



**THE DATASHEET OF
SQE48T40025-NDCKG**



SQE48T40025

Eighth-Brick DC-DC Converter

The new high performance 40 A SQE48T40025 DC-DC converter provides a high efficiency single output, in a physical package that is only 62% the size of the industry-standard quarter-brick. Specifically designed for operation in systems that have limited airflow and increased ambient temperatures, the SQE48T40025 converter utilizes the same pinout and functionality of the industry-standard quarter-bricks.

The SQE48T40025 converter provides thermal performance in high temperature environments that exceeds most 40 A quarter-bricks in the market. This performance is accomplished through the use of patented/patent-pending circuits, packaging, and processing techniques to achieve ultra-high efficiency, excellent thermal management, and a low-body profile.

Low-body profile and the preclusion of heat sinks minimize impedance to system airflow, thus enhancing cooling for both upstream and downstream devices. The use of 100% automation for assembly, coupled with advanced electronic circuits and thermal design, results in a product with extremely high reliability.

Operating from a 36-75 V input, the SQE48T40025 converter provides a 2.5 V output voltage that can be trimmed from -20% to +10% of the nominal output voltage, thus providing outstanding design flexibility.

With standard pinout and trim equations, the SQE48T40025 converter is a perfect drop-in replacement for existing 40 A quarter-brick designs. Inclusion of this converter in a new design can result in significant board space and cost savings. The designer can expect reliability improvement over other available converters because of the SQE48T40025's optimized thermal efficiency.



Key Features & Benefits

- 36-75 VDC Input; 2.5 VDC @ 40 A Output
- Industry-standard quarter-brick pinout
- On-board input differential LC-filter
- Start-up into pre-biased load
- No minimum load required
- Low height of 0.374" (9.5 mm) / Weight 0.88 oz [25.1 g]
- Withstands 100 V input transient for 100 ms
- Fixed-frequency operation
- Remote output sense
- Positive or negative logic ON/OFF option
- Output voltage trim range: +10%/-20% with industry-standard trim equations
- High reliability: MTBF = 15.4 million hours, calculated per Telcordia SR-332, Method I Case 1
- Designed to meet Class B conducted emissions per FCC and EN 55022 when used with external filter
- All materials meet UL94, V-0 flammability rating
- RoHS lead-free solder and lead-solder-exempted products are available
- Approved to the latest edition and amendment of ITE Safety standards UL/CSA 60950-1



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1. ELECTRICAL SPECIFICATIONS

Conditions: $T_A = 25\text{ }^\circ\text{C}$, Airflow = 300 LFM (1.5 m/s), $V_{in} = 48\text{ VDC}$, $C_{in} = 33\text{ }\mu\text{F}$, unless otherwise specified.

| PARAMETER | DESCRIPTION / CONDITION | MIN | TYP | MAX | UNITS |
|---|---------------------------------------|------|-----|-------|------------------|
| Absolute Maximum Ratings | | | | | |
| Input Voltage | Continuous | -0.3 | | 80 | VDC |
| Operating Ambient Temperature | | -40 | | 85 | $^\circ\text{C}$ |
| Operating Altitude | $I_{out} = 40\text{ A}$ | | | 3000 | m |
| | $I_{out} \leq 32\text{ A}$ | 3001 | | 10000 | m |
| Storage Temperature | | -55 | | 125 | $^\circ\text{C}$ |
| Isolation Characteristics | | | | | |
| Standard Product: Option 0 (refer to Converter Part Numbering / Ordering Information) | | | | | |
| I/O Isolation | | 2250 | | | VDC |
| Isolation Capacitance | | | 160 | | pF |
| Isolation Resistance | | 10 | | | $\text{M}\Omega$ |
| Option K (refer to Converter Part Numbering / Ordering Information) | | | | | |
| I/O Isolation | | 1500 | | | VDC |
| Isolation Capacitance | | | 200 | 1500 | pF |
| Isolation Resistance | | 10 | | | $\text{M}\Omega$ |
| Feature Characteristics | | | | | |
| Switching Frequency | | | 440 | | kHz |
| Output Voltage Trim Range ¹ | Industry-std. equations | -20 | | +10 | % |
| Remote Sense Compensation ¹ | Percent of $V_{OUT(NOM)}$ | | | +10 | % |
| Output Overvoltage Protection | Non-latching | 117 | 122 | 130 | % |
| Overtemperature Shutdown (PCB) | Non-latching | | | 125 | $^\circ\text{C}$ |
| Operating Humidity | Non-condensing | | | 95 | % |
| Storage Humidity | Non-condensing | | | 95 | % |
| Peak Back-drive Output Current (Sinking current from external source) during startup into pre-biased output | Peak amplitude | | 1 | | ADC |
| | Peak duration | | 50 | | μs |
| Back-drive Output Current (Sinking Current from external source) | Converter OFF; external voltage 5 VDC | | 10 | 50 | mADC |
| Auto-Restart Period | Applies to all protection features | | 200 | | ms |
| Turn-On Time | See Figures E, F, and G | | 3 | 15 | ms |
| ON/OFF Control (Positive Logic) | Converter Off (logic low) | -20 | | 0.8 | VDC |
| | Converter On (logic high) | 2.4 | | 20 | VDC |
| ON/OFF Control (Negative Logic) | Converter Off (logic high) | 2.4 | | 20 | VDC |
| | Converter On (logic low) | -20 | | 0.8 | VDC |

¹ V_{out} can be increased up to 10% via the sense leads or 10% via the trim function. However, the total output voltage trim from all sources should not exceed 10% of V_{OUT} (nom), in order to ensure specified operation of overvoltage protection circuitry.

