 - 1.8}{1 + 2.5\text{ mV/V*psi} * 10\text{ psi}} \right) = 1.366\text{ V} \quad (3)$$

$V_{EXT(NOM)}$  can in turn be used to calculate the desired value of  $R_1$ :

$$R_1 = R \left( \frac{V_{EXT}}{V_{EXT(NOM)}} - 1 \right) = 4.99 \text{ k}\Omega \left( \frac{2.5 \text{ V}}{1.366 \text{ V}} - 1 \right) = 4.144 \text{ k}\Omega \quad (4)$$

Use a standard 0.1% resistor value of 4.12 k $\Omega$ .

Calculate the maximum value of  $V_{DIFF}$  by solving the following equation for the maximum pressure of 10 psi:

$$V_{DIFF} = (S_{MAX} * P_{MAX}) * V_{EXT(NOM)} = (2.5 \text{ mV/V} * 10 \text{ psi}) * 1.366 \text{ V} = 34.15 \text{ mV} \quad (5)$$

Use the resulting value to verify that the minimum bridge common-mode voltage,  $V_{CM(MIN)}$ , is within the limits of the INA823 by solving the following:

$$V_{CM(MAX)} = V_{CM(MIN)} + \frac{V_{DIFF}}{2} = 1.8 \text{ V} + \frac{34.15 \text{ mV}}{2} = 1.817 \text{ V} \quad (6)$$

Next, use Equation 7 to calculate the required gain for the given maximum sensor output voltage span,  $V_{DIFF}$ , with respect to the required  $V_{OUT}$ , which is the full-scale range of the ADC.

$$G = \frac{V_{OUT}}{V_{DIFF(MAX)}} = \frac{4.5 \text{ V}}{34.15 \text{ mV}} = 131.77 \text{ V/V} \quad (7)$$

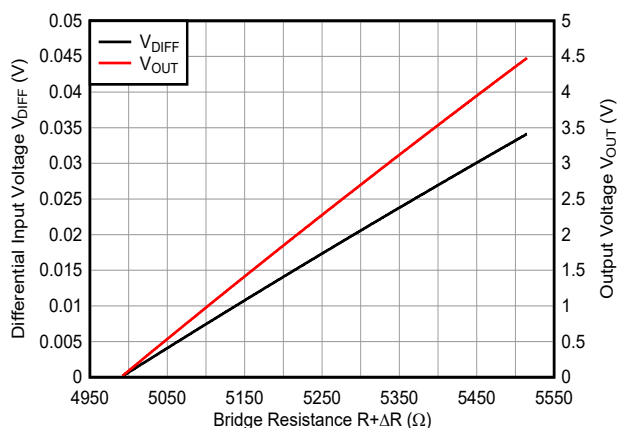
Equation 8 calculates the gain-setting resistor value using the INA823 gain equation shown in Equation 2:

$$R_G = \frac{100 \text{ k}\Omega}{G - 1} = \frac{100 \text{ k}\Omega}{131.77 \text{ V/V} - 1} = 764.69 \text{ }\Omega \quad (8)$$

Use a standard 0.1% resistor value of 768  $\Omega$ , so as not to exceed the full-scale range of the ADC.

### 9.2.1.3 Application Curves

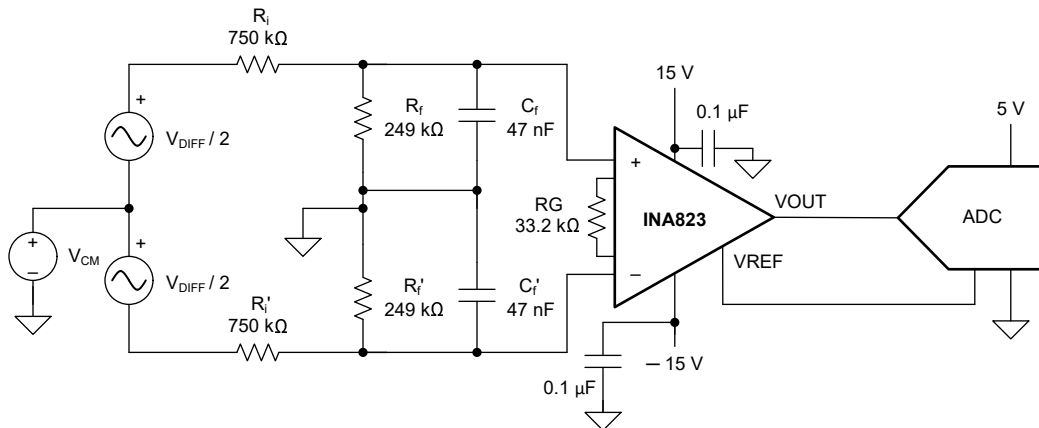
The following typical characteristic curve is for the circuit in Figure 9-2.