| Input Characteristics | | | | | |
|--|--|------|---------------------|--------|---------------------|
| Operating Input Voltage Range | | 36 | 48 | 75 | VDC |
| Input Undervoltage Lockout | Turn-on Threshold | 33 | | 35.5 | VDC |
| | Turn-off Threshold | 32.5 | | 34.5 | VDC |
| Lockout Hysteresis Voltage | | 1.0 | | 2.0 | VDC |
| Input Voltage Transient | 100 ms | | | 100 | VDC |
| Input Voltage Transient Rate | | | | 7 | V/ms |
| Input Current Transient Rate | | | | 0.1 | A2s |
| Required Input Capacitance | ESR < 1Ω | 33 | | | μF |
| Maximum Input Current | 40 ADC Out @ 36 VDC In; VOUT = 2.5 VDC | | | 2.4 | ADC |
| Input Stand-by Current | Vin = 48 V, converter disabled | | 3.5 | | mA |
| Input No Load Current (0A load on the output) | Vin = 48 V, converter enabled; VOUT = 2.5 VDC | | 39 | 50 | mA |
| Input Reflected-Ripple Current, <i>i_s</i> | Vin = 48 V, 25 MHz bandwidth; VOUT = 2.5 VDC | | 6 | 30 | mAPK-PK |
| Input Voltage Ripple Rejection | 120 Hz, VOUT = 2.5 VDC | | 60 | | dB |
| Output Characteristics | | | | | |
| External Load Capacitance | Plus full load (resistive) | | | 10,000 | μF |
| Output Current Range | | 0 | | 40 | ADC |
| Current Limit Inception | Non-latching | 42 | | 52 | ADC |
| Peak Short-Circuit Current | Non-latching, Short = 10 mΩ | | | 61 | A |
| RMS Short-Circuit Current | Non-latching | | 6 | 8 | Arms |
| Output Voltage Set Point (no load) ² | | -1 | | +1 | %Vout |
| Output Regulation | Over Line | | ±2 | ±5 | mV |
| | Over Load | | ±2 | ±5 | mV |
| Output Voltage Range | Over line, load and temperature (-40 °C to 85 °C) | -3.0 | | +3.0 | %Vout |
| Output Ripple and Noise – 25 MHz bandwidth | Full load + 10 μF tantalum + 1 μF ceramic V _{OUT} = 2.5 VDC | | 35 | 50 | mV _{PK-PK} |
| Dynamic Response | | | | | |
| Load Change 50%-75%-50% of I _{out} Max, di/dt = 0.1 A/μs | Co = 1 μF ceramic (Figure 8) | | 30 | | mV |
| di/dt = 2.5 A/μs | Co = 470 μF POS + 1 μF ceramic | | 60 | | mV |
| Settling Time to 1% of Vout | | | 15 | | μs |
| Efficiency | | | | | |
| 100% Load | V _{OUT} = 2.5 VDC | | 89.0 | | % |
| 50% Load | V _{OUT} = 2.5 VDC | | 92.5 | | % |
| Mechanical | | | | | |
| Weight | | | 25.1 g | | |
| Vibration IEC Class 3M5 | Freq. Velocity IEC 68-2-6 | | 5-9 Hz 5 mm/s | | |
| | Freq. Accelerat. IEC 68-2-6 | | 9-200 Hz 1 g | | |
| Shocks IEC Class 3M5 | Accelerat. IEC 68-2-29 | | 10 g | | |
| | MIL-STD-202F | | Method 213B Cond. F | | |
| Reliability | | | | | |
| MTBF | Telcordia SR-332, Method I Case 1 50% electrical stress, 40°C ambient | | 15.4 | | MHrs |

2. OPERATIONS

2.1 INPUT AND OUTPUT IMPEDANCE

These power converters have been designed to be stable with no external capacitors when used in low inductance input and output circuits.

However, in some applications, the inductance associated with the distribution from the power source to the input of the converter can affect the stability of the converter. A 33 μF electrolytic capacitor with an ESR $< 1 \Omega$ across the input is required to ensure proper operation of the converter over wide range of input source impedance and transients.

In many applications, the user has to use decoupling capacitance at the load. The power converter will exhibit stable operation with external load capacitance up to 10,000 μF .

2.2 ON/OFF (Pin 2)

The ON/OFF pin is used to turn the power converter on or off remotely via a system signal. There are two remote control options available, positive and negative logic, with both referenced to $V_{in(-)}$. A typical connection is shown in Fig. A.

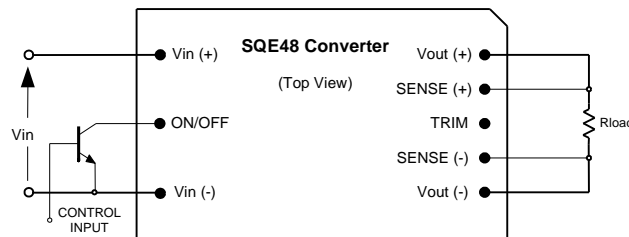


Figure A. Circuit configuration for ON/OFF function.

The positive logic version turns on when the ON/OFF pin is at a logic high and turns off when the pin is at a logic low. The converter is on when the ON/OFF pin is left open. See the Electrical Specifications for logic high/low definitions.

The negative logic version turns on when the pin is at a logic low and turns off when the pin is at a logic high. The ON/OFF pin can be hard wired directly to $V_{in(-)}$ to enable automatic power up of the converter without the need of an external control signal.

The ON/OFF pin is internally pulled up to 5 V through a resistor. A properly de-bounced mechanical switch, open-collector transistor, or FET can be used to drive the input of the ON/OFF pin. The device must be capable of sinking up to 0.2 mA at a low level voltage of $\leq 0.8 \text{ V}$. An external voltage source ($\pm 20 \text{ V}$ maximum) may be connected directly to the ON/OFF input, in which case it must be capable of sourcing or sinking up to 1 mA depending on the signal polarity. See the Startup Information section for system timing waveforms associated with use of the ON/OFF pin.

2.3 REMOTE SENSE (PINS 5 AND 7)

The remote sense feature of the converter compensates for voltage drops occurring between the output pins of the converter and the load. The SENSE (-) (Pin 5) and SENSE (+) (Pin 7) pins should be connected at the load or at the point where regulation is required (see Fig. B).

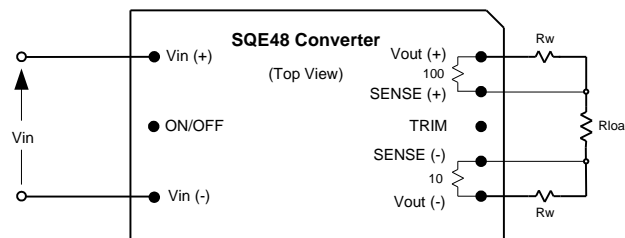


Figure B. Remote sense circuit configuration.

CAUTION

If remote sensing is not utilized, the SENSE(-) pin must be connected to the Vout(-) pin (Pin 4), and the SENSE(+) pin must be connected to the Vout(+) pin (Pin 8) to ensure the converter will regulate at the specified output voltage. If these connections are not made, the converter will deliver an output voltage that is higher than the specified data sheet value.

Because the sense leads carry minimal current, large traces on the end-user board are not required. However, sense traces should be run side by side and located close to a ground plane to minimize system noise and ensure optimum performance. The converter’s output overvoltage protection (OVP) senses the voltage across Vout(+) and Vout(-), and not across the sense lines, so the resistance (and resulting voltage drop) between the output pins of the converter and the load should be minimized to prevent unwanted triggering of the OVP.

When utilizing the remote sense feature, care must be taken not to exceed the maximum allowable output power capability of the converter, which is equal to the product of the nominal output voltage and the allowable output current for the given conditions.

When using remote sense, the output voltage at the converter can be increased by as much as 10% above the nominal rating in order to maintain the required voltage across the load. Therefore, the designer must, if necessary, decrease the maximum current (originally obtained from the derating curves) by the same percentage to ensure the converter’s actual output power remains at or below the maximum allowable output power.

2.4 OUTPUT VOLTAGE ADJUST / TRIM (PIN 6)

The output voltage can be adjusted up 10% or down 20%, relative to the rated output voltage by the addition of an externally connected resistor.

The TRIM pin should be left open if trimming is not being used. To minimize noise pickup, a 0.1 μF capacitor is connected internally between the TRIM and SENSE(-) pins.

To increase the output voltage, refer to Fig. C. A trim resistor, R_{T-INCR}, should be connected between the TRIM (Pin 6) and SENSE(+) (Pin 7), with a value of:

$$R_{T-INCR} = \frac{5.11(100 + \Delta)V_{O-NOM} - 626}{1.225\Delta} - 10.22 \quad [k\Omega],$$

where,

R_{T-INCR} = Required value of trim-up resistor [kΩ]

V_{O-NOM} = Nominal value of output voltage [V]

$$\Delta = \left| \frac{(V_{O-REQ} - V_{O-NOM})}{V_{O-NOM}} \right| \times 100 \quad [%]$$

V_{O-REQ} = Desired (trimmed) output voltage [V].

When trimming up, care must be taken not to exceed the converter’s maximum allowable output power. See the previous section for a complete discussion of this requirement.

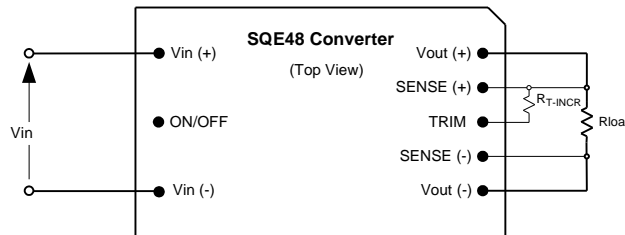


Figure C. Configuration for increasing output voltage.

To decrease the output voltage (Fig. D), a trim resistor, R_{T-DECR}, should be connected between the TRIM (Pin 6) and SENSE(-) (Pin 5), with a value of:

$$R_{T-DECR} = \frac{511}{|\Delta|} - 10.22 \quad [k\Omega]$$

where,

R_{T-DECR} = Required value of trim-down resistor [kΩ] and Δ is defined above.

NOTE:

The above equations for calculation of trim resistor values match those typically used in conventional industry-standard quarter-bricks.

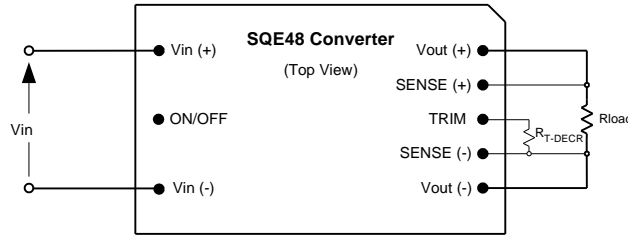


Figure D. Configuration for decreasing output voltage.

Trimming/sensing beyond 110% of the rated output voltage is not an acceptable design practice, as this condition could cause unwanted triggering of the output overvoltage protection (OVP) circuitry. The designer should ensure that the difference between the voltages across the converter's output pins and its sense pins does not exceed 10% of $V_{OUT(nom)}$, or:

$$[V_{OUT(+)} - V_{OUT(-)}] - [V_{SENSE(+)} - V_{SENSE(-)}] \leq V_{O-NOM} \times 10\% \quad [V]$$

This equation is applicable for any condition of output sensing and/or output trim.

3. PROTECTION FEATURES

3.1 INPUT UNDERVOLTAGE LOCKOUT

Input undervoltage lockout is standard with this converter. The converter will shut down when the input voltage drops below a pre-determined voltage.

The input voltage must be typically 34 V for the converter to turn on. Once the converter has been turned on, it will shut off when the input voltage drops typically below 33 V. This feature is beneficial in preventing deep discharging of batteries used in telecom applications.

3.2 OUTPUT OVERCURRENT PROTECTION (OCP)

The converter is protected against overcurrent or short circuit conditions. Upon sensing an overcurrent condition, the converter will switch to constant current operation and thereby begin to reduce output voltage.

If the converter is equipped with the special OCP version designated by the suffix K in the part number, the converter will shut down in approximately 15ms after entering the constant current mode of operation. The standard version (suffix 0) will continue operating in the constant current mode until the output voltage drops below 60% at which point the converter will shut down as shown in Figure 14.

Once the converter has shut down, it will attempt to restart nominally every 200 ms with a typical 3-5% duty cycle as shown in . The attempted restart will continue indefinitely until the overload or short circuit conditions are removed or the output voltage rises above 40-50% of its nominal value.

Once the output current is brought back into its specified range, the converter automatically exits the hiccup mode and continues normal operation.