**Figure 9-4. Input Differential Voltage, Output Voltage vs Bridge Resistance**

### 9.2.2 Supporting High Common-Mode Voltage in PLC Input Modules

Figure 9-5 showcases a high common-mode voltage circuit that is commonly required for programmable logic controller (PLC) analog input modules. This circuit uses a resistive scaling network in front of the IA.



**Figure 9-5. High Common-Mode Voltage PLC Input Module**

For a detailed description of the passive scaling approach and more, see the [Supporting High-Voltage Common Mode Using Instrumentation Amplifier](#) application brief.

#### 9.2.2.1 Design Requirements

Table 9-2 lists the requirements for this design example.

**Table 9-2. Design Parameters**

PARAMETER	VALUE
Supply voltage	±15 V
Common-mode voltage	+36 V / -43 V
Input differential signal	1 V
Gain $V_{OUT}/V_{DIFF}$	1 V/V
Minimum dc CMRR	65 dB

#### 9.2.2.2 Detailed Design Procedure

The gain of the IA is calculated so that the circuit operates at unity gain, where  $V_{OUT} = V_{DIFF}$ .

The single-ended input impedance,  $R_{in}(SE)$ , of the circuit is the sum of the scaling resistors ( $R_f + R_i$ ). To minimize the error that is caused by the tolerance of the scaling resistors, keep  $R_{in} > 1 \text{ M}\Omega$ .

Ideally, choose the resistors so that  $R_f / R_i = R_f' / R_i'$ . In the real world, designers have to trade off between the mismatch of ratios that degrades the common-mode rejection ratio (CMRR) and the acceptable cost for the design.

The following text describe how to estimate the CMRR performance of the external resistor scaling approach. In the calculation of CMRR, the following factors are considered:

- Take into account the number of resistors, which is estimated by  $\sqrt{n}$ , where n is the number of resistors applied. In this case, this estimation results in a factor of 2.
- $\Delta R / R$  is the resistor matching ratio. The resistor tolerance for all four resistors is 0.1%.
- Take into account that a normal production distribution of the resistor value with a standard deviation of  $\pm 3 \sigma$  (99.7%). In this case, the assumption results in a factor  $\sigma = 1/3 = 0.33$  into the equation.

Equation 9 calculates the common-mode rejection ratio with given factors:

$$\text{CMRR}_{\text{dB}} = \frac{G1 + 1}{\alpha \cdot \frac{\Delta R}{R} \cdot \sqrt{n}} \quad (9)$$

$$\text{CMRR}_{\text{dB}} = \frac{0.25 + 1}{0.33 \cdot 0.1\% \cdot \sqrt{4}} = 65.5 \text{ dB} \quad (10)$$

The scaling ratio G1 is calculated by:

$$G1 = \frac{R_f}{R_f + R_i} \quad (11)$$

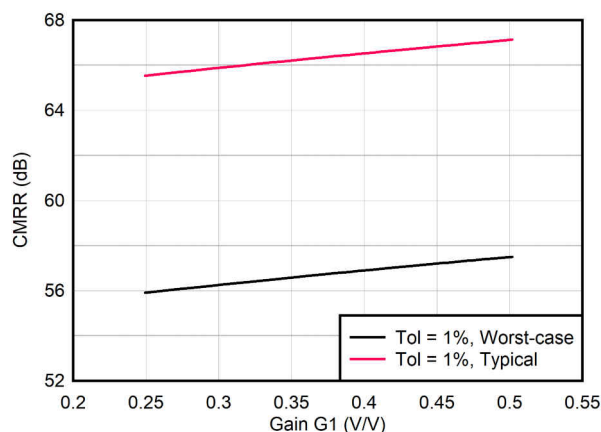
where

- $R_f$  is variable
- $R_i$  is fixed at 750 k $\Omega$ .

Figure 9-6 shows a comparison between the CMRR performance at worst-case ( $\alpha$  neglected) and considering normal distribution for different gain settings of G1.

For more details about the calculation of CMRR, see the [Difference amplifier \(subtractor\) circuit analog engineer's circuit](#).

### 9.2.2.3 Application Curves



**Figure 9-6. Common-mode Rejection Ratio of External Resistor Network for Different Scaling Ratios**

## 10 Power Supply Recommendations

The nominal performance of the INA823 is specified with a supply voltage of  $\pm 15$  V and midsupply reference voltage. The device also operates using power supplies from  $\pm 1.35$  V (2.7 V) to  $\pm 18$  V (36 V) and non-midsupply reference voltages with excellent performance. Parameters that can vary significantly with operating voltage and reference voltage are shown in [Section 7.6](#).