3.3 OUTPUT OVERVOLTAGE PROTECTION (OVP)

The converter will shut down if the output voltage across $V_{out}(+)$ (Pin 8) and $V_{out}(-)$ (Pin 4) exceeds the threshold of the OVP circuitry. The OVP circuitry contains its own reference, independent of the output voltage regulation loop. Once the converter has shut down, it will attempt to restart every 200 ms until the OVP condition is removed.

3.4 OVERTEMPERATURE PROTECTION (OTP)

The converter will shut down under an overtemperature condition to protect itself from overheating caused by operation outside the thermal derating curves, or operation in abnormal conditions such as system fan failure. Converter with the non-latching option will automatically restart after it has cooled to a safe operating temperature.

3.5 SAFETY REQUIREMENTS

The converters meet the requirements of the latest edition and amendment of ITE Safety standards UL/CSA 60950-1. Basic Insulation is provided between input and output.

The converters have no internal fuse. If required, the external fuse needs to be provided to protect the converter from catastrophic failure. Refer to the "Input Fuse Selection for DC/DC converters" application note on www.belpowersolutions.com for proper selection of the input fuse. Both input traces and the chassis ground trace (if applicable) must be capable of conducting a current of 1.5 times the value of the fuse without opening. The fuse must not be placed in the grounded input line.

Abnormal and component failure tests were conducted with the input protected by a TBD fuse. If a fuse rated greater than TBD A is used, additional testing may be required. To protect a group of converters with a single fuse, the rating can be increased from the recommended value above.

3.6 ELECTROMAGNETIC COMPATIBILITY (EMC)

EMC requirements must be met at the end-product system level, as no specific standards dedicated to EMC characteristics of board mounted component DC-DC converters exist. However, Bel Power Solutions tests its converters to several system level standards, primary of which is the more stringent EN55022, *Information technology equipment - Radio disturbance characteristics-Limits and methods of measurement*.

An effective internal LC differential filter significantly reduces input reflected ripple current, and improves EMC.

With the addition of a simple external filter, the SQE48T40025 converter passes the requirements of Class B conducted emissions per EN55022 and FCC requirements. Contact Bel Power Solutions Applications Engineering for details of this testing.

4. CHARACTERIZATION

4.1 GENERAL INFORMATION

The converter has been characterized for many operational aspects, to include thermal derating (maximum load current as a function of ambient temperature and airflow) for vertical and horizontal mounting, efficiency, startup and shutdown parameters, output ripple and noise, transient response to load step-change, overload, and short circuit.

The following pages contain specific plots or waveforms associated with the converter. Additional comments for specific data are provided below.

4.2 TEST CONDITIONS

All data presented were taken with the converter soldered to a test board, specifically a 0.060" thick printed wiring board (PWB) with four layers. The top and bottom layers were not metalized. The two inner layers, comprised of two-ounce copper, were used to provide traces for connectivity to the converter.

The lack of metalization on the outer layers as well as the limited thermal connection ensured that heat transfer from the converter to the PWB was minimized. This provides a worst-case but consistent scenario for thermal derating purposes.

All measurements requiring airflow were made in the vertical and horizontal wind tunnel using Infrared (IR) thermography and thermocouples for thermometry.

Ensuring components on the converter do not exceed their ratings is important to maintaining high reliability. If one anticipates operating the converter at or close to the maximum loads specified in the derating curves, it is prudent to check actual operating temperatures in the application. Thermographic imaging is preferable; if this capability is not available, then thermocouples may be used. The use of AWG #40 gauge thermocouples is recommended to ensure measurement accuracy. Careful routing of the thermocouple leads will further minimize measurement error. Refer to Fig. E for the optimum measuring thermocouple locations.



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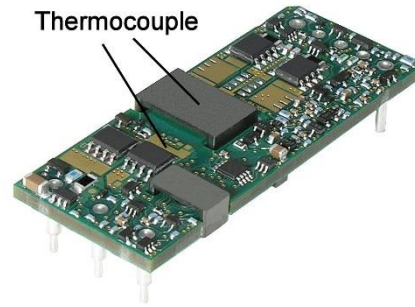


Fig. E: Location of the thermocouple for thermal testing.

4.3 THERMAL DERATING

Load current vs. ambient temperature and airflow rates are given in Figure 1. Ambient temperature was varied between 25°C and 85°C, with airflow rates from 30 to 500 LFM (0.15 to 2.5 m/s).

For each set of conditions, the maximum load current was defined as the lowest of:

- (i) The output current at which any FET junction temperature does not exceed a maximum temperature of 120 °C as indicated by the thermographic image, or
- (ii) The temperature of the transformer does not exceed 120 °C, or
- (iii) The nominal rating of the converter (40 A at 2.5 V).

During normal operation, derating curves with maximum FET temperature less or equal to 120 °C should not be exceeded. Temperature at both thermocouple locations shown in Fig. E should not exceed 120 °C in order to operate inside the derating curves.

4.4 EFFICIENCY

Figure 2 shows the efficiency vs. load current plot for ambient temperature of 25 °C, airflow rate of 300 LFM (1.5 m/s) with vertical mounting and input voltages of 36 V, 48 V, and 72 V. Also, a plot of efficiency vs. load current, as a function of ambient temperature with $V_{in} = 48$ V, airflow rate of 200 LFM (1 m/s) with vertical mounting is shown in Figure 3.

4.5 POWER DISSIPATION

Figure 4 shows the power dissipation vs. load current plot for $T_a = 25$ °C, airflow rate of 300 LFM (1.5 m/s) with vertical mounting and input voltages of 36 V, 48 V, and 72 V. Also, a plot of power dissipation vs. load current, as a function of ambient temperature with $V_{in}=48$ V, airflow rate of 200 LFM (1 m/s) with vertical mounting is shown in Figure 5.

4.6 STARTUP

Output voltage waveforms, during the turn-on transient using the ON/OFF pin for full rated load currents (resistive load) are shown without and with external load capacitance in Figure 6 and Figure 7, respectively.

4.7 RIPPLE AND NOISE

Figure 10 shows the output voltage ripple waveform, measured at full rated load current with a 10 μ F tantalum and 1 μ F ceramic capacitor across the output. Note that all output voltage waveforms are measured across a 1 μ F ceramic capacitor. The input reflected-ripple current waveforms are obtained using the test setup shown in Figure 11. The corresponding waveforms are shown in Figure 12 and Figure 13.

4.8 STARTUP INFORMATION (USING NEGATIVE ON/OFF)

Scenario #1: Initial Start-up From Bulk Supply
 ON/OFF function enabled, converter started via application of V_{IN} . See Figure F.

| Time | Comments |
|-------|---|
| t_0 | ON/OFF pin is ON; system front end power is toggled on, V_{IN} to converter begins to rise. |
| t_1 | V_{IN} crosses Under-Voltage Lockout protection circuit threshold; converter enabled. |
| t_2 | Converter begins to respond to turn-on command (converter turn-on delay). |
| t_3 | Converter V_{OUT} reaches 100% of nominal value. |

For this example, the total converter start-up time ($t_3 - t_1$) is typically 3 ms.

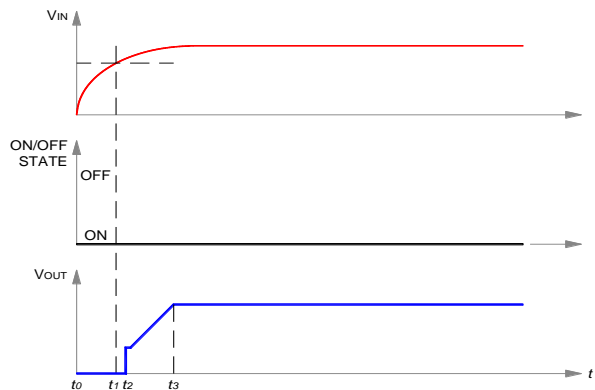


Figure F. Startup scenario #1.

Scenario #2: Initial Start-up Using ON/OFF Pin

With V_{IN} previously powered, converter started via ON/OFF pin. See Figure G.

| Time | Comments |
|-------|--|
| t_0 | V_{INPUT} at nominal value. |
| t_1 | Arbitrary time when ON/OFF pin is enabled (converter enabled). |
| t_2 | End of converter turn-on delay. |
| t_3 | Converter V_{OUT} reaches 100% of nominal value. |

For this example, the total converter start-up time ($t_3 - t_1$) is typically 3 ms.

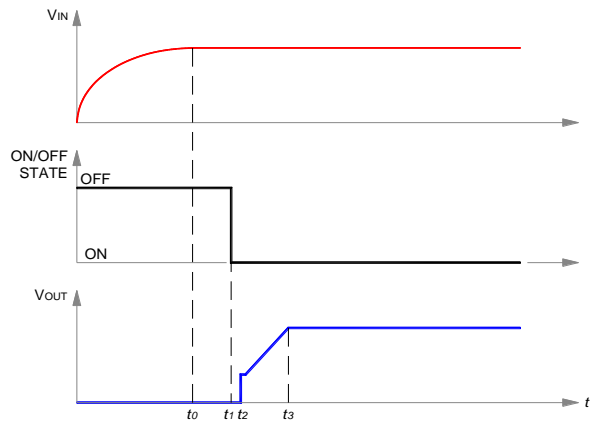


Figure G. Startup scenario #2.

Scenario #3: Turn-off and Restart Using ON/OFF Pin

With V_{IN} previously powered, converter is disabled and then enabled via ON/OFF pin. See Figure H.

| Time | Comments |
|-------|---|
| t_0 | V_{IN} and V_{OUT} are at nominal values; ON/OFF pin ON. |
| t_1 | ON/OFF pin arbitrarily disabled; converter output falls to zero; turn-on inhibit delay period (100 ms typical) is initiated, and ON/OFF pin action is internally inhibited. |
| t_2 | ON/OFF pin is externally re-enabled. If $(t_2 - t_1) \leq 200$ ms, external action of ON/OFF pin is locked out by start-up inhibit timer. If $(t_2 - t_1) > 200$ ms, ON/OFF pin action is internally enabled. |
| t_3 | Turn-on inhibit delay period ends. If ON/OFF pin is ON, converter begins turn-on; if off, converter awaits ON/OFF pin ON signal; see Figure F. |
| t_4 | End of converter turn-on delay. |
| t_5 | Converter V_{OUT} reaches 100% of nominal value. |

For the condition, $(t_2 - t_1) \leq 200$ ms, the total converter start-up time ($t_5 - t_2$) is typically 203 ms. For $(t_2 - t_1) > 200$ ms, start-up will be typically 3 ms after release of ON/OFF pin.

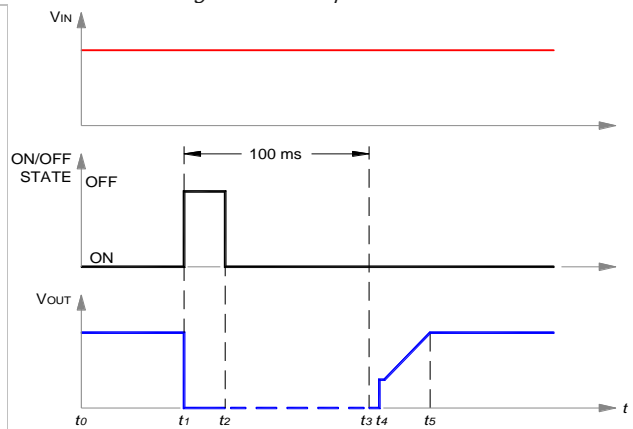


Figure H. Startup scenario #3.