### CAUTION

Supply voltages higher than 40 V ( $\pm 20$  V) can permanently damage the device.

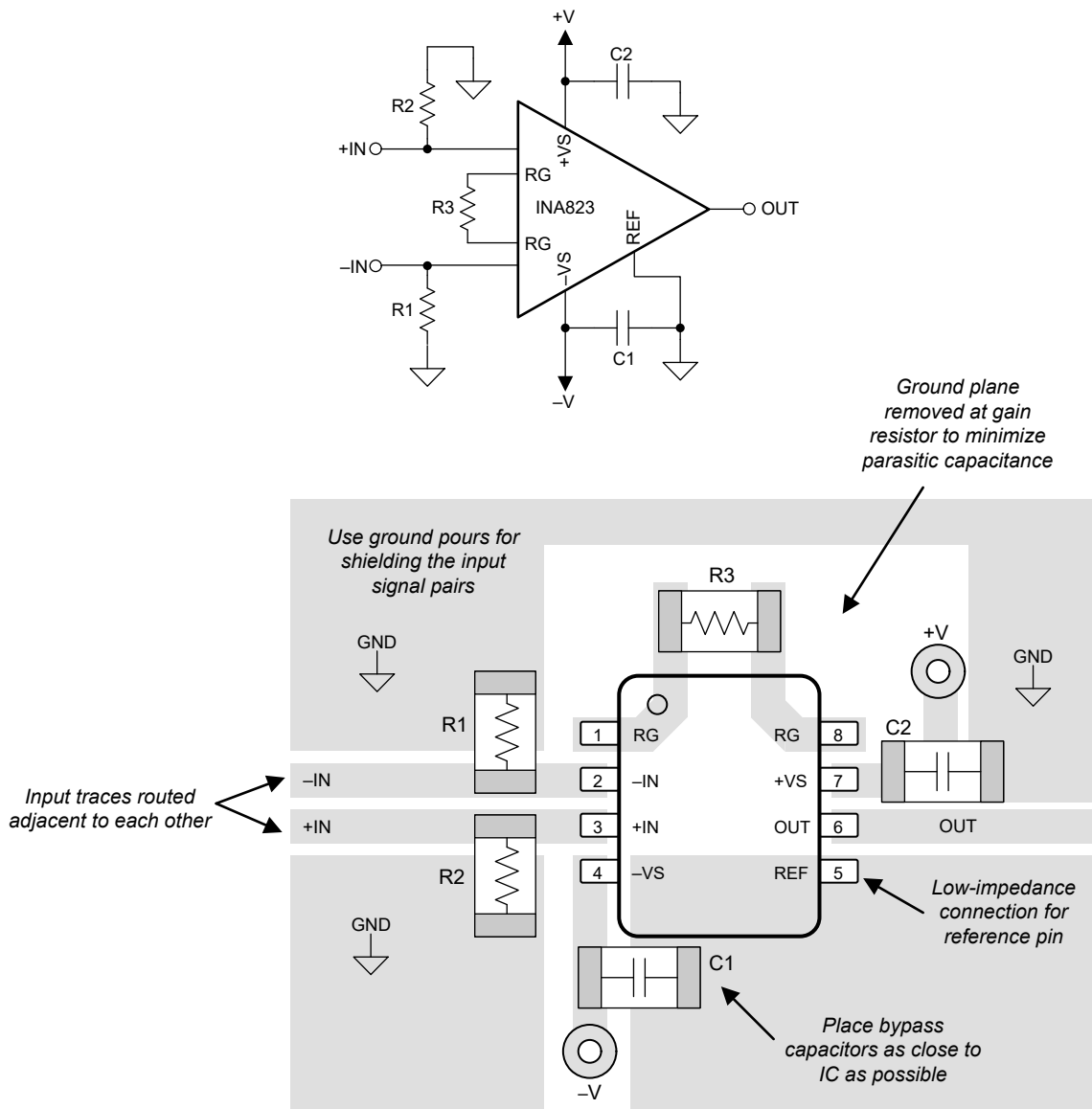
## 11 Layout

### 11.1 Layout Guidelines

Attention to good layout practices is always recommended. For best operational performance of the device, use the following PCB layout practices:

- Make sure that both input paths are well-matched for source impedance and capacitance to avoid converting common-mode signals into differential signals.
- Use bypass capacitors to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu$ F ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Route the input traces as far away from the supply or output traces as possible to reduce parasitic coupling. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better than crossing in parallel with the noisy trace.
- Place the external components as close to the device as possible.
- Use short, symmetric, and wide traces to connect the external gain resistor to minimize capacitance mismatch between the RG pins.
- Keep the traces as short as possible.