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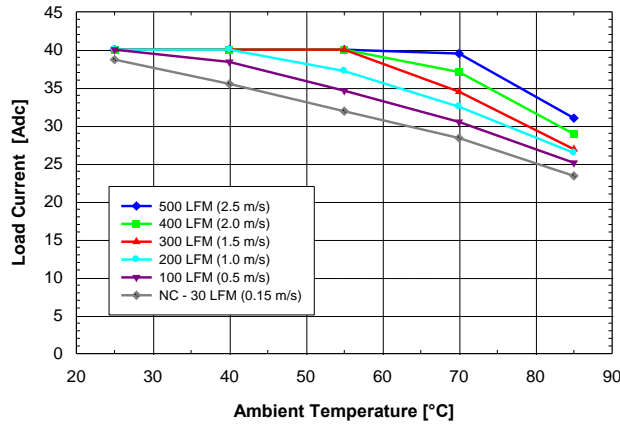


Figure 1. Available load current vs. ambient air temperature and airflow rates for SQE48T40025 converter mounted vertically with air flowing from pin 3 to pin 1, MOSFET temperature $\leq 120\text{ }^{\circ}\text{C}$, $V_{in} = 48\text{ V}$. (Note: NC – Natural convection)

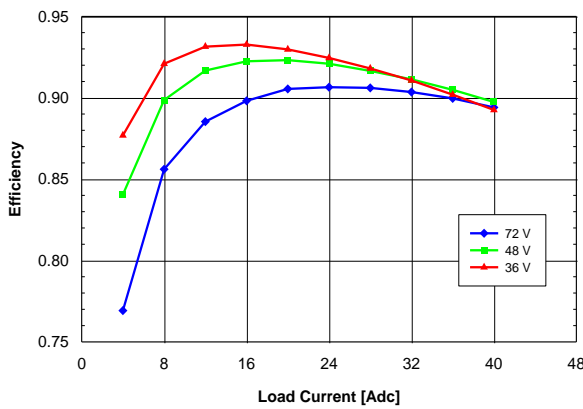


Figure 2. Efficiency vs. load current and input voltage for SQE48T40025 converter mounted vertically with air flowing from pin 3 to pin 1 at 300 LFM (1.5 m/s) and $T_a = 25\text{ }^{\circ}\text{C}$.

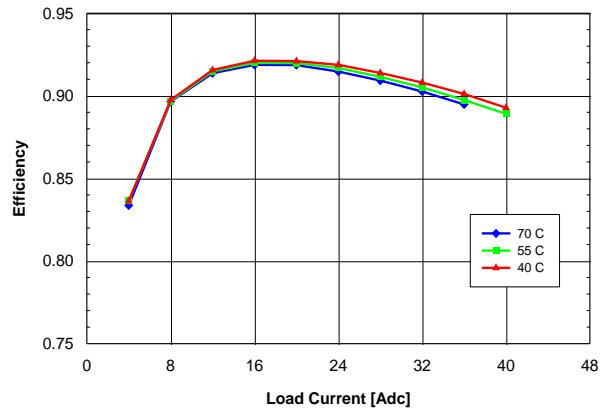


Figure 3. Efficiency vs. load current and ambient temperature for SQE48T40025 converter mounted vertically with $V_{in} = 48\text{ V}$ and air flowing from pin 3 to pin 1 at 200 LFM (1.0 m/s).

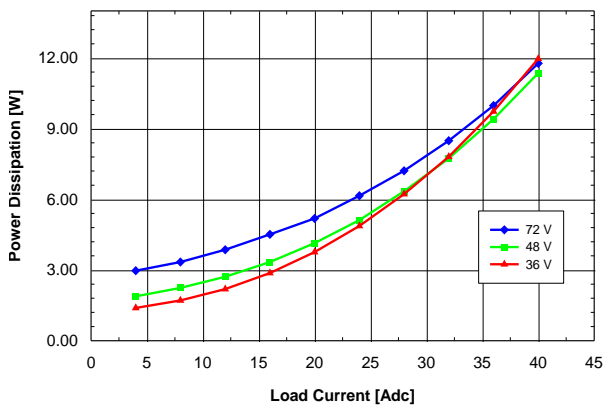


Figure 4. Power dissipation vs. load current and input voltage for SQE48T40025 converter mounted vertically with air flowing from pin 3 to pin 1 at a rate of 300 LFM (1.5 m/s) and $T_a = 25\text{ }^{\circ}\text{C}$.

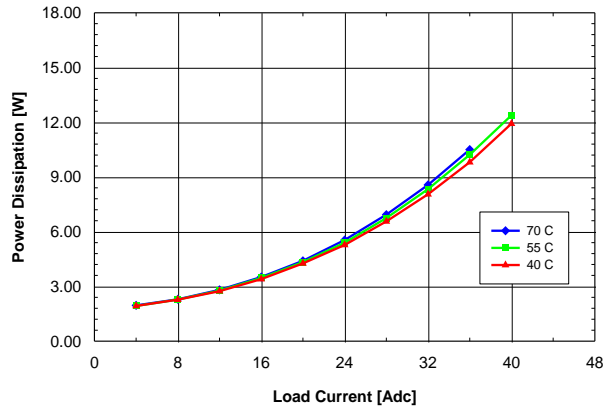


Figure 5. Power dissipation vs. load current and ambient temperature for SQE48T40025 converter mounted vertically with $V_{in} = 48\text{ V}$ and air flowing from pin 3 to pin 1 at a rate of 200 LFM (1.0 m/s).

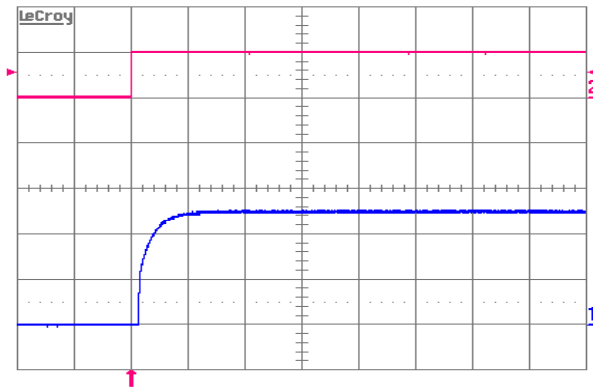


Figure 6. Turn-on transient at full rated load current (resistive) with no output capacitor at $V_{in} = 48\text{ V}$, triggered via ON/OFF pin. Top trace: ON/OFF signal (5V/div.). Bottom trace: Output voltage (1.0 V/div.). Time scale: 5 ms/div.

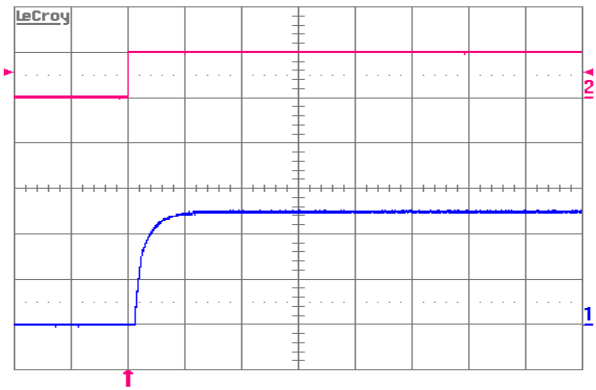


Figure 7. Turn-on transient at full rated load current (resistive) plus 10,000 μF at $V_{in} = 48\text{ V}$, triggered via ON/OFF pin. Top trace: ON/OFF signal (5 V/div.). Bottom trace: Output voltage (1.0 V/div.). Time scale: 5 ms/div.

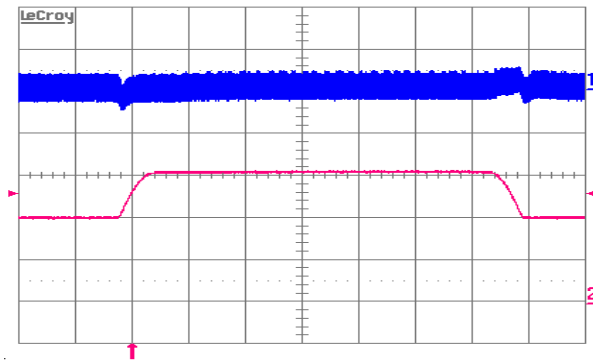


Figure 8. Output voltage response to load current step-change (20 A - 30 A - 20 A) at $V_{in} = 48\text{ V}$. Top trace: output voltage (20 mV/div.). Bottom trace: load current (10 A/div.). Current slew rate: 0.1 A/ μs . $C_o = 1\ \mu\text{F}$ ceramic. Time scale: 0.2ms/div.

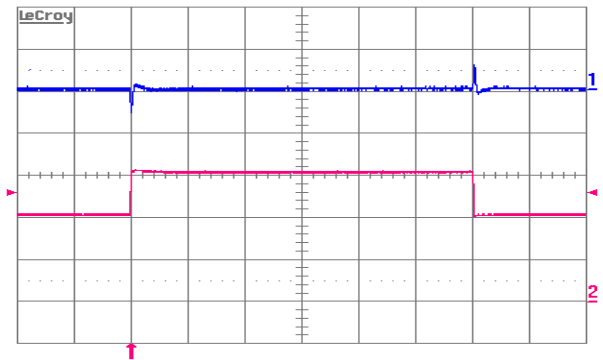


Figure 9. Output voltage response to load current step-change (20 A - 30 A - 20 A) at $V_{in} = 48\text{ V}$. Top trace: output voltage (100 mV/div.). Bottom trace: load current (10 A/div.). Current slew rate: 2.5 A/ μs . $C_o = 470\ \mu\text{F POS} + 1\ \mu\text{F}$ ceramic. Time scale: 0.2 ms/div.

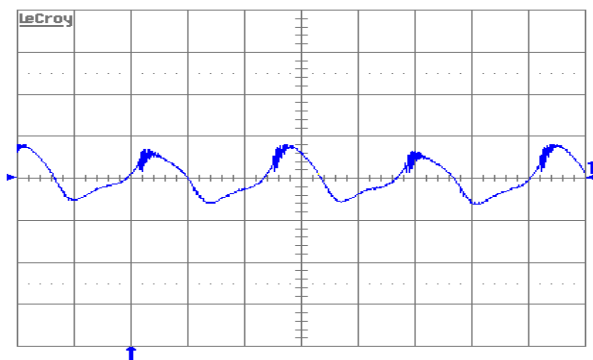


Figure 10. Output voltage ripple (20 mV/div.) at full rated load current into a resistive load with $C_o = 10\ \mu\text{F}$ tantalum + 1 μF ceramic and $V_{in} = 48\text{ V}$. Time scale: 1 μs /div.

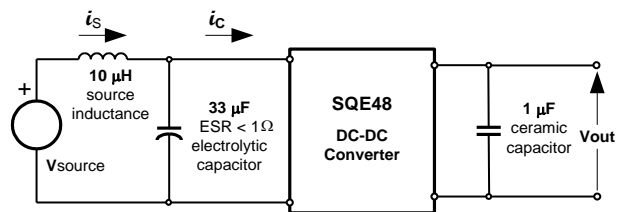


Figure 11. Test setup for measuring input reflected ripple currents, i_c and i_s .

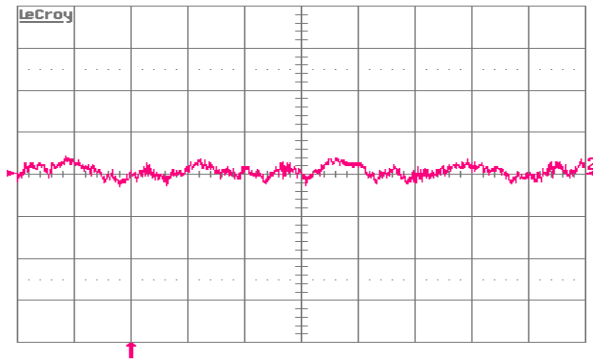


Figure 12. Input reflected-ripple current, i_s (10 mA/div.), measured through 10 μ H at the source at full rated load current and $V_{in} = 48$ V. Refer to **Error! Reference source not found.** for test setup. Time scale: 1 μ s/div.

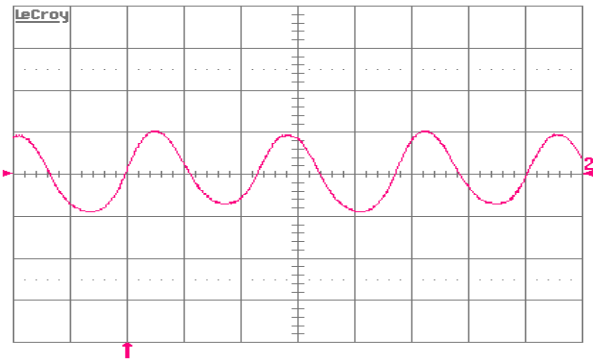


Figure 13. Input reflected ripple-current, i_c (100 mA/div.), measured at input terminals at full rated load current and $V_{in} = 48$ V. Refer to Figure 11 for test setup. Time scale: 1 μ s/div.