## 11.2 Layout Example



**Figure 11-1. Example Schematic and Associated PCB Layout**

## 12 Device and Documentation Support

### 12.1 Device Support

#### 12.1.1 Development Support

- [SPICE-based analog simulation program — TINA-TI software folder](#)
- [Analog Engineer's Calculator](#)

##### 12.1.1.1 PSpice® for TI

PSpice® for TI is a design and simulation environment that helps evaluate performance of analog circuits. Create subsystem designs and prototype solutions before committing to layout and fabrication, reducing development cost and time to market.

### 12.2 Documentation Support

#### 12.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, [Comprehensive Error Calculation for Instrumentation Amplifiers application note](#)
- Texas Instruments, [Importance of Input Bias Current Return Paths in Instrumentation Amplifier Applications application note](#)
- Texas Instruments, [REF50xx Low-Noise, Very Low Drift, Precision Voltage Reference data sheet](#)
- Texas Instruments, [OPAx191 36-V, Low Power, Precision, CMOS, Rail-to-Rail Input/Output, Low Offset Voltage, Low Input Bias Current Op Amp data sheet](#)

### 12.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](http://ti.com). Click on [Subscribe to updates](#) to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 12.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

### 12.5 Trademarks

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All trademarks are the property of their respective owners.

### 12.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 12.7 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
INA823DGKR	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2IVJ	<a href="#">Samples</a>
INA823DGKT	ACTIVE	VSSOP	DGK	8	250	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2IVJ	<a href="#">Samples</a>
INA823DR	ACTIVE	SOIC	D	8	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	INA823	<a href="#">Samples</a>
INA823DT	ACTIVE	SOIC	D	8	250	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	INA823	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
INA823DGKR	VSSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
INA823DGKT	VSSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
INA823DR	SOIC	D	8	3000	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
INA823DT	SOIC	D	8	250	180.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
INA823DGKR	VSSOP	DGK	8	2500	356.0	356.0	35.0
INA823DGKT	VSSOP	DGK	8	250	210.0	185.0	35.0
INA823DR	SOIC	D	8	3000	356.0	356.0	35.0
INA823DT	SOIC	D	8	250	210.0	185.0	35.0



D0008A

# PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



4214825/C 02/2019

### NOTES:

- Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- This drawing is subject to change without notice.
- This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed  $.006$  [0.15] per side.
- This dimension does not include interlead flash.
- Reference JEDEC registration MS-012, variation AA.

# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
 EXPOSED METAL SHOWN  
 SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.



# EXAMPLE BOARD LAYOUT

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

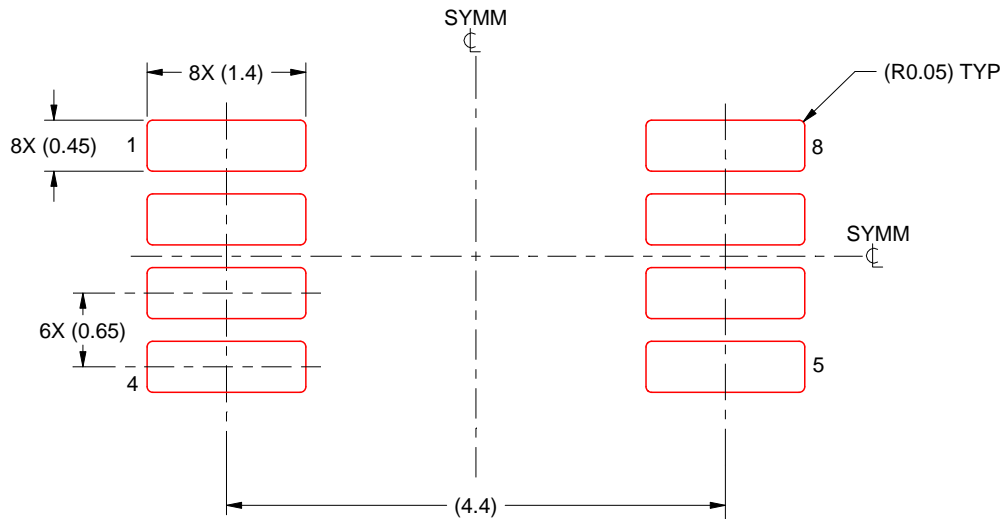
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

# EXAMPLE STENCIL DESIGN

DGK0008A

<sup>TM</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
SCALE: 15X

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NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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