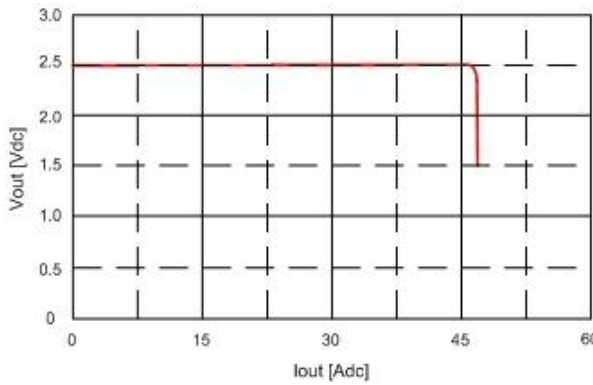


Figure 14. Output voltage vs. load current showing current limit point and converter shutdown point. Input voltage has almost no effect on current limit characteristic.

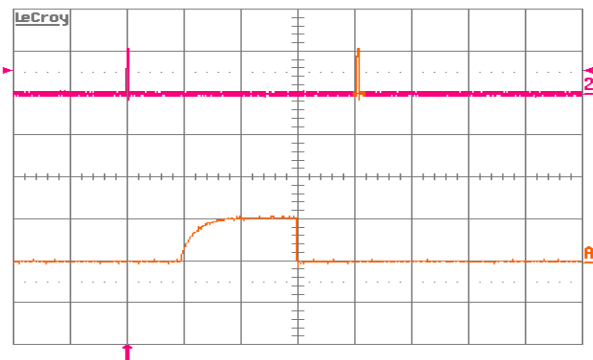
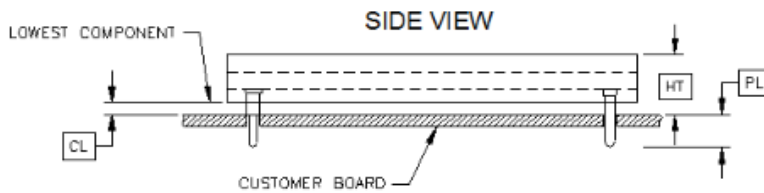
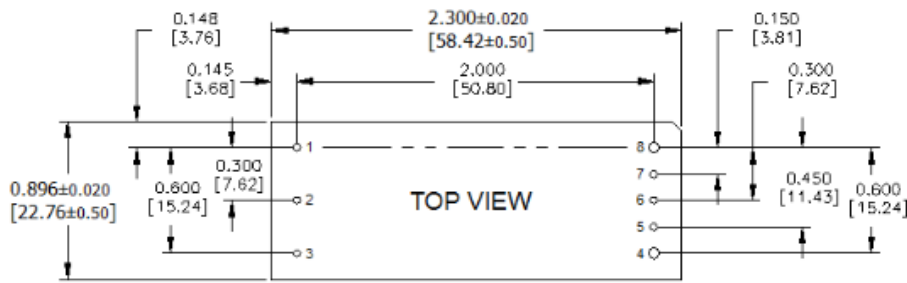


Figure 15. Load current (top trace, 50 A/div., 50 ms/div.) into a 10 m Ω short circuit during restart, at $V_{in} = 48$ V. Bottom trace 50 A/div., 1 ms/div.) is an expansion of the on-time portion of the top trace.

5. MECHANICAL PARAMETERS



SQE48T Pinout (Through-hole)

| PAD/PIN CONNECTIONS | |
|---------------------|----------|
| Pad/Pin # | Function |
| 1 | Vin (+) |
| 2 | ON/OFF |
| 3 | Vin (-) |
| 4 | Vout (-) |
| 5 | SENSE(-) |
| 6 | TRIM |
| 7 | SENSE(+) |
| 8 | Vout (+) |

| Pin Option | PL Pin Length |
|------------|----------------|
| | ±0.005 [±0.13] |
| A | 0.188 [4.77] |
| C | 0.110 [2.79] |

SQE48T Platform Notes

- All dimensions are in inches [mm]
- Pins 1-3 and 5-7 are $\varnothing 0.040$ [1.02] with $\varnothing 0.078$ [1.98] shoulder
- Pins 4 and 8 are $\varnothing 0.062$ [1.57] without shoulder
- Pin Material: Brass Alloy 360
- Pin Finish: Tin over Nickel

| Height Option | HT (Max. Height) | CL (Min. Clearance) |
|---------------|----------------------------------|----------------------------------|
| | +0.000 [+0.00] -0.038 [-0.97] | +0.016 [+0.41] -0.000 [-0.00] |
| D | 0.374 [9.5] | 0.045 [1.14] |

6. ORDERING INFORMATION

| Product Series ¹ | Input Voltage | Mounting Scheme | Rated Load Current | Output Voltage | ON/OFF Logic | Maximum Height [HT] | Pin Length [PL] | Special Features | RoHS | |
|--------------------------------|---------------|------------------|--------------------|----------------|------------------------------|---------------------|--|--|---|----------|
| SQE | 48 | T | 40 | 025 | - | N | D | A | K | G |
| 1/8 th Brick Format | 36-75 V | T ⇒ Through-hole | 40 A | 025 ⇒ 2.5 V | N ⇒ Negative P ⇒ Positive | D ⇒ 0.374" | Through hole A ⇒ 0.188" C ⇒ 0.110" | 0 ⇒ 2250VDC isolation, no CM cap K ⇒ 1500VDC isolation, CM cap, and special OCP | No Suffix ⇒ RoHS lead-solder-exemption compliant G ⇒ RoHS compliant for all six substances | |

The example above describes P/N SQE48T40025-NDAKG: 36-75 V input, through-hole, 40A @ 2.5V output, negative ON/OFF logic, maximum height of 0.374", 0.188" pins, 1500VDC isolation, common mode capacitor, special OCP, and RoHS compliant for all 6 substances. Consult factory for availability of other options.

For more information on these products consult: tech.support@psbel.com

NUCLEAR AND MEDICAL APPLICATIONS - Products are not designed or intended for use as critical components in life support systems, equipment used in hazardous environments, or nuclear control systems.

